

Abstract

High-Frequency Grating-Based Microelectromechanical Systems Actuator †

Inês Pires ^{1,2}, Inês S. Garcia ¹ , João Vieira ¹ , Zeev Zalevsky ³ , Carlos Calaza ¹ , Filipe S. Alves ¹ 
and Rosana A. Dias ^{1,*} 

¹ INL—International Iberian Nanotechnology Laboratory, 4715-330 Braga, Portugal; ines.pires@inl.int (I.P.); ines.garcia@inl.int (I.S.G.); joao.vieira@inl.int (J.V.); carlos.calaza@inl.int (C.C.); filipe.alves@inl.int (F.S.A.)

² Department of Industrial Electronics, University of Minho, 4800-058 Guimarães, Portugal

³ Institute for Nanotechnology and Advanced Materials, Bar-Ilan University, Ramat-Gan 52900, Israel; zeev.zalevsky@biu.ac.il

* Correspondence: rosana.dias@inl.int; Tel.: +351-253140112

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Abstract: A silicon mechanical-photonic wavelength converter, not based on absorption, has been recently proposed to address the need for all-silicon photodetectors in the infrared spectrum. Its implementation requires high-frequency modulation, from hundreds of kHz to 1 MHz, of a light beam over an area of a few hundred microns. Since the displacement amplitudes of tens of microns at these frequencies are unfeasible, a moving grate is proposed to locally modulate the light. The MEMS actuator, an array of 1 μm -wide 1 μm -spaced beams ($100 \times 100 \mu\text{m}^2$ area), achieved displacements of 70 nm at atmospheric pressure and 350 nm under low vacuum, with 10 Vpp actuation at 290 kHz (FOM displacement \times frequency² above previously reported works).

Keywords: high frequency; electrostatic; actuator

1. Introduction

Several silicon-based photonic detectors have been proposed but are unsuitable for wavelengths larger than 1 μm . A silicon mechanical-photonic wavelength converter (MPWC) was proposed [1] for an all-silicon infrared detector, not based on absorption, consisting of a Mach–Zehnder interferometer (Figure 1) in which the incident input light is modulated at a temporal frequency matched to the mechanic resonance of nanorods in the reference beam waveguide, and relying on the resonance of the nanorods due to optical gradient force. The challenge is to fabricate MEMS shutters/actuators with high-enough operation frequencies (and enough displacement amplitude) and silicon nanorod arrays with matching resonant frequencies, resulting in a 1–2 MHz feasible range. High-frequency MEMS resonators exist but with displacements limited to the picometer range [2,3].

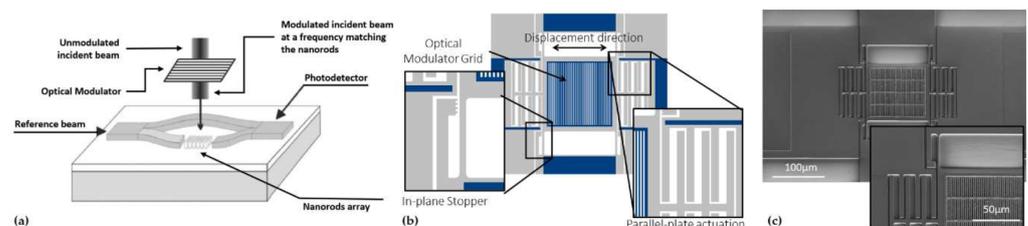


Figure 1. (a) Schematic representation of MPWC device with MEMS optical modulator, (b) MEMS optical modulator devices layout, and (c) SEM images of the fabricated devices.



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2. MEMS Optical Modulator

A MEMS optical modulator with a grate-shape or beam array is proposed to decrease the required displacement amplitude. For an array of $1\mu\text{m}$ -wide beams at a $2\mu\text{m}$ pitch, a displacement of $\pm 500\text{ nm}$ at a frequency of 0.5 kHz would be effective in locally modulating light at 1 MHz . The challenge lies in having micrometer displacements at such a high frequency with a movable structure with an area of $100 \times 100\ \mu\text{m}^2$ (given the trade-off between the resonance frequency and displacement amplitude typical of MEMS optical shutters). The design includes a $2\ \mu\text{m}$ pitch grating, four springs, and parallel-plate actuation electrodes on a $3\ \mu\text{m}$ SOI (Figure 1b, Table 1). The main micromachining steps are (a) device layer thinning from $5\ \mu\text{m}$ to $2\ \mu\text{m}$; (b) FS metal deposition; (c) FS and BS SiO_2 deposition; (d) metal grid patterning; (e) BS hard-mask patterning; (f) FS device lithography; (g) FS lithography and Si etching; (h) BS Si etch; and (i) HF vapor etching.

Table 1. Microstructure’s main parameters.

Parameters	Mass	Resonance Freq	Elasticity, k	Initial Gap	Damping Coeff.	No. Electrodes	Q-Factor, Q
Theoretical	81.2 pg	293.8 kHz	276.6 kN/m	2.03 μm	449 nN.s/m	12	333.8
Experimental	-	290.6 kHz	277.3 kN/m	2.03 μm	558 nN.s/m	12	271.9

3. Experimental Results and Discussion

The in-plane motion of the fabricated devices (Figure 1c) was measured on a Polytec MSA-500 at atmospheric pressure and in low vacuum (above -0.9 bar) using an acrylic vacuum chamber (Figure 2a). A natural frequency (F_n) near 290 kHz (lower than expected due to over-etch) and quality factors (Q) of 271 (atm) and 507 (in vacuum) were extracted from measurements (Figure 2b). At a higher vacuum ($\sim 10\text{ mbar}$), maximum displacement amplitudes of 378 nm at 293 kHz were achieved (Figure 2c), with positive F_n shifts (from nonlinear spring softening). Further work focuses on the redesign to meet the 0.5 MHz target and optical modulation validation.

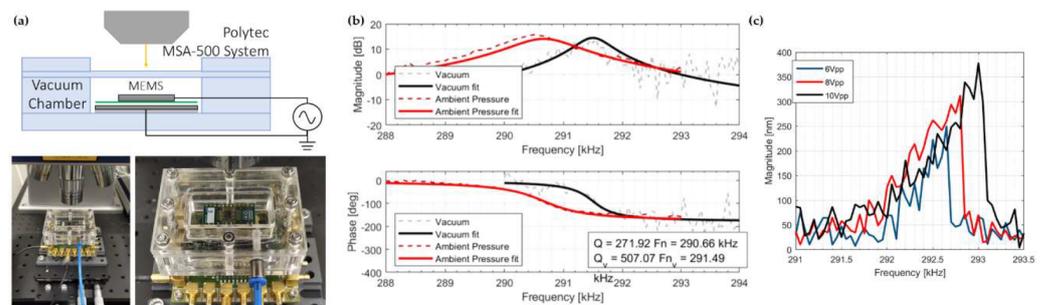


Figure 2. (a) Experimental setup, (b) bode plots at different pressures, and (c) magnitude displacement in low-pressure conditions for different amplitude actuation signals.

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