



Article

# Hydrodynamic Model Tests for Seaweed as a Source of Energy Reduction during Extreme Events

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**Abstract:** One fifth of the world's population and critical infrastructures are close to the coast and regions of high-risk sea level rise elevation. The last decades have been characterized by increasing extreme events, including storm surges, flooding, coastal erosion, enhanced coastal vulnerability with associated livelihood, and economic losses. Nature-based engineering solutions are being adopted as sustainable solutions for helping existing technologies live their design life and providing climate change adaptation and resilience for coastal and riverine communities. This paper involves the investigation of nature-based eco-hydraulic soft coastal engineering to cultivate seaweed for coastal protection. In this context, the present study involves an advanced risk evaluation performed by conducting an extreme bore interaction with seaweed as a soft engineering coastal protection measure. The load reduction on the inland structure during extreme flooding conditions, incorporating seaweed, is addressed. The present study indicates that the load on inland structures can be reduced by as much as 14% in extreme flooding conditions in the presence of seaweed with two rows of seaweed, indicating the usage of seaweed as a part of coastal protection over existing site protection infrastructure for improved coastal mitigation.

**Keywords:** macroalgae; nature-based solution; hydrodynamic; model test; extreme event



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## 1. Introduction

Sea level rise and ecological impacts on the ecosystem are expected to intensify coastal flood events and increase their frequency. The last decades have been characterized by increasing extreme events, including storm surges, flooding, coastal erosion, enhanced coastal vulnerability with associated livelihood, and economic losses [1–3]. Hard engineering structures such as seawalls have been used to protect inland structures from extreme hydrodynamic forces during flood inundation [4–6]. Nature-based approaches such as mangrove forests or the application of seaweed can protect infrastructure from high-energy wave events and flash floods, while also maintaining local ecosystems by regulating the local biodiversity and providing fish habitats [7–9].

Recognizing the increased risk in coastal areas due to population growth, climate change, and the shortcomings of standard mitigation measures, the demand for alternative approaches is rising [10–12]. This study involves a hydrodynamic model test experiment at the Institute of Hydraulic Engineering and Water Resources Management (IWW), RWTH Aachen University, to evaluate coastal flood energy reduction by incorporating seaweed as a soft engineering coastal protection measure and the provision of resilience for the existing environment and infrastructure.

### *Seaweed as a Source of High Wave Energy Reduction*

Seaweed (*Macroalgae*) are fast-growing aquatic plants that grow naturally in most coastal areas around the world. The application of seaweed benefits from their simple cultivation, which does not require irrigation, fertilizers, or arable land areas and can be realized as non-invasive [13–15]. The c. 10,000 existing species of seaweeds are divided into

three main groups: Phaeophyta (brown algae), Chlorophyta (green algae), and Rhodophyta (red algae). These seaweed groups have specific properties and environmental preferences (e.g., regarding salinity and water temperature). While Phaeophyta prefer environments of cold water and can reach sizes of 10–30 m, Chlorophyta are most common in coastal water, freshwater, and terrestrial environments, while generally being smaller, at around 5–10 m.

The majority of the c. 6500 Rhodophyta species are marine and prefer intertidal to subtidal environments in up to 40 m water depths. The main biomass of red algae is provided by the species Corallinaceae and Gigartinaceae, with various additional species documented for the North and Baltic Seas [16]. Rhodophyta are also common in the open sea. Besides the widespread utilization of seaweed (approx. 30 billion tons per year) as a resource for products of all types (e.g., nutrition, food, bioplastic, and pharmaceuticals) [17,18], seaweed is known to support local ecosystems by supporting the restoration of biodiversity and bioremediation, while also providing fish habitats [19,20]. On a larger scale, seaweed is attributed to positively regulating the ocean temperature, capturing carbon, and subsequently mitigating climate change [21–23]. Furthermore, seaweed is capable of mitigating the nearshore wave climate and cross-shore current velocity, thus reducing coastal erosion significantly [24].

Studies on the advantage and performance of nature for coastal protection are being explored. Seaweed is capable of mitigating the nearshore wave climate and cross-shore currents, thus reducing coastal erosion significantly [4,24]. Branched algae species act as an area reducer by limiting dragged sediment by reducing the projected area inflow. Seaweed has reportedly been found to attenuate waves by 80% [25]. However, there is a lack of available data on understanding the hydrodynamic load reduction due to seaweed platform design under extreme conditions such as coastal floods and tsunamis. Thus, model tests are the best way to quickly obtain such data. For this purpose, samples of seaweed cultures are obtained and subjected to dynamic tests. These tests are expected to provide insight into the performance of soft vegetation in coastal protection. Oladokun (2013) conducted a related experiment measuring the wave and current force loads on seaweed [26]. The present study is the extension of the first author's previous work. In this study, we investigate seaweed as a source of energy or momentum reduction, similar to hard structures such as seawalls, by analyzing the reduction in the force on the inland building.

## 2. Physical Modelling

The experiments were carried out in the Large Tilting flume at the Institute of Hydraulic Engineering and Water Resources Management, RWTH Aachen, Germany, to replicate coastal flood events on the model scale. The inundating flood during extreme events resembles the movement of the mass of water over the existing still water depth. Henceforth, the experiments were conducted with three wet bed conditions (1 cm, 3 cm, and 5 cm). The movement of the mass of water over the still water depth is called a bore [2,27]. The bore was generated with the help of two pumps. The experimental flume could generate a discharge of up to 400 L/s. The bores of different strengths were generated by controlling the opening valve positions of the two pumps. The period of bore generation could also be controlled in the current experimental facility. To generate the wet bed bore, an initial still water depth ' $d_s$ ' was ensured in the laboratory by adjusting the height of the barriers in the front end and rear end of the flume (Table 1). The generated bore in the wet bed case had an initial aerated bore front, followed by a quasi-steady flow phase; the characteristics were almost similar to the traditional tsunami bore [28–30]. The generated bore details are provided in Table 1. The test conditions in the laboratory were adopted from Harish et al. (2021) for comparability [28].

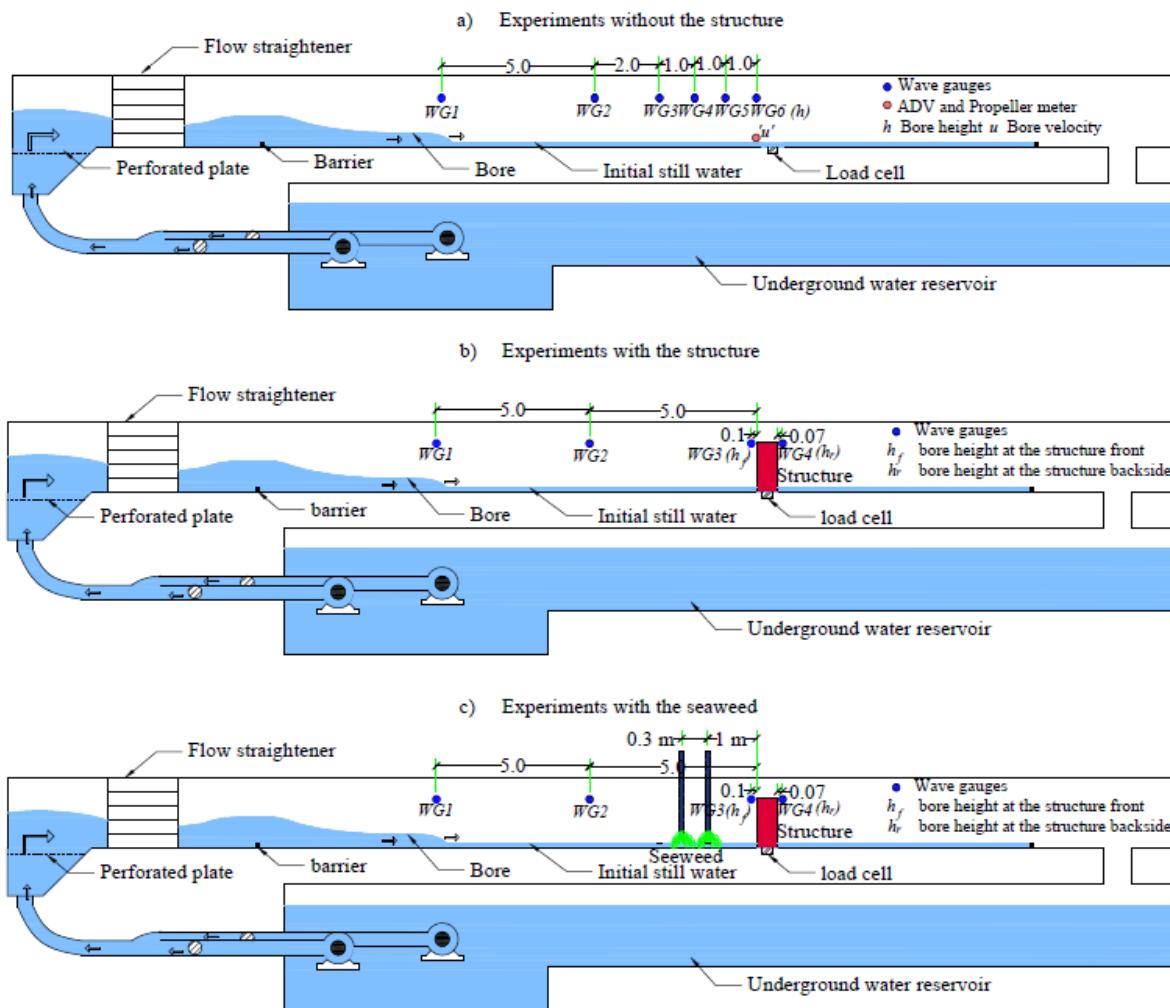
**Table 1.** Test cases were used in the experiments. Bore depth ( $h$ ) and depth-averaged velocity ( $u$ ) were measured in the absence of seaweed and the structure [31].

Test Case	$d_s = 1 \text{ cm}$		$d_s = 3 \text{ cm}$		$d_s = 5 \text{ cm}$	
	$h \text{ (m)}$	$u \text{ (m/s)}$	$h \text{ (m)}$	$u \text{ (m/s)}$	$h \text{ (m)}$	$u \text{ (m/s)}$
Case 1	0.105	1.495	0.137	1.211	0.161	1.106
Case 2	0.125	1.652	0.150	1.409	0.179	1.181
Case 3	0.146	1.744	0.174	1.526	0.208	1.143
Case 4	0.159	1.818	0.188	1.592	0.217	1.304
Case 5	0.170	1.866	0.194	1.652	0.227	1.319

The experiments were carried out at a 1:30 scale. Three sets of experiments were carried out to understand the effect of seaweed in reducing the forces on the inland structure. (1). Experiments without seaweed and the structure for understanding the free-flow hydrodynamics (bore depth,  $h$  and bore velocity,  $u$ ), (2). Experiments with the structure and without seaweed for obtaining forces in the absence of seaweed. (3). Experiments with the seaweed and structure for obtaining the force reduction. The idea behind the experiments was that design engineers can evaluate the forces on inland structures using  $h$  and  $u$  from the field measurements. As such, the second and third authors' previous study results were partially used to appreciate the force reduction in this study. The instrumentation details are provided further.

A rectangular model was placed behind the seaweed to estimate the momentum loss due to the seaweed. The model represented a typical coastal building in a 1:30 Froude scaling. The building model was made of acrylic sheets. The model had  $0.3 \text{ m} \times 0.3 \text{ m}$  in its cross-section, representing  $b/W = 0.3$  in the laboratory, where  $b$  was the building model width and  $W$  was the flow channel width. The building model was fixed at 16.9 m from the barrier (Figure 1). The seaweed was placed at 1 m and 1.3 m in front of the building. A six-axis load cell was used for measuring the force on the structure (interface force 6A130). Six ultrasonic wave gauges were used for measuring the bore height. WG6 measured the free-flow bore depth ( $h$ ) in the absence of the structure and seaweed. A propeller meter was used to measure the flow velocity ( $u$ ) at 3 cm and 6 cm from the bottom level (Figure 1a). Depth-averaged velocity was used further during the analysis. It is to be noted that the velocity measurements were carried out only for the experiments without the structure and seaweed. Figure 1 shows the location of all the instruments and the modeled structure and seaweed in the experimental flume for the experiments without the structure and the experiments with the structure and seaweed.

All the instruments were connected to a standard Data Acquisition System (NI USB-6211 DAQ). The seaweed was placed at 15.9 m and 15.6 m from the barrier (1 m and 1.3 m before the building). Once the bore generation started, the DAQ was started manually. Since all the instruments were synchronized to a single DAQ, the time synchronization was directly handled. For the analysis, the time at which the incoming bore crossed WG1 was taken as a reference time (time,  $t = 0 \text{ s}$ ), and all the data were time-shifted to this reference time for the analysis.



**Figure 1.** Schematics of the instrumentation, showing load cell installed under the structural barrier (in red, representing typical coal building) [28].

#### Seaweed Models

The 5 seaweed species are native to the European water were used for the experiment. Samples (clumps) of dried seaweed (see Figure 2) can be restored to nearly nominal properties when soaked in water for some time. A typical-size seaweed clump is shown in Figure 2. A clump may weigh up to 2.0 kg in the air when fully grown. However, the buoyancy nature of seaweed makes its weight in water almost insignificant. Nevertheless, the plant's movement affected the incoming flow characteristics, thereby reducing the flow momentum. The samples were subjected to a series of tests to determine the hydrodynamic loading coefficients in a few different configurations. The experiments followed Froude scaling laws, where the seaweed was scaled based on weight at 1:30. This scale was chosen because of the tolerable dimension of the flume and the similar scale used there in the past. The weight of typical fully-grown seaweed is provided by Oladokun, (2013) [26] and the weight of the seaweed used for our experiment was taken and scaled at 1:30 compared with the weight of fully-grown seaweed.



**Figure 2.** Clumps of 5 wet and dry seaweed.

The platform consisted of a frame, an anchoring system, and a geotextile for the algae. The frame with the seaweed was tested in the IWW flume, evaluating the force loss on the inland structure, thereby evaluating the flow attenuation.

A rope was used to tie a sufficient quantity of scaled seaweed. Up to five clumps of seaweed were hung on the line rope, which weighed up to 20 N in dry conditions. The rope was 0.1 m above the flume level. The experiments were carried out with single and two rows of seaweed. Figure 3 shows the two rows of seaweed hung in the lab before the bore interaction. In total, 30 individual experiments were carried out with the seaweed to understand the significance of seaweed in the force reduction on inland structures [6].



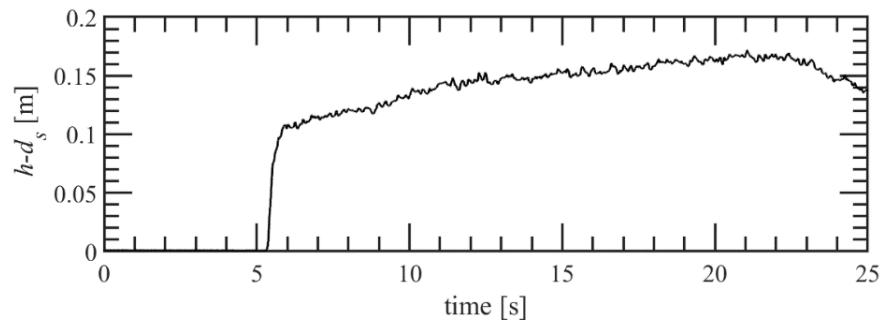
**Figure 3.** Seaweed fixed in the lab.

### 3. Result

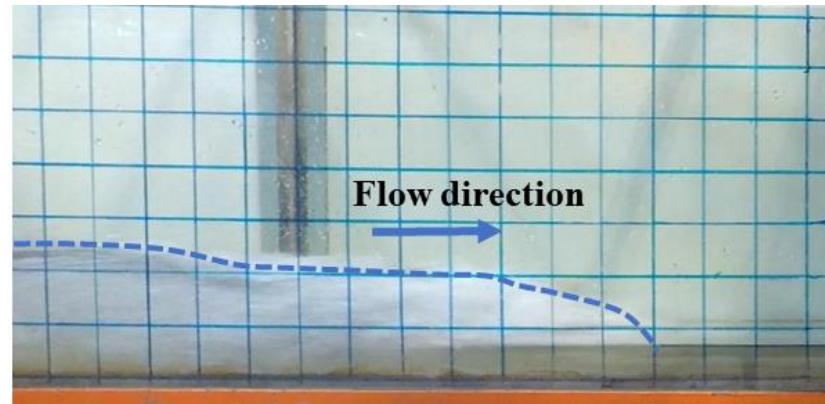
#### 3.1. Bore Characteristics in the Absence of Seaweed and the Structure

Figure 4 presents the sample bore depth time history ( $h$ ) for case 3 and  $d_s = 3$  cm. From the time history, it can be observed that the bore had a steep bore front due to the movement of the bore over a wet bed. Visually, it resembles a turbulent aerated hydraulic jump (Figure 5). In addition, the Froude number (Fr) obtained from the study was in the range of that from previously occurred tsunamis (Figure 6); hence, this study could find direct applications in tsunami studies [32–36]. The Fr was evaluated by, u refer to flow velocity

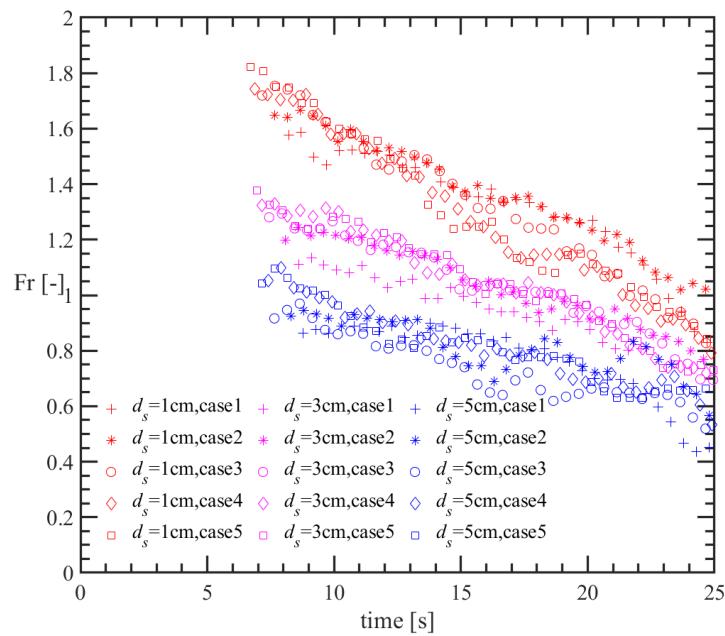
$$\text{Fr} = \frac{u}{\sqrt{gh}} \quad (1)$$



**Figure 4.** Typical bore depth time history of the generated bore in the IWW Lab.



**Figure 5.** Typical bore front propagation in the laboratory.

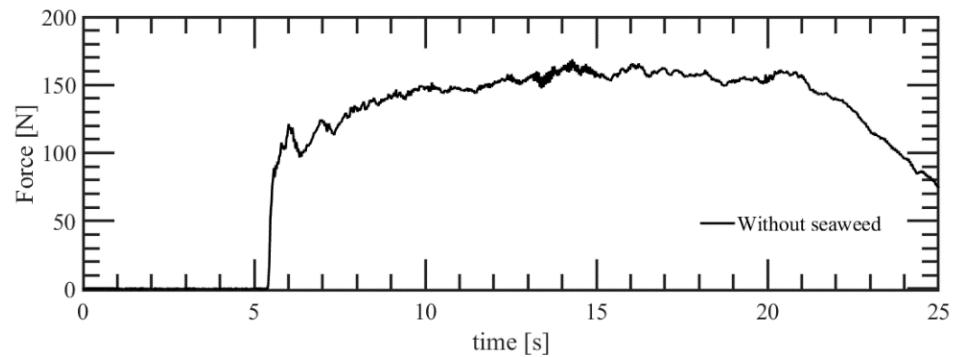


**Figure 6.** Froude number tested in this study [28].

In the Fr plot, the initial few seconds of measurements are not shown, since the bore front was a highly turbulent aerated bore front (Figure 5) that was not captured by the propeller meter [37].

### 3.2. Forces on the Building in the Absence of Seaweed

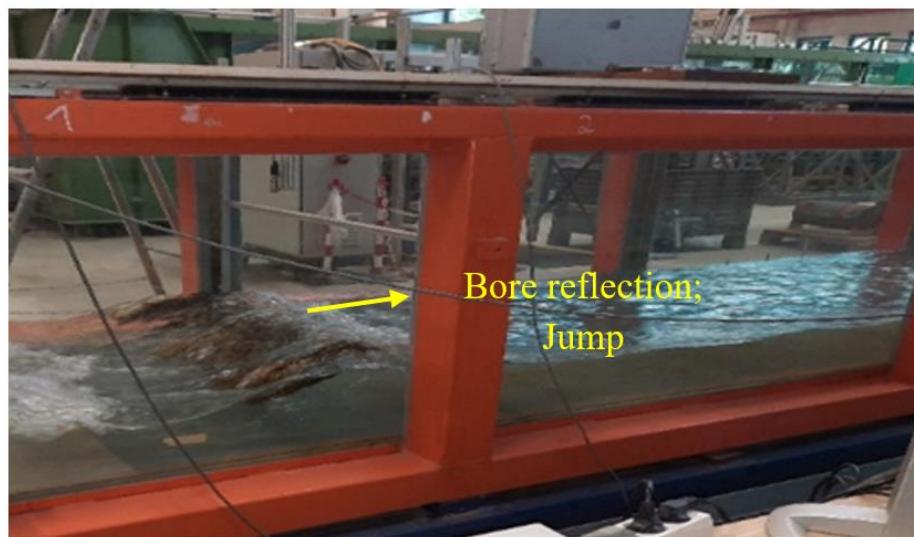
Figure 7 presents the force time history for test case 3 and  $d_s = 3$  cm. As observed, during the initial impact and initial reflection stage, a steep increase in the force on the structure was noticed.



**Figure 7.** Forces on the structure in the absence of seaweed.

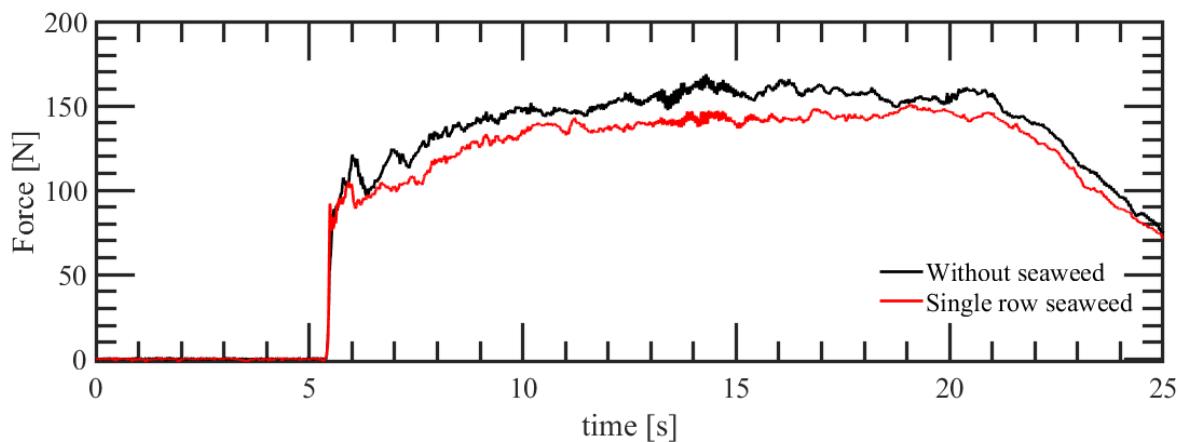
### 3.3. Experiments with a Single Row of Seaweed

Figure 8 presents a picture of the seaweed during the bore interaction with the seaweed. It was observed that, once the bore interacted with the seaweed, the seaweed floated due to the buoyancy and hydrodynamic loading.

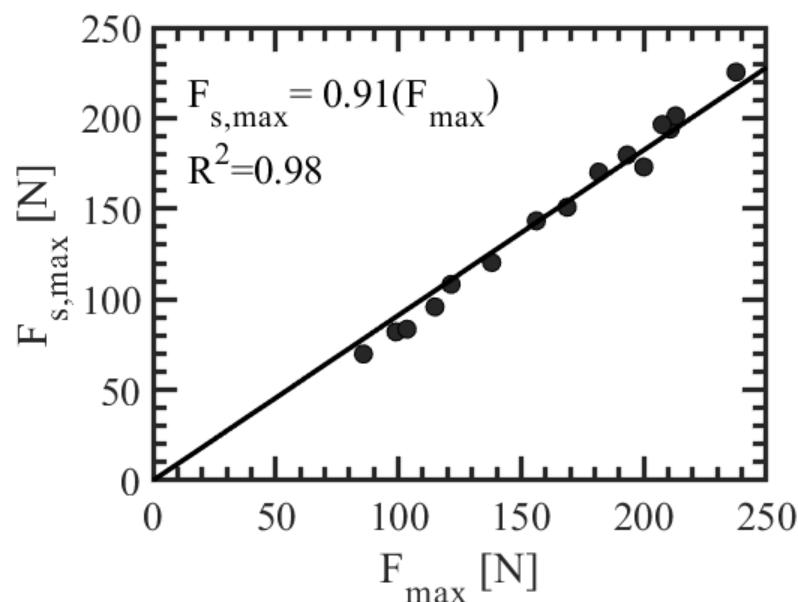


**Figure 8.** During bore interaction with the seaweed.

Figure 9 shows the force-time history of the structure with and without a single row of seaweed. As one could observe, there was a marginal decrease in the force on the inland structure due to the presence of the seaweed. Figure 10 presents a comparison between the maximum force with the seaweed and the force without the seaweed for all the test cases.



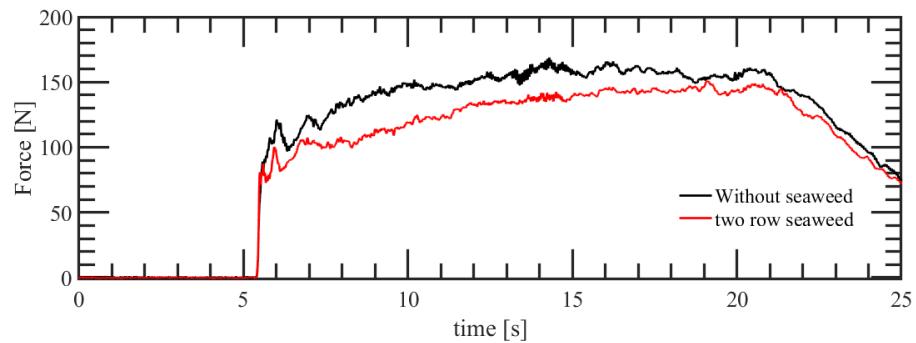
**Figure 9.** Force time history (with a single row of seaweed and without seaweed) for  $d_s = 3$  cm and Case 3.



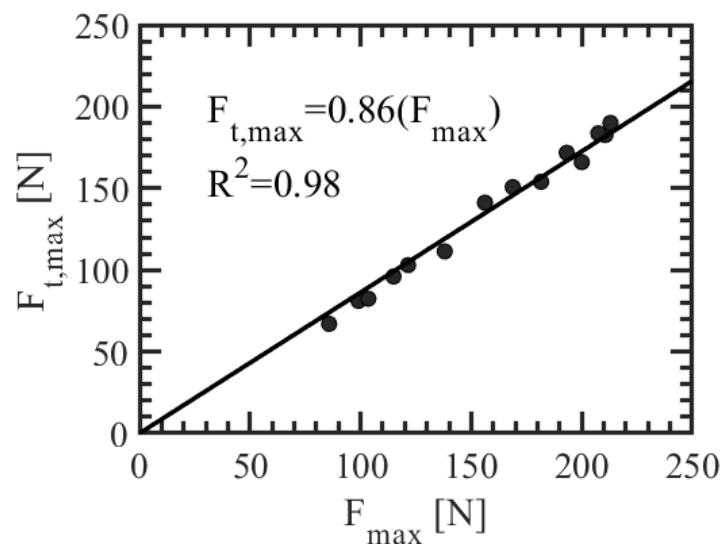
**Figure 10.** Comparison of maximum force with and without a single row of seaweed.

#### 3.4. Experiments with Two Rows of Seaweed

Figure 11 shows the force-time history of the structure with and without two rows of seaweed. It was observed that the force acting on the structure was reduced with an increase in the number of rows, as one could expect. Figure 12 presents a comparison between the maximum force with the two rows of seaweed and without the seaweed. One could observe that the linear trend line yielded a value of 0.863 with an  $R^2$  value of 0.98. This indicated that the two rows of seaweed could reduce approximately 14 percent of the force on the inland structure.



**Figure 11.** Force time history (with two rows of seaweed and without seaweed) for  $d_s = 3$  cm and Case 3.



**Figure 12.** Comparison of maximum force with two rows of seaweed and without Seaweed.

As observed in Figure 6, the Fr of the flow varied between different still water depths. Nevertheless, observing Figures 9 and 11 shows that the force reduction was independent of the test cases in different still water depths ( $d_s$ ); hence, the Fr was not in agreement with Ahmed and Ghumman (2019) [38], who observed a linear decrease in the energy reduction with an increase in the Fr in experiments with rigid vegetation.

#### 4. Discussion

##### 4.1. Bore Characteristics in the Absence of Seaweed and the Structure

As explained in Section 2, the bore characteristics in Harish et al. (2021 and 2022) [28,37] and the bore height time history in the absence of the structure at the structure location were used for the experiment. Figure 4 presents the sample bore depth time history ( $h$ ) for case 3 and  $d_s = 3$  cm. The bore steepness could also increase with the roughness of the bed [27,39]. It can be observed that the bore depth gradually increased over time, representing the continuous flow inundation during tsunamis and storm surges. Once the bore generation period ended, the flow depth was reduced drastically. Thus, the generated bore characteristics resembled a tsunami inundation or coastal flood inundation.

##### 4.2. Forces on the Building in the Absence of Seaweed

The experiments were carried out in the absence of seaweed for measuring the forces on the structure model (i.e., building) without seaweed. Figure 7 shows the force time history for test case 3 and  $d_s = 3$  cm. This was due to the steeper bore front slope in wet conditions, agreeing with Cross (1967) and Wüthrich et al. (2018) [40,41]. Nevertheless, the

maximum force occurred a long time after impact (i.e., during the quasi-steady flow phase). Furthermore, it also depended on the characteristics of the generated bore. In their studies, Harish et al. (2021) observed that, after a certain time from the bore tip interaction [28], the pressure profile on the structure's front face was linear due to the flow-choked conditions. Since the experiments mainly focused on force reduction, the maximum force ( $F_{max}$ ) was chosen for further analysis.

#### 4.3. Experiments with a Single Row of Seaweed

A single row of seaweed was placed 1 m away from the structure (building model) location.

Figure 8 presents a picture of the seaweed during the bore interaction with the seaweed. The presence of seaweed reflected a part of the incoming bore, thereby reducing the bore energy before the interaction with the building. Similar flow observations have been reported by earlier studies, which worked with rigid vegetation as a source of energy reduction [42,43]. Since the seaweeds were rigidly tightened with the side frame at the flume, the free-flow motions in the flow directions were restricted. Nevertheless, even in the field, although flexible, seaweed always sticks to the rock or the farm upon which it grows. The present study focused on understanding hydrodynamic force reduction; hence, the ends of the seaweed rope were tightened with the rigid frame.

Figure 9 revealed the force-time history of the structure with and without a single row of seaweed. The seaweed changed the overall flow behavior and induced a comparatively lesser force in the impact and quasi-steady phase. To potentially understand the force reduction, the maximum force ( $F_{s,max}$ ) in the presence of the seaweed was chosen, where the subscript represents a single row. Figure 10 shows the differences between the maximum force with the seaweed and the force without the seaweed for all the test cases. A linear trend line yielded a value of 0.912 with an  $R^2$  value of 0.98. This indicated that the force reduction in the presence of the seaweed was approximately 9% for a single row of seaweed. The percentage of force reduction was comparable to the load reduction due to the low-rise seawall tested by Thomas and Cox (2011) and Harish et al. (2022b) [44,45], who observed only a 5 to 15% reduction in the force in the presence of a seawall. Thus, growing highly tensile seaweeds could reduce the flow momentum, comparable to a low-rise seawall.

#### 4.4. Experiments with Two Rows of Seaweed

As a next step, the inland structure was tested with two rows of seaweed to better understand the overall performance in the form of seaweed bushes. In this case, another row of seaweed was placed 1.3 m away from the building model, including the first row. In Figure 11, the force-time history of the structure with and without two rows of seaweed is presented. To understand the force reduction, the maximum force on the inland building in the presence of the seaweed was chosen ( $F_{t,max}$ ), similar to the previous subsection. Figure 12 shows a comparison between the maximum force with the two rows of seaweed and without the seaweed. The linear trend line yielded a value of 0.863 with an  $R^2$  value of 0.98 being observed. Rahman et al. (2020) and Ahmed et al. (2021) [46,47] also observed that an increase in the length of rigid vegetation such as trees positively affected energy reduction, like the present study's observation. Furthermore, two rows of seaweed had a 5% higher force reduction than a single row of seaweed, which also indicated that the linear superposition principle may not be valid for identifying force reduction due to rows, thus necessitating investigations over a large length of seaweed cultivation.

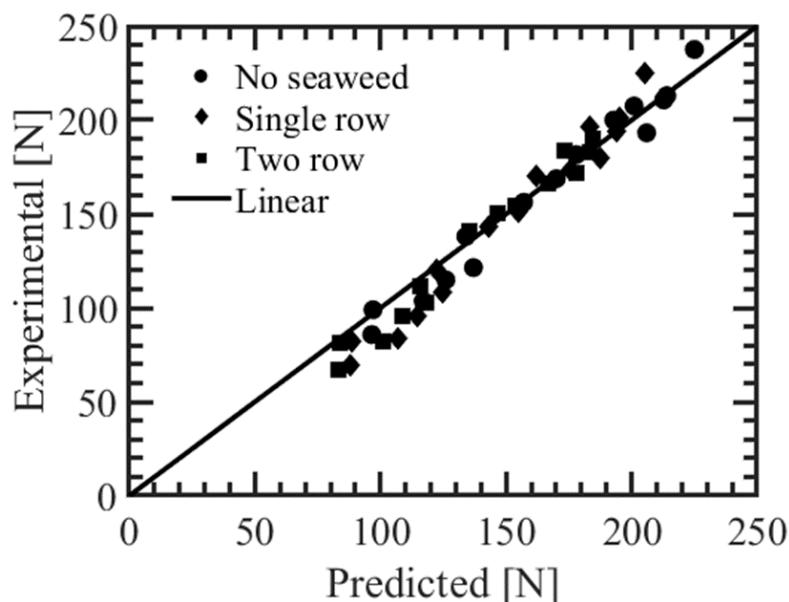
#### 4.5. Application of the Obtained Result

A prediction equation for the force is required to use the above results in the design of seashore buildings. Harish et al. (2021) suggested a method to estimate the forces on inland structures during quasi-steady conditions [28]. Since hydrostatic pressure exists during quasi-steady flow conditions, force prediction using bore depth at the structure's front and backside is possible using the hydrostatic approach [28]. The maximum force predicted

for the no seaweed condition is multiplied by the load reduction factors obtained from the single and two rows of seaweed. This is then compared with the experimental results to appreciate the prediction (Equation (2)). The procedure for predicting the forces for the no-seaweed case is summarized in Appendix A. The reduction factors for the single and two rows of seaweed are 9% and 14%, respectively.

Figure 13 presents a comparison of the predicted and measured force. It can be observed that the prediction yielded good results, since the data points pass through the plot diagonally, with an  $R^2$  value of 0.93. It should also be noted that the force prediction equation uses only  $h$  and  $u$  measured in the absence of any structure or obstruction. Zhang (2021) [48] presented in his work that tidal flats provide wave damping and equivalent protection standards for designing hybrid flood designs. The use of seaweed provides a better hybrid coastal protection (hard and soft technology) solution for modelling coastal protection because they can regulate the water temperature, provide a comforting biodiversity habitat, and provide climate change adaptation [3,49]. Design engineers can easily estimate the forces on an inland structure using free-flow hydrodynamics and seaweed information.

$$F_{max, seaweed} = Predic * Reduction\ factor \quad (2)$$



**Figure 13.** Comparison of predicted maximum force from Harish et al. (2021) with maximum experimental force using Equation (2) [28].

## 5. Conclusions and Limitations

The present experimental study tried to understand the effect of seaweed as an alternate solution to reducing the forces on inland structures. Seaweeds of different species were tied together, resembling flexible bushes (vegetation) at the coast. Despite the buoyancy and flexible nature of the seaweed, they played an essential role in reducing the forces on the inland structure. The seaweed was tested in an idealized condition, where the seaweed did not break due to the tensile nature of the species for the hydrodynamic conditions. The experiments were conducted on a 1:30 geometric scale. Based on the extensive experimental results, it was found that a single row of seaweed presented before the inland structure could reduce the force on the inland structure by 9%, whereas two rows could reduce the force by 14%. The presence of flexible vegetation in the form of seaweed could reduce the hydrodynamic strength of the incoming bore by altering the flow characteristics. The force equation for no-seaweed conditions was utilized to predict the forces with the seaweed by multiplying the reduction factor obtained from the present study. Furthermore, the

reduction percentage between one and two rows suggested that the linear superposition principle for the rows of seaweed was invalid, requiring further research with multiple rows, or more preferably, an investigation with the seaweed spread over the surface of the experimental flume is expected to provide more damping.

This study, which utilized seaweed as a source of energy reduction during extreme events, was successful in identifying seaweed as an alternate source to flow energy and momentum reduction; hence, the force. We achieved this by conducting experiments with a single row of seaweed, with each row weighing approximately 20 N in the lab. When scaled to the prototype using Fr scaling, the weight could be approximately 267 N/m (27 kg/m). The weights mentioned above are reasonable in the field [3]. Nevertheless, the spatial modelling still could not be replicated because seaweed is more spread in the actual field, unlike the rows of seaweed tested in this study. The scaling of the physical features and motion characteristics of seaweed has not been established until now, to our knowledge [22].

As mentioned above, the weight was predominantly used for the scaling, but other parameters such as the surface area or length should be further explored in the scaling for better results. More experimental runs should be carried out over a larger period to improve the results. Furthermore, it is not possible to use natural seaweed all the time and store them for a very long time. In this case, the use of a correctly modelled artificial plant that mimics real seaweed properties could mitigate this limitation.

The present study provides a pioneering idea for the coastal community to adopt seaweed as an alternate source of energy reduction under extreme conditions, as these seaweeds pose a good tensile strength [17]. Therefore, we encourage further modelling and research using seaweed spread over a large surface to potentially understand their influence as a source of energy dissipator under extreme wave conditions. Seaweed species are numerous and they have different shapes, which makes their scaling very challenging. Future work on scaling will provide more valuable information for the application of seaweed for coastal protection.

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**Conflicts of Interest:** The author declares no conflict of interest.

## Appendix A Prediction Equation

The prediction formula for estimating the quasi-static forces on the structure during the quasi-steady flow phase using bore height ( $h$ ), Froude number (Fr), and structure width/flume width ( $b/W$ ) are provided. In this study,  $b/W = 0.3$ . The force is estimated using the hydrostatic approach. The bore height at the structure front ( $h_f$ ) is obtained from the mass and momentum conservation equation, whereas the bore height and structure backside ( $h_r$ ) are obtained empirically.

Step 1: Obtain the bore height at the structure front iteratively by using Equation (A1):

$$\frac{h_f}{h} = \frac{2\text{Fr}^2 \left(1 - \frac{u_f}{u}\right)^2}{\frac{h_f}{h} - \frac{1}{\frac{h_f}{h}}} + 1 \quad (\text{A1})$$

The unknown  $u_f/u$  should be obtained using the following empirical equation:

$$\frac{u_f}{u} = -0.4359 \left( \frac{b}{W} \right) + 0.4366 \quad (\text{A2})$$

Step 2: obtain the bore height at the structure backside using the empirical equation (Equation (A2)):

$$\frac{h_r}{h_f} \left( 1 - \frac{u_f}{u} \right)^2 = -\frac{1}{120} \text{Fr}^2 + \frac{1}{9}; \frac{b}{W} > 0.2 \quad (\text{A3})$$

Step 3: Obtain the force (Equation (A4)):

$$F = 0.5 \rho g b \left( h_f^2 - h_r^2 \right) \quad (\text{A4})$$

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