



# **The Global Carbon Footprint and How New Carbon Mineralization Technologies Can Be Used to Reduce CO<sub>2</sub> Emissions**

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Abstract: Carbon dioxide is a byproduct of our industrial society. It is released into the atmosphere, which has an adverse effect on the environment. Carbon dioxide management is necessary to limit the global average temperature increase to 1.5 degrees Celsius and mitigate the effects of climate change, as outlined in the Paris Agreement. To accomplish this objective realistically, the emissions gap must be closed by 2030. Additionally, 10–20 Gt of CO<sub>2</sub> per year must be removed from the atmosphere within the next century, necessitating large-scale carbon management strategies. The present procedures and technologies for CO<sub>2</sub> carbonation, including direct and indirect carbonation and certain industrial instances, have been explored in length. This paper highlights novel technologies to capture CO<sub>2</sub>, convert it to other valuable products, and permanently remove it from the atmosphere. Additionally, the constraints and difficulties associated with carbon mineralization have been discussed. These techniques may permanently remove the CO<sub>2</sub> emitted due to industrial society, which has an unfavorable influence on the environment, from the atmosphere. These technologies create solutions for both climate change and economic development.

**Keywords:** CO<sub>2</sub> emissions; CO<sub>2</sub> mineralization; carbon management; CO<sub>2</sub> technologies; CO<sub>2</sub> capture; greenhouse gas emission; sequestration; amine absorption

# 1. Introduction

 $CO_2$  emissions from industries that use fossil fuels can be a significant cause of  $CO_2$ accumulation in the atmosphere. More than 36 Gt of  $CO_2$  is emitted globally per year from fossil fuel combustion, cement production, and other industrial processes. Between 1975 and 2018, atmospheric  $CO_2$  levels dramatically increased from 250 ppm to 410 ppm [1,2]. Comparatively, this increase was 48% greater than records from the previous two decades; however, even these two decades demonstrated a 39% increase in  $CO_2$  levels, resulting in a 0.8  $^{\circ}$ C rise in the global surface temperature [2,3]. Continuous improvements in CO<sub>2</sub> mitigation stabilized the global annual CO<sub>2</sub> emissions between 2014 and 2017; however, data obtained between 2018 and 2019 suggested an annual 2.7% and 0.6% increase, respectively. These data predict  $CO_2$  emissions to increase further in the coming years [4]. In the absence of any climate sustainability policies, using 2000 as a baseline, a 25–90% increase of global greenhouse gases (GHG) emissions is expected by 2030. The growth in atmospheric  $CO_2$ -equivalent concentrations for this estimate is considered to be as much as 600–1550 ppm [5]. Different fuel sources contribute in different ways to the emission of CO<sub>2</sub>, though typically emissions are the result of energy and industrial production. The contributing fuels include gas, liquid (i.e., oil), solids (coal and biomass), flaring, and cement production [4,6]. The global energy-related CO<sub>2</sub> emissions increased in 2018 to 33.1 Gt of CO<sub>2</sub>, indicating a 1.7% rise in emissions. Eighty-five percent of the net increase was attributed to China, India, and the United States' emissions, mainly from using coal in power generation. For Asia, the emission levels surpassed 10 Gt of CO<sub>2</sub> [7]. Besides coal, other fossil fuels, including oil and gas, cause severe environmental concern [3]. CO2



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**Copyright:** © 2022 by the author. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). emissions are the main cause of climate change and increased global warming, creating many global issues. This concern has triggered the international research community to examine how best to reduce the concentration of  $CO_2$  in the atmosphere [3–7]. Various countries have considered and adopted different approaches. These approaches include:

- Improve and promote energy conservation and efficiency
- Use fuels with low carbon output, such as nuclear, hydrogen, natural gas, etc.
- Set up solar, hydropower, wind, and bioenergy as renewable energy sources (RES)
- Promote carbon capture and storage (CCS)
- Use and promote geoengineering approaches—for example, reforestation and afforestation [3].

To reduce  $CO_2$  emissions, a variety of mitigation strategies have been developed [1,4]. Among the technological alternatives for reducing the amount of  $CO_2$  emitted into the atmosphere are the following: (a) substituting less carbon-intensive fuels, such as natural gas, for coal; (b) increasing the use of RES or nuclear energy, both of which emit little or no net CO<sub>2</sub>; and (c) capturing and sequestering CO<sub>2</sub>. This article will examine the third option, CO<sub>2</sub> capture and sequestration (CCS), as a cost-effective strategy for mitigating climate destabilization caused by high levels of energy-related  $CO_2$  emissions [8]. Table 1 (below) compares the strategy, areas of application, advantages, and limitations for the reduction of  $CO_2$  emissions using different approaches. Some of the approaches deal with reducing the sources that  $CO_2$  comes from, such as using clean technologies or clean fuel. Others use demand-side management, for example, energy conservation for source emissions reduction. Depending upon the applicability, each approach has its advantages and limitations under specific conditions. Furthermore, a single strategy or approach is unlikely to be adequate enough to meet the Intergovernmental Panel on Climate Change (IPCC) goals for  $CO_2$  emissions [3]. These include the goal of a 50–85% reduction by 2050 as compared to levels in 2000. To maintain the rise in Earth's temperature below 1.5  $^\circ$ C, the IPCC has emphasized achieving the Paris Agreement climate targets by 2030. Clean hydrocarbon technologies (CHTs) can play a crucial role in meeting the demands of a circular carbon economy. The CHTs result in a minimal carbon footprint while converting hydrocarbons' energy into electricity, fuel, or other valuable mechanical work [9]. Newer conversion technologies are under development and are being researched for meeting climatic targets while realizing energy transitions, including direct hydrocarbon fuel cells, conversion of CO<sub>2</sub> into fuels, and underground gasification of hydrocarbons in combination with CCS to enable a cost-effective global circular carbon economy (CCE) [9].

Implementing the CCE recommended clean energy transitions can be accomplished by promoting the '4Rs' [10]. The first 'R' stands for reduce, which involves using energy efficiency and other alternative energy sources such as renewable or nuclear energy to reduce the amount of carbon entering the atmosphere. The second stands for reuse, which involves capturing and converting carbon into valuable industrial feedstock or increasing productivity by re-injecting carbon back into oil and gas reservoirs. The third stands for recycling, which consists of producing fertilizer, cement, or other valuable fuels through natural processes used for carbon transformation. Finally, the last 'R' stands for remove, which involves geological and chemical carbon removal from the system [11].

A stepwise closure of the carbon cycle through utilization and conversion of carbon is involved in the CCE, which significantly reduces carbon emissions. Many of the CHTs which are needed for CCE are still under development [9]. The integration of carbon capture and utilization (CCUS) into existing power plants and the increase in its implementation is expected to lower the electricity consumption costs to \$50/ton in 2050 [12]. However, the CCUS technology is still being researched for cost-reduction and developed for improved energy needs and capture efficiency. Based on the CO<sub>2</sub> capture and production process used in CCUS, its projects can be categorized as carbon positive, carbon-neutral, or carbon negative. To ensure sustainable utilization of hydrocarbons, the carbon-neutral and carbon-negative CCUS projects are required [9].

The direct capture of carbon dioxide from air using absorbent technologies or biomass combustions is performed in negative  $CO_2$  capture technologies, whose economic viability can be enhanced by producing high-value chemical products from captured  $CO_2$ . Gasification of hydrocarbons is another promising commercially demonstrated technology that involves producing high-value gaseous products from heavy low-value feedstock, thus improving the cost efficiency of the system. However, this technology is still being developed for underground implementation [13].

The solid oxide fuel cell (SOFC) system is considered the most efficient for producing clean power. Theoretically, an efficiency of 90% is recorded for SOFCs when combined with underground gasification or carbon capture systems. Thermal splitting technology is also used for clean hydrogen production, which competes with electrochemical, photo-chemical, and photo-biological routes utilizing solar energy for clean hydrogen production [14]. The latter provides the heat for the production process through concentrated solar radiation, and the combustion or fuel cells are used to generate electricity from the produced hydrogen. However, unlike nuclear, photo-biological, or photo-chemical routes, thermal splitting does not require the construction of new plants, as it can utilize the existing conventional facilities with modifications [9].

Mineralization of carbon, known alternatively as mineral carbonation or  $CO_2$  mineral sequestration, is an emerging approach used for carbon dioxide  $(CO_2)$  removal and storage. Although government agencies generally adopt a piecewise approach to  $CO_2$ management, long-term solutions typically involve the underground injection of  $CO_2$ . This solution, however, involves substantial risk and cost. An alternative to traditional geological sequestration is carbon mineralization, in which CO<sub>2</sub> is reacted to form carbonate minerals with metal cations such as magnesium, calcium, and iron. This storage is mainly performed in carbonate minerals, e.g., calcite or magnesite. The solid inorganic carbonates, which are thermodynamically more stable, are provided as an alternative by mineral carbonation to the underground storage of gaseous carbon dioxide [2]. Industrial or large-scale CO<sub>2</sub> utilization or recycling can result in large-scale production of carbon dioxide products that can be sold to different industries and thus help improve the economic viability of such processes. Calcium carbonate products can potentially be produced using Ca-based  $CO_2$  mineralization processes. These products can find application in industries requiring precipitated calcium carbonates, e.g., paper and cement, or landfill storage options. For example, cement clinkers and road construction aggregates require calcium carbonate [15]. Carbon dioxide products obtained from different technologies have two separate applications. These include low-end high-volume uses and high-end low-volume uses. However, these products should fulfill certain specifications and quality criteria of commercial value [16]. Diverse industrial applications are currently recorded for carbonate minerals, finding use in construction, paper and pulp, the pharmaceutical industry, and applications in the agricultural sector and refractory metals [17]. Potential markets have been explored for inorganic and organic carbonates obtained from carbon mineralization. These products include CaCO<sub>3</sub>, MgCO<sub>3</sub>, NaCO<sub>3</sub>, KCO<sub>3</sub>, polycarbonate, dimethyl/ethyl carbonates, etc. [15–17].

Strategy Application Area		Advantages	Limitations	
Enhance efficiency and conservation of energy	iency and of energyMainly used in industrial and commercial buildings.10% to 20% energy saving.		Extensive investment in installation.	
Use renewable energy	Solar (thermal), hydro, and wind power.	Uses local natural resources; no toxic gas emissions.	Intermittent energy generation limitations open spatial and temporal gaps between the availability of the energy and its consumption by the end-users.	
Increase clean fuels usage Substitute natural gas with coal. Emits 40–50% less na combustion efficiency. Natural gas has lower carbon dioxide. Has higher combustion efficiency.		More costly than conventional natural gas.		
Replace conventional         combustion through         Adaptation of clean coal       pressurized fluidized bed       Use of coa         technologies       combustor, integrated       er         gasification combined cycle       (IGCC), etc.		Use of coal with lower CO <sub>2</sub> emissions.	Significant investment is needed.	
Afforestation and reforestation	Applicability in all countries.	Approach to create natural and sustainable sinks of $CO_2$ .	Restricts the use of land for other applications.	
Nuclear power development	Nuclear fission was adopted mainly in France, Russia, the US, Japan, and China. It is still in the developmental phase.		Controversial to use. Hindered due to the nuclear accident at Fukushima in 2011.	
CCS (Carbon capture and storage)	CCS (Carbon capture and storage)Applicability to significant emission sources of CO2		Technologies of CCS are not commercially approved.	

Table 1	Comparing	the Carbon	<b>Dioxide Reduction</b>	Ap	proaches	[3,18].
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The construction industry offers the most suitable application opportunities for mineral carbonates concerning overall  $CO_2$  emission avoidance [17]. Crushed stone construction aggregates present the largest conventional carbonate market, with a 22.5 Gt global demand for carbonate materials such as limestone and dolomite [16].

The low-end high-volume uses of mineral carbonate products include liming agents in soil acidity treatment, silica, magnesium, and calcium carbonates for land reclamation and mine reclamation, etc. The high-end product applications call for strict specifications. Other applications include catalysts, chromatography, ceramics, pigments, pharmacy, photographic emulsions, etc. Moreover, other novel functional usages of calcium carbonate include plastics, rubber, paint, printing ink, weaving, toothpaste, make-up, and foodstuffs. Different polymorphic forms of CaCO<sub>3</sub> can improve paint dispersion, plastic reinforcement, and ink transparency. However, these applications require a high level of purity, which demands additional post-processing of these products [16].

Therefore, complementary strategies need to be developed to reduce  $CO_2$  emissions. As far as the different approaches are concerned, CCS can functionally reduce around 85–90% of the emission of  $CO_2$  from significant sources. This process involves technology such as cement kiln plants. These plants separate the captured  $CO_2$  from the gases into the sorbent. After being detached,  $CO_2$  can be reutilized or permanently stored. Different technologies concerning various processes, such as capture, separation, storage, transport, etc., are used for  $CO_2$  capturing. They all fall under the portfolio of CCS, which is discussed in the following section [3,18].

## 2. Current Industrial Technologies to Mitigate CO<sub>2</sub> Emissions

CCS is an auspicious method of reducing GHG emissions by capturing CO<sub>2</sub> at the power plant, transporting it to an injection site, and sequestering it in suitable formations for long-term storage. By installing a CCS unit at thermoelectric plants, approximately 85–95% of CO<sub>2</sub> processed in a capture plant can be captured efficiently. CO<sub>2</sub> capture technologies have been introduced, but they are costly. They typically make up 70–80% of the total cost of an entire CCS system, including various technological processes such as separate capture and storage, etc. [19,20]. Various R&D groups are working to develop a cheaper operating system with less energy penalties. The CCS process consists of three major components: capturing CO<sub>2</sub> for an extended period of time rather than releasing it into the atmosphere. Four primary CO<sub>2</sub> capture processes are linked to combustion processes, which are post-combustion, pre-combustion, oxy-fuel combustion, and chemical looping combustion, as illustrated in Table 2 [3].

Post-combustion  $CO_2$  capture is a widely used technique in the chemical processing industry [7]. Post-combustion capture technology can be retrofitted to existing significant point sources of carbon dioxide emissions in the atmosphere, such as fossil fuel power plants, cement manufacturing industries, or refineries [21]. It collects and captures carbon dioxide primarily using sorption and the sorption/desorption principle. Prior to combustion, post-combustion capture technology treats the exhaust stream to reduce the concentration of secondary species such as nitrogen oxide (NOx), sulfur oxide (SOx), water vapor, and particulate matter in the flue gas. Existing power plants also retrofit postcombustion technologies and can achieve a recovered rate of  $CO_2$  of around 800t/day at a small-scale plant [22]. However, this process of capturing  $CO_2$  has significant challenges associated with a large parasitic load. As the flue gas has low emissions of  $CO_2$  (around 4%) compared to coal-fired emissions (7–14%), it requires the energy penalty and cost for the capture unit to have a high concentration of  $CO_2$  (above 95.5%) for transport and storage [23,24]. According to the report, the U.S. National Energy Technology Laboratory elucidates that using post-combustion technology would increase the electricity production cost by 70%. Post-combustion technology in gas and coal-fired plants would increase the cost of producing electricity by 32% and 65%, respectively. Furthermore, it has been noted that 16 large-scale CCS projects are operating. Out of this amount, two of them are running on post-combustion technology [25].

Pre-combustion carbon capture is the process of sequestering carbon dioxide from fossil fuels or biomass fuels prior to the combustion process being completed. Typically, it is used in the gasification of coal and biomass and in natural gas power plants. A typical pre-combustion carbon capture system for a gasification power plant begins with the gasification (or partial oxidation) of fuel to produce synthesis gas (or syngas) that is enriched in carbon monoxide and hydrogen. After removing particulate matter with a cyclone separator, syngas is processed in a water–gas shift (WGS) reformer, where carbon monoxide reacts with steam to form carbon dioxide and hydrogen.

In pre-combustion, the fuel is treated before the combustion, such as when coal is pre-treated by a gasification process under a low oxygen level. This results in syngas compromised of CO and H<sub>2</sub> (Equation (1)). The syngas is free from pollutant gas that undergoes a gas-shift reaction. This results in more H<sub>2</sub>, and during the process, CO is oxidized to CO<sub>2</sub> (Equation (2)) [25]. As defined, natural gas is mainly methane (CH<sub>4</sub>), which can lead to H<sub>2</sub> and CO, or syngas (Equation (3)). In order to expand the amount of H<sub>2</sub>, a water-shift reaction can increase the concentration of H<sub>2</sub> (Equation (2)) [26].

$$gasificationC + H_2O \ gasification' CO + H_2$$
(1)

$$CO + H_2O$$
 water – gas shift  $H_2 + CO_2$  (2)

$$CH_4 + H_2O$$
 water - gas shift  $CO + 3H_2$  (3)

Regarding the application of low-carbon technology, the Energy Sector is undergoing a rapid technological transformation. Consequently, conventional gas turbines and internal combustion engines will probably need to be incorporated into systems utilizing biofuels and/or CCUS. Also, the European Union is moving quickly toward low-carbon technologies (such as energy efficiency, Smart Grids, renewables, and CCUS), as seen by the Energy Union Strategy [27]. A viable method for efficiently capturing carbon dioxide emissions generated by natural gas burning in the combustion chamber could be implementing improved combustion technology. When it comes to a combined cycle (CC) powered entirely by hydrogen, this is a new technology that is expected to hit the market in the coming years; one example is Vattenfall's Magnum natural gas-fired gas turbine combined cycle (GTCC) plant (440 MW) in the Netherlands, which will be converted from natural gas to hydrogen by Mitsubishi Hitachi Power Systems (MHPS) in 2025 [28]. From 2010 to 2018, the Fusina power station in Italy was powered by hydrogen (16 MW, estimated efficiency of 43 percent, GE10-1 type, single shaft, eleven compressor stages, three turbine stages) [28]. More than 75 GE gas turbines have accumulated more than 5 million working hours using hydrogen-based fuels. An A-Frame 6B unit at the Daesan petrochemical facility in Korea was constructed in 1997 and consistently runs with hydrogen concentrations between 85 and 97 percent [29]. It is an example of a hydrogen fleet leader. The HYFLEXPOWER is also moving towards this approach [30]. It uses hydrogen instead of natural gas ( $H_2$ -CC) (a CC powered by hydrogen). The substitution of natural gas with hydrogen ( $H_2$ -CC) reduces  $CO_2$  by 33% from natural gas combined cycle (NGCC), which consumes 450 to 150 kgCO<sub>2</sub>eq/MWh using hydrogen instead (Table 2) [31]. However, the gas turbines of the combined cycles must be somewhat updated, and the power plants require an infrastructure capable of providing hydrogen at a cost-effective rate. The production of hydrogen through power-to-gas technology represents a possibility. Because of this, the excess electricity from wind and solar PV is utilized to produce hydrogen via electrolyzers [31].

Instead of using air, oxygen is used in the combustion of the oxyfuel process. When pure oxygen is used in place of air for combustion, an oxy-fuel capture system produces a flue gas mixture primarily composed of  $CO_2$  and condensable water vapor, which can be separated and cleaned relatively easily during the compression process. This reduces the nitrogen production present in exhaust gas, hindering the separation process. Using pure oxygen is beneficial and results in the production of flue gases including  $CO_2$  and water. Additionally,  $SO_2$  and particulates are also produced. These can be removed via desulphurization and conventional electrostatic precipitator, respectively. Other gases produced also contain some  $CO_2$ , depending on the fuel used. These can be separated, transported, and stored [32]. This process is more feasible, but the large consumption of oxygen results in a high loss and an energy penalty of 7% [3]. Moreover, system corrosion problems can be intensified with the high concentration of SO<sub>2</sub>. Many developmental oxy-fuel projects are currently operating and under further development. Some subscale oxy units are also under development, as CS energy and Vattenfall proposed [33]. Burning coal under these conditions produces a flue gas rich in CO<sub>2</sub> (60–70 mol%) with substantial amounts of  $H_2O$  (20–25 mol%),  $O_2$  (3–4 mol%), and  $N_2$  (0–10 mol%), which varies according to coal rank and process design. Using a gas processing unit (GPU), this flue gas is enhanced to transport criteria [34–36]. The oxyfuel coal CCS system can reduce the impact of global warming. However, the energy demand of the air separation unit (ASU) and CO<sub>2</sub> compression unit in the oxyfuel CCS system necessitates an increase in fuel combustion per kilowatt-hour, hence increasing the chain-wide consequences. Due to the energy demand of the air separation unit, the use of oxyfuel combustion in a power plant reduces the facility's net efficiency (ASU). Due to the energy allocation for ASU, the natural gas oxyfuel combustion system is projected to have an efficiency loss of 11.3% [31]. By upgrading NGCC to oxy-NGCC, 450 can be lowered to 111 kgCO<sub>2</sub>eq/MWh (a reduction of 75%).

In chemical looping combustion (CLC), the metal oxide is used for combustion instead of pure oxygen, which is used in oxy-fuel combustion. The metal results from metal oxide, and fuel oxidation produces  $CO_2$  and water in this process. Metal is further oxidized and recycled; water (a by-product) is removed by condensation, while  $CO_2$  can be separated without consuming additional energy. Researchers found that using inert material can optimize the ability of metal oxide, but the inert material is specific for each metal oxide [33,37,38]. Moreover, the feasibility of this combustion in an experiment was studied, finding this technology to be promising for  $CO_2$  capture [39]. In comparison to IGCC using pre-combustion technology, the efficiency of chemical looping is 2.8% higher [40]. CLC has unrealized potential for use in power generation systems with zero  $CO_2$  emissions. CLC technology can compete with other pro-CCS technologies, such as oxy-fuel combustion, pre-combustion capture, and post-combustion capture, due to the inherent separation in CLC reactors, which drastically reduces the internal load of the plant. However, it is not yet mature enough to be implemented commercially [41]. The combination of CLC and gas turbines (GT)s can reduce a CC power plant's efficiency from 60% to around 40% [42]. To maintain the same level of energy output, more natural gas will need to be used. This type of plant's investment expenses is also anticipated to rise. It is estimated that the combustion chamber accounts for 11% of the total turbine expenditure [43] and that a pressurized fluidized bed combustor can cost between 2140 and 5700 \$/kW [44]. Based on these economic numbers, a comprehensive financial analysis of the required investment for a standard CC power plant and a CC power plant with CLC was undertaken. Studies using sensitivity analysis were performed on the carbon credit price to determine at what price the investment becomes attractive [31]. In addition, a comprehensive analysis of the life cycle of the two power plants was conducted to determine whether the loss of efficiency of the plant employing the chemical looping combustor impacts environmental performance. Fan et al. conducted an intriguing Life Cycle Assessment (LCA) on CLC plants coupled to CC fueled by natural gas. They evaluated the influence of four technical aspects on the ultimate impact: the type of oxygen carrier, its lifespan, the environmental impact caused by its production, and the thermodynamic performance of the technology. The environmental impact is highly dependent on the thermodynamic efficiency of the plant. Thus, it is preferable to use a CC with a pressurized CLC reactor instead of an atmospheric reactor, which can only be coupled to a steam turbine and has lower efficiency. In addition, the duration of the oxygen carrier has a significant impact on the plant's environmental impact. The oxygen carrier is concerned with attrition and reactivity losses. An NGCC plant emits around 450 kgCO2eq per megawatt-hour of power produced. Upgrading NGCC to CLC-NGCC can reduce emissions by 422 MtCO<sub>2</sub> (a reduction of 49%) [31].

The utilization of CO<sub>2</sub> in CCS is more feasible for high-concentration point sources (12–15%) such as power plants and cement industries, while in small-concentration sources of  $CO_2$  emissions such as those being removed from transportation, it is less likely to be feasible.  $CO_2$  capture from flow gas has been implemented in multiple natural gas processing industries and existing power plants. The ability of this strategy to be retrofitted to existing power plants and other industries makes it superior to prior combustion of  $CO_2$ . The  $CO_2$  content ranges from 3 to 15%, the lower end of this range (3–5%) being typical for gas-fired plants and the upper end (12-15%) for coal-fired plants. The CO<sub>2</sub> emissions from steel production typically amount to ~1.4 t-CO<sub>2</sub>/t-steel. Oil refineries accounted for  $\sim$ 3% of global emissions with a total of  $\sim$ 0.9 Gt-CO<sub>2</sub> emitted to the atmosphere in 2015 [45]. An IPCC analysis of large point sources identified 638 refineries emitting an average of  $1.25 \text{ Mt-CO}_2$ /year [46]. Total global CO<sub>2</sub> emissions from cement production amounted to ~2 Gt-CO<sub>2</sub> and yielded a flue gas with CO<sub>2</sub> of typically 14–33% with ~0.8 t-CO<sub>2</sub>/t-cement. Large fossil fuel power plants account for almost half of the total CO<sub>2</sub> emissions from fossil fuel combustion. These large point sources emit nearly 26% of the total global fossil fuel and industry emissions. Modern technologies, such as coal-fired, oil-fired, and combined cycle gas turbine (CCGT) power plants, are primarily responsible for most of the  $CO_2$  emissions from the power sector. Depending on the fossil fuel composition and lower heating value

(LHV),  $CO_2$  emissions are assessed. The greater the percentage of fuel, the greater the  $CO_2$  emissions. Considering lower heating value (LHV) and  $CO_2$  emission levels, the increasing proportion of H<sub>2</sub> gives fossil fuels better properties. Natural gas consists primarily of CH<sub>4</sub> and has nearly two times fewer emissions than hard and lignite coal as well as an almost two-times greater LHV. This fact is based on the composition of gas fuels, in which each methane molecule contains four hydrogen atoms for every carbon atom [47].

Other contemporary power generation methods, such as nuclear, RES, and hydrogenbased methods, are less likely to produce emissions [48]. Without carbon capture, a newly constructed CCGT power plant emits 350 kgCO<sub>2</sub>/MWh of CO<sub>2</sub>, which is the same as a gas-fired power plant. In the case of a coal-fired ultra-supercritical power plant, CO<sub>2</sub> emissions of up to 700 kgCO<sub>2</sub>/MWh are possible. CO<sub>2</sub> emissions range between 690 and 820 kgCO<sub>2</sub>/MWh, depending on the type of coal-fired critical power plant used [49]. Modern energy technology will continue to use fossil fuels until they are replaced by alternative technologies, such as renewable energies and emission-free power production. CO<sub>2</sub> capture is required to reduce greenhouse gases and protect the environment until these technologies can be replaced with those that do not emit CO<sub>2</sub>.

Table 2. Comparison of Four Capture Processes [3,27,31,50–54].

Capture Process	Application Sector	Advantages	Advantages Disadvantages		Carbon Footprint (kgCO <sub>2</sub> eq/MWh)
Post- combustion	Gas-fired and coal-fired plants	More mature technology; easily retrofit into existing plantsCapture efficiency can be affected by low CO2 concentration		0.50 [50]	-
Pre- combustion	Plant of coal gasification	High CO <sub>2</sub> concentration enhances efficiency; fully developed technology, commercially deployed, and can be retrofitted into existing plants	Heat transfer and efficiency decay problems associated with turbine fuel, such as using hydrogen-rich gas; high operational cost; and parasitic power requirement for sorbent regeneration	2.6–3.0 [51]	150 [31]
Oxy-fuel combustion	Coal-fired and gas-fired plants	A high concentration of CO <sub>2</sub> enhances absorption efficiency; mature air separation technologies are also available	Drop-in efficiency and energy penalty; costly O <sub>2</sub> production; and the problem of corrosion may arise	0.10–0.50 [52]	110–120 [27,31]
Chemical looping combustion	Coal-gasification plants	CO <sub>2</sub> , the main combustion product, remains unaltered with N <sub>2</sub> to avoid air separation	A process under development and inadequate for large scale operation	1.30 [53]	65–69 [31,54]

After  $CO_2$  is captured, it is compressed to create a supercritical fluid with properties intermediate between a gas and a liquid. It is then transported to a long-term storage location. When selecting  $CO_2$  storage sites, several factors are typically considered: the volume, purity, and rate of the  $CO_2$  stream; the proximity of the source and storage sites; the infrastructure for  $CO_2$  capture and delivery; the presence of groundwater resources; and the storage site's safety [55,56]. There are several options for  $CO_2$  storage, including injecting it into the ocean and allowing it to sink to the bottom or, more commonly, using geological formations as natural reservoirs, in which wells are drilled and  $CO_2$  is injected to depths greater than 1 km. Carbon sequestration is the long-term storage of carbon in soils, plants, oceans, and geologic formations which occurs spontaneously and due to anthropogenic activities. It refers to the storage of carbon, which can become  $CO_2$ . Due to climate change, carbon sequestration has been increasing in response to increased  $CO_2$  in the atmosphere. Changes in the land, forestry, and CCS techniques can increase carbon sequestration for the long-term storage of carbon [57]. Gas reservoirs and depleted oils, un-minable coal seams, deep saline formations, and enhanced oil recovery operation formations are the geological sinks of  $CO_2$ . Together with the help of different physical and mechanical trapping mechanisms, carbon sequestration can store thousands of GtC (gigatons of carbon) [58]. Geological storage is considered the most reliable way of storing a large quantity of  $CO_2$  to reduce the increasing global warming [59–61]. The site for geological storage of  $CO_2$  should be suitable, with appropriate porosity and a stable geological environment [61]. Table 3 shows the potential  $CO_2$  storage capacity of worldwide reservoirs for the sequestration sources as illustrated by Figure 1.

**Table 3.** The potential CO<sub>2</sub> storage capacity of worldwide reservoirs, reprinted with permission from Ref. [58]. Copyright 2022 Elsevier.

Sequestration Option	Worldwide Capacity (Gt C)		
Depleted Oil and Gas Reservoirs	100–1000		
Deep Saline Formations	100–10,000		
Ocean	1000–10,000+		
Terrestrial	10–100		
Coal Seams	10–1000		



**Figure 1.** Sequestration sources of CO<sub>2</sub> captured from power plants are a byproduct of industry or decarbonization plants.

# 3. Carbon Dioxide Mineralization

#### 3.1. Background

Although government agencies generally adopt a piecemeal approach to CO<sub>2</sub> management, long-term solutions typically involve the underground injection of CO<sub>2</sub>. This solution, however, involves substantial risk and cost. An alternative to traditional geological sequestration is carbon mineralization. In this process, CO<sub>2</sub> is reacted to form carbonate minerals with metal cations, such as magnesium, calcium, and iron. The mineralization of carbon, known alternatively as mineral carbonation or  $CO_2$  mineral sequestration, is an emerging approach used for  $CO_2$  removal and storage. This storage is mainly performed in the form of carbonate minerals, e.g., calcite or magnesite. The solid inorganic carbonates, which are thermodynamically more stable, are provided as an alternative by mineral carbonation to the underground storage of gaseous carbon dioxide [62]. The weathering of silicate materials and rocks is considered natural mineralization. Olivine, serpentine, and wollastonite are examples of silicate materials (Equations (4)–(8)). Rocks that are considered to have undergone the natural mineralization process should be rich in Ca and Mg. Peridotite rocks are one such example, and they form a significant component of Earth's upper mantle and basaltic lava [63]. Spontaneous and exothermic reactions take place at this level [15–17].

Walloastonite

$$CaSiO_3 + CO_2 \rightarrow CaCO_3 + SiO_2 \tag{4}$$

Olivine (forsterite)

$$Mg_2SiO_4 + 2CO_2 \rightarrow 2MgCO_3 + SiO_2$$
 (5)

Pyroxenes

$$CaMgSi_2O_6 + 2CO_2 \rightarrow CaMg(CO_3)_2 + 2SiO_2$$
(6)

Serpentine polytypes

$$Mg_{3}Si_{2}O_{5}(OH)_{4} + 3CO_{2} \rightarrow 3MgCO_{3} + 2SiO_{2} + 2H_{2}O$$

$$\tag{7}$$

Serpentine polytypes

$$Mg(OH)_2 + CO_2 \rightarrow MgCO_3 + H_2O$$
 (8)

Relatively rapid reactions are observed for high surface area to volume ratios with wollastonite, olivine, fibrous serpentines, and brucite. Asbestiform chrysotile is an example of a material with high surface area to volume ratios. The rate of reaction for Ca and Mg is identical to that of wollastonite. During the mineralization process, carbonates are formed by the reaction of CO<sub>2</sub> with Ca- and Mg-rich minerals. Examples of carbonates which are the product of this process include calcite (CaCO<sub>3</sub>), magnesite (MgCO<sub>3</sub>), dolomite  $(CaMg(CO_3)_2)$ , and often quartz (SiO<sub>2</sub>) [64]. The utilization or sale of carbon dioxide mineralization products to different industries can help improve the economic viability of the carbonation process. Industrial or large-scale CO2 mineralization can result in large-scale production of products, which can be reused or resold [15]. Calcium carbonate products can potentially be produced as a result of Ca-based CO<sub>2</sub> mineralization processes. These products have found applications in industries that require precipitated calcium carbonates. They are commonly used in the paper and cement industry or as landfill storage options [65]. Potential markets have been explored for inorganic and organic carbonates obtained from carbon mineralization. These products include CaCO<sub>3</sub>, MgCO<sub>3</sub>, NaCO<sub>3</sub>, KCO<sub>3</sub>, polycarbonate, and dimethyl/ethyl carbonates [15].

The carbonate products obtained from the mineral carbonation of  $CO_2$  have two separate applications. These include low-end high-volume uses and high-end low-volume uses. However, these products should fulfill certain specifications and quality criteria to be of commercial value. A low level of contaminants and a reasonable particle size are examples of such parameters [16]. Diverse industrial applications are currently recorded for carbonate minerals. They have been found to be useful in construction, paper, and pulp manufacturing, the pharmaceutical industry, the agricultural sector, and refractory metals. The construction industry offers the most suitable application opportunities for mineral carbonates and overall  $CO_2$  emission avoidance. The overview for these applications is shown in Figure 2, which also indicates the potential risk of  $CO_2$  release in some of these applications, often making them unsuitable [17].



Figure 2. Industrial applications of carbonate minerals.

At present, crushed stone construction aggregates present the largest conventional carbonate market. There is a 22.5 Gt global demand for carbonate materials such as limestone and dolomite [17,66]. However, this application is inexpensive due to the readily available crushed stone at just under 12 USD t<sup>-1</sup> [67]. The higher-purity requirements (>99%) related to other applications of carbonate products may add to the expenses during the mineral carbonation processes despite the market value for these product applications being around 550 USD t<sup>-1</sup> in the case of creating fillers for paints and paper. Therefore, if mineral carbonation products are to compete effectively with their natural counterparts, they should possess previously unestablished end uses and be superior in their physical or economic characteristics [17].

The low-end high-volume uses of mineral carbonate products include using liming agents in soil acidity treatment and silica and using magnesium and calcium carbonates for land and mine reclamation [68]. The high-end product applications call for strict specifications. The widely industrially applicable mono-disperse nanoparticles can be produced using mineral carbonation processes, such as silica in the amorphous phase, with potential use as filler or pozzolanic cement replacement material. Other applications include catalysts, chromatography, ceramics, pigments, pharmacy, and photographic emulsions. Moreover, other novel functional uses of calcium carbonate include plastics, rubber, paint, printing ink, weaving, toothpaste, make-up, and foodstuffs. Different polymorphic forms of CaCO<sub>3</sub> can improve paint dispersion, plastic reinforcement, and ink transparency. However, These applications necessitate a substantial amount of purity, which in turn demands additional post-processing in these products [16]. Mineralized calcium carbonate products can be majorly used as a replacement for limestone in the cement industry [65]. Carbonate ore mining can be avoided by using mineralized calcium carbonate as the lime precursor, eventually resulting in a potential net gain. The widespread calcium carbonate applications provide an extensive market for calcium carbonate mineralized from carbon dioxide fixation. For example, cement clinkers and road construction aggregates require calcium carbonate. Concrete carbonation has also been explored using flue gas CO<sub>2</sub>. Moreover, the usage of hydrated magnesium carbonate products as an acid-resistant building material has been tested. This product is obtained by flushing magnesium-rich brine with CO<sub>2</sub> gas. Despite the potential benefits, the possibility of carbon dioxide release from carbonated products requires attention [15].

 $CO_2$  capture and sequestration in underground geological storage (CCGS) are the most widely endorsed methods for carbon dioxide mitigation. The most apparent and significant alternative for these techniques is provided by carbon dioxide mineralization, which provides a CSS option for long-term storage of  $CO_2$  [69]. The geological storage reservoirs for CO<sub>2</sub> storage used in carbon dioxide sequestration were assessed in a U.S. geological survey. A significant concern is a potential for liquefied carbon dioxide gas leakage from fractures or permeable rock and the overlying aquifers. Leakage from subsequent reservoirs may result from the improper engineering and buoyancy of the residually trapped gas. This problem is not faced during carbon dioxide storage, as it uses stable and inert carbonate rock produced from mineral carbonation reactions [70]. These more stable carbonates tend not to release  $CO_2$  until they are dissolved in harsh acidic environments. Thus,  $CO_2$ mineralization makes carbon dioxide storage permanently verifiable and uses a cost-free monitoring process. The process can be economically attractive, producing industrially valuable carbonate, silicate, and rare earth metal products [63]. Moreover, the carbonation of industrial byproducts eliminates the need for a separate carbon capture step due to  $CO_2$ availability at the source, applying the process to the entire  $CO_2$ -containing flue gas or process gas.

In contrast, heavy energy penalties and significant losses of sorbent are faced when using amine absorption methods [69]. Mineral carbonation provides an opportunity to utilize and process toxic wastes to produce stabilized materials. These materials involve lower risks of leaching heavy metals. As a result, the products of  $CO_2$  mineralization have a greater potential for industrial application, such as in industrial work. Moreover, there are zero chances for  $CO_2$  leakage once it has been stored through mineral carbonation. This is because the carbon dioxide is bound for transformation into solid calcium or magnesium carbonates. This implies the possibility of retaining 100% of  $CO_2$  stored using mineral carbonation, even after 1000 years. This limits the requirement for disposal site monitoring [69].

#### 3.2. Currently Used Processes and Technologies

Two process routes are identified for  $CO_2$  mineralization, including direct carbonation, a kinetically slow one-step process involving the direct reaction of carbon dioxide with the mineral source (Figure 3). It further consists of the use of two general schemes. These are dry gas–solid carbonation and aqueous carbonation. To lower the processing costs for these reactions, the reactions must be explored at the particle–reactant interface for rate-limiting mechanisms [15].

The other process route is indirect carbonation, which comprises multiple kinetically faster steps. The two general reactions essentially included in this process are Ca or Mg reactive components' extraction and carbonate formation/precipitation reactions (Figure 4). The two reactions are kept separate due to the difference in their pH requirements. Twostage or pH swing routes are examples of indirect carbonation techniques [15]. The carbon mineralization methods aim to either ensure solid storage or combined mineral capture and storage. Solid storage involves carbon dioxide storage in the form of carbonate minerals. Ex situ carbon mineralization involves transporting the solid reactants to the  $CO_2$  capture site used to accomplish solid storage carbon mineralization. The reaction is then performed between these solid reactants and  $CO_2$ -rich fluid or gas [64]. Surficial carbon mineralization is based on mine tailings and other fine-grained solid reactants. These mine tailings, alkaline industrial wastes, or sedimentary formations are reacted with  $CO_2$ -bearing fluid or gas, as they have a rich proportion of reactive rock fragments and surface area [64]. Others performed in situ carbon mineralization, where two mediumscale experiments in basaltic rocks have been studied for this technology. Suitable rock formations with appropriate depths are selected to circulate  $CO_2$ -bearing fluids through them during this process [64]. Surficial or in situ carbon mineralization processes also allow the accomplishment of combined mineral capture and storage. However, the difference lies in using natural surface waters as an alternative for  $CO_2$ -enriched fluids. Additional technologies and energy input may be needed in the case of direct air capture systems. In in situ mineral capture and storage, a lower-cost potential is observed compared to surficial methods. However, in terms of permeability, reactive surface area, and reaction rate, the former faces uncertain feedbacks [64].



Carbonation Carbonated minerals CaCO<sub>3</sub> MgCO<sub>3</sub>

Figure 4. Principles of Indirect Carbonation.

Aside from mining, the generation of high-surface-area materials containing  $Fe^{2+}$ ,  $Mg^{2+}$ , and  $Ca^{2+}$  cations is gained through different industrial processes, and evaluation of industrial byproducts such as cement kiln dust, fly ash, iron, and steel slag has been done for potential mineral carbonation [71,72]. According to an estimation, using these byproducts could prevent 7.6 million metric tons of carbon dioxide. It is noted that a small number of total byproducts could restrict niche application usage. In contrast, carbonation could remediate hazardous waste to achieve emissions targets for the company [73]. Moreover, high concentrations of brines possess cations that could form carbonates. The injection of a  $CO_2$  mixture and brine in disposal wells could mineralize in-depth pore space and create scaling within the disposal well, leading to pressure management issues. The desalination process forming carbonates in the reaction could have many economic uses [70].

Constituents of fly ash contain MgO and CaO that help gradually absorb moisture for concrete and cement (Figure 5). This increases the product's life cycle and is widely used in the construction industry. Increased fly ash stability and reduced  $CO_2$  emissions can be achieved using fly ash in  $CO_2$  sequestration. However, the capacity of  $CO_2$  sequestration is lower in fly ash than in other industrial wastes due to the low content of carbon dioxide present. Regardless of its low capacity, the application of fly ash is still attracting attention as viable mineral carbonation of  $CO_2$  [74]. Large-scale industrial processes such as solid waste incineration, the paper and steel industry, and oil or coal shale fired power plants all use solid wastes to avoid drawbacks. This is because feedstock in primary earth minerals arises from mineral carbonation, which leads to the following advantages:

- Calcium or magnesium mineral matter is originated from waste materials in the form of CaO or Ca(OH)<sub>2</sub> without mining.
- They require less energy and pre-treatment conditions to increase carbonation yield, as they are chemically less stable than other minerals.
- The materials used are considered to be associated with the point source emission of carbon dioxide.
- The end product derived after sequestration can be re-used in other products. For example, precipitated carbonates of Ca and Mg, road base, and a range of other construction materials.
- Mineral transformation and pH neutralization can reclassify the hazardous waste.

Contrarily, the legislation issues, technological developments, chemical composition, and availability all limit industrial waste materials. Additionally, research is currently in progress to increase/maximize  $CO_2$  storage by improving gas humidity, gas flow rate, temperature, pressure, liquid ratio to solid, solid pretreatment, and particle size [16].

According to an IEA report, the fuel transformation sector and industry (e.g., cement and steel production) contribute 26% and 20% to the mitigation of CO<sub>2</sub>, respectively, through the application of CCS. There is less likelihood of generating an economically viable option by scaling down the CCS systems to distributed energy systems or industrial processes [75].



**Figure 5.** Innovative CCUM process: integration of carbon mineralization and waste utilization through accelerated carbonation [76].

Such an approach ensures the fixing of gaseous flue gas  $CO_2$  into solid carbonates with simultaneous neutralization of the wastewater to a pH value of 6–7. These fixed solid carbonates are upgraded in terms of physicochemical properties to find their applications as green cementitious materials. Moreover, the heavy metal immobilization and reduction in leaching are positively aided by the carbonation process due to the sorption of these metals (Pb, Zn, Cr, Cd, Cu, and Mo) into the carbonated products [77]. The durability of concrete can be effectively improved using the carbonation process, involving the conversion of soluble  $Ca(OH)_2$  into insoluble  $CaCO_3$  in concrete. Hence, the chemical and physical quality improvement of the carbonated and treated residues can result in their reuse on an industrial scale, e.g., in construction materials [78]. This ex situ carbonation further involves two different approaches:

#### 1. Direct Carbonation:

There are two ways to conduct direct carbonation: a dry gas–solid reaction or an aqueous reaction (gas–liquid–solid). The gas–solid carbonation is considered to be the simplest method and is represented by the following equation:

$$Ca/Mg-silicate_{(s)} + CO_{2(g)} \rightarrow (Ca/Mg)CO_{3(s)} + SiO_{2(s)}$$
(9)

However, the dry gas–solid reaction has decreased efficiency in large-scale carbon capture utilization in mineralization (CCUM) due to extremely slow reaction kinetics at ambient pressure and temperature. Feedstock pretreatment or possessing carbonation up to 500 °C can help slightly accelerate the reaction. However, these steps are energy-intensive, ultimately offsetting the environmental benefits of this technique and making it unviable on an industrial scale. The reaction kinetics are accelerated significantly in the aqueous carbonation due to the addition of water, which causes the mobility of ions. The schematic diagram for this direct aqueous carbonation is demonstrated in Figure 6, indicating  $CO_2$  fixation for construction material production [76]. This process can use industrial alkaline solid waste or wastewater for carbonation. In solid waste, the liquid phase is used, in which the waste is brought into direct contact with the flue gas. Waste separation follows this into carbonated solid wastes and liquid solution; the latter is heated with relatively hotter flue gas in a heat exchanger. A reactor is then used to recirculate it for the next carbonation [76].



Figure 6. Ex situ Direct Aqueous Carbonation (one-step carbonation), adapted from Pan et al. [76].

This process requires no extra heat to enhance the reaction kinetics, and its process chemistry can be classified into three spontaneous pathways:

• Leaching of Ca/Mg ions into solution from the alkaline solid matrix:

$$Ca/Mg-silicate_{(s)} + H_2O_{(l)} \to (Ca/Mg)CO_{3(s)} + SiO_{2(s)} + 2H^+_{(aq)}$$
(10)

• Dissolution of gaseous CO<sub>2</sub> into solution:

$$CO_{2(g)} + H_2O_{(l)} \to H_2CO_{3(aq)} \rightleftharpoons HCO_3^{-}{}_{(aq)} + H^{+}{}_{(aq)} \rightleftharpoons 2H^{+}{}_{(aq)} + CO_3^{-2}{}_{(aq)}$$
(11)

Ca/Mg carbonates' precipitation:

$$(Ca, Mg)^{2+}_{(aq)} + CO_3^{2-}_{(aq)} \to (Ca, Mg)CO_3_{(s)} \downarrow$$
 (12)

Aqueous carbonation has focused on previous studies exploring reaction kinetics modeling, process evaluation, optimization, multi-feedstock development, and novel reactor design [76].

2. Indirect Carbonation:

Figure 7 represents the schematic diagram for indirect carbonation, which can be divided into the following steps:

• Metal ions' extraction from alkaline solid wastes, e.g., calcium ions are extracted from the mineral crystals of CaSiO<sub>3</sub> using acetic acid.

$$CaSiO_{3(s)} + 2CH_{3}COOH_{(l)} \rightarrow Ca^{2+}_{(aq)} + 2CH_{3}COO^{-}_{(aq)} + H_{2}O_{(aq)} + SiO_{2(s)}$$
(13)



Figure 7. Ex situ indirect carbonation (multi-step carbonation), adapted from Pan et al. [76].

- Liquid–solid separation—A fiber membrane filters and separates the mother solution and extracted solids. The former is rich in Ca ions, while the latter can be Ca-depleted SiO2 particles.
- Filter solution carbonation—Precipitation occurs after filtering solution with a CO<sub>2</sub> source.

$$Ca^{2+}_{(aq)} + 2CH_3COO^{-}_{(aq)} + CO_{2(aq)} + H_2O_{(aq)} \to CaCO_{3(s)} \downarrow + 2CH_3COOH_{(l)}$$
(14)

The extraction stage may also use several other effective extractants, including CH<sub>3</sub>COONH<sub>4</sub>, NH<sub>4</sub>NO<sub>3</sub>, NH<sub>4</sub>SO<sub>4</sub>, NH<sub>4</sub>HSO<sub>4</sub>, etc. [76].

Pure carbonates such as  $CaCO_3$  and  $MgCO_3$  are produced as the end products due to the extraction and direct carbonation of oxides and hydroxides with the  $CO_2$ . The limiting factor for its large-scale application is the energy intensity of this process. However, ways to reduce energy and chemical costs have been indicated in various pieces of research [76].

## 3.2.1. Calera Process: Using Brines for Cement Manufacture

Calera has introduced a new approach to owning a demonstration plant in the USA. It is known as the gas-fired Moss Landing power plant. It aims to capture flue gas  $CO_2$  for at least two years with a 90% efficiency from a 10 MW power generator. Figure 8 defines the Calera process, which foresees the brine in the reactor containing alkaline earth metal ions [79]. In the Calera process, calcium carbonate is produced from flue gas and brines [16]. Calera is a process that captures  $CO_2$  from power plants and stores it in carbonaceous material. The Calera process converts gas to stable solids such as metastable calcium, magnesium carbonate, and bicarbonate minerals through a process called "mineralization via aqueous precipitation." Because the process requires a high pH, it is most economically feasible when power plants are located near sources of suitable brines extracted from geological formations and alternative sources of alkalinity and minerals. Calera cement and aggregate are similar to Portland cement (PC) and aggregate, but may vary by location due to the addition of trace components. After processing, the Calera process produces solid materials that can be used in a variety of construction applications. Calera also has a



proprietary high-efficiency electrochemical process called "alkalinity based on low energy" that produces sodium hydroxide and hydrochloric acid using only salt and electricity.

Figure 8. Schematic Diagram for Calera Process, adapted from Sanna et al. [16].

CO<sub>2</sub> and brine contact each other, whereas CO<sub>2</sub> dissolves in water to create carbonate and bicarbonate to decrease the pH of the solution. To produce the precipitates that contain carbonate, it is necessary to remove a proton from the solution. This makes the pH around 9–11 and shifts the equilibrium towards carbonate. The alkalinity increases the pH (hence carbonates precipitated), making cement manufacture feasible. Around 10–40% of the energy penalty is associated with the characteristics of power plants and the brine's availability of the process [79]. The brine's technical suitability and alkaline earth metal ions (such as calcium and magnesium) are more present in brines and offer potential feedstocks. Besides this, alkaline water for the Calera process and the need for seawater reduce this technology's broad application.

#### 3.2.2. SkyMine Process Via Direct Mineral Carbonation of Brines

Skymine is another process for CO<sub>2</sub> sequestration using brines. Skyonic Corporation is producing sodium carbonate and bicarbonate using the SkyMine<sup>TM</sup> technology, which also utilizes flue gas and brines [80] The SkyMine® Process is a patented, one-of-a-kind method for removing carbon dioxide from a gaseous waste stream, converting it to mineralized carbon, and producing valuable chemical byproducts (Figure 9). SkyMine<sup>®</sup> is a multicolumn system that reacts carbon dioxide from waste flue gas with sodium hydroxide to form sodium bicarbonate. Columns equipped with recirculation pumps, metering pumps, pH sensors, temperature sensors, pressure sensors, sample points (for fluid samples), test points (for gas samples), drip trays (for fluid distribution), flow indicators, and manual valves to control recirculation flow were used in the on-site field test unit. SkyMine® is a process that is capable of removing more than 90% of carbon dioxide from a flue gas stream. This project aims to capture 15% of the flue gas from Capitol Aggregates' cement plant. The process produces high-purity products that are readily marketable and in demand. Before construction, Skyonic had multiple off-take agreements to sell or distribute these products for use in various industries, including oil and gas, animal feed, municipal water treatment, and industrial cleaning. Skyonic anticipates that its products will be certified for use in the food and pharmaceutical industries due to their purity. It involves the absorption of CO<sub>2</sub> in caustic soda to produce carbonate or bicarbonate products [81,82]. Besides

having a 98% conversion rate using electricity or NaOH, the SkyMine process also claims to remove heavy metals such as mercury and clean NO<sub>2</sub> and SO<sub>x</sub> from flue gas [81]. The Skyonic Corporation, a joint venture that includes ConocoPhillips and BP, has launched the commercial capturing of CO<sub>2</sub> to remove 83,000 tCO<sub>2</sub> from the cement plant annually. The strength of this process lies in low-energy and low-cost mineralization plants with chemical inputs involved in the production of valued carbon-negative products, such as NaHCO<sub>3</sub> and HCl. However, this limits the broad application of the technology, as there is no significant market for bicarbonate and hydrochloric acid [16]. Heat exchangers cool down the flue gas from 300 °C to 30 °C. At the bottom, NaOH is absorbed to form the final product, followed by brine electrolysis [83–85]. The following reaction occurs in the carbonation chamber:

$$2NaOH + CO_2 \rightarrow Na_2CO_3 + H_2O \text{ and } Na_2CO_3 + H_2O + CO_2 \rightarrow 2NaHCO_3$$
 (15)





Potential applications of Products from the Skyonic and Calera process are highlighted in Table 4.

Carbonation Process	Amount of CO <sub>2</sub> Utilized	Value of Byproducts (\$ Per tCO <sub>2</sub> )	Energy Penalty for By-Product Process (%)	CO <sub>2</sub> Emissions Avoided	Products Market	Market Size (Billion \$ Per Year)
Skyonic	Cl <sub>2</sub> : 14 Mt per year; Na <sub>2</sub> CO <sub>3</sub> : 20 Mt per year; H <sub>2</sub> : 836 Mt per year	Na <sub>2</sub> CO <sub>3</sub> : ~300 \$ per t, H <sub>2</sub> : ~10 \$ per t, Cl <sub>2</sub> : 240 \$ per t	20	2.9 t per tCO <sub>2</sub> ; captured	Solvay process (Na <sub>2</sub> CO <sub>3</sub> or CaCO <sub>3</sub> )	3.4–9
Calera	Sand and aggregate market: 1500 Mt per year; cement: 24 Mt per year	Aggregate: 7 \$ per t, cement: 100 \$ per t	8–28	0.5 t per tCO <sub>2</sub> captured	CaCO <sub>3</sub> for cement, aggregates	21

Table 4. Use of Carbonation Products, adapted from Sanna et al. [16].

# 3.2.3. Production of Low-Carbon Concrete Products

 $CO_2$  mineralization in concrete during the batching phase [86–88], natural carbonation throughout the service life of a concrete structure and at the end of life [89], and natural carbonation during the service life of a concrete structure have all gained attention in the last decade, as they are viewed as options to lessen the impact of concrete on the environment. A group of academics attempted to calculate the global yearly  $CO_2$  fixed by natural carbonation using a model. According to the researchers, natural carbonation mitigates 43% of annual worldwide calculation emissions [88]. Additionally, other researchers studied the degree of carbonation in end-of-life concrete structures. They found that between 3.6% and 10% of process-based cement manufacturing emissions are reabsorbed [89].

The production of both PCs and carbonated calcium silicate-based cement (CSCs) consumes a lot of energy and produces a lot of  $CO_2$ . The raw grain must be dried, the limestone must be calcined, the oxide components must be reacted, and the cement clinker must be formed. This analysis will not consider the electrical energy required to crush and grind the raw materials, operate the clinkering process, comminute the clinker, and transport materials throughout the process. The changes in energy usage and CO<sub>2</sub> emissions are outlined below to demonstrate the advantages of CSC processing. The manufacturing of one tonne of PC clinker in existing cement plants requires 3.2 GJ of heat energy [90]. The thermal energy needed to produce one ton of PC clinker is around 1.757 GJ. The heat retained in clinker, heat losses via kiln dust and exit gases, and heat losses from radiation contribute to the gap between actual and theoretical heat requirements. Because the endothermic decomposition of calcium carbonate (calcination) consumes the most heat energy during pyroprocessing, the thermal energy of CSC clinker is expected to be lower than that of ordinary portland cement (OPC) clinker [87]. The vast concrete market offers an impactful sink for CO<sub>2</sub> emissions, using CO<sub>2</sub> mineralization reactions thermodynamically [91–95]. Sustainable concrete is made by capturing and mineralizing  $CO_2$  from air and water, producing a more robust cement-like material than traditional concrete and significantly reducing the carbon footprint. With this solution, buildings can be made with less energy, less cost, and less pollution.  $CO_2$  is used to replace limestone in concrete, meaning that the  $CO_2$  never escapes into the atmosphere. This technology can remove  $CO_2$ from the air while also using it to make carbon-negative concrete. This means that  $CO_2$  is reduced in the air producing a product that absorbs more  $CO_2$  than it emits (Figure 10). If this product is proved to be successful, it would be a significant step in addressing climate change [86–95].



**Industry Stack Flue Gas** 

**Figure 10.** Production of low-carbon CO<sub>2</sub> concrete products from coal combustion residues, flue gas CO<sub>2</sub>, and low-grade waste heat, adapted from Sant [96].

This process is yet to be developed and may produce various precast concrete/concrete masonry products. Hollow-core block (concrete masonry units) may be obtained as the initial product, fulfilling the ASTM C90 performance criteria. These criteria include:

- Compressive strength (>13.8 MPa)
- Density (determines weight classification)
- Water absorption (<320 kg/m<sup>3</sup>)
- Physical appearance/dimensional tolerances
- Preliminary lifecycle analysis (LCA): ~65% CO<sub>2</sub> emissions reduction relative to conventional CMU

The project aims to utilize  $CO_2$  in flue gas and coal combustion residues (CCRs) to synthesize concrete by using the  $CO_2$  mineralization process and accelerating its pace of development. This product is designed to provide a functional replacement for traditional concrete. This project is to be created, fabricated, and optimized as a field-scale  $CO_2$ processing (carbonation) system by the University of California, Los Angeles (UCLA) with the support of Susteon Inc. [96].

Additionally, Solidia Cement, patented in 2016 [86], is a non-hydraulic binder made from the same raw ingredients as OPC but with a lower proportion of CaCO<sub>3</sub> and a kiln temperature of roughly 1200 °C, resulting in a 30% reduction in CO<sub>2</sub> emissions [86,87]. This binder's overall C/S molar ratio is 1, and it is primarily made up of wollastonite/ pseudowollastonite, with minor amounts of rankinite (13%wt) belite (3%wt) [97]. This mixture of calcium silicate phases has the potential to harden through a carbonation process; therefore, no water is required for the reaction to take place [87]. The granulated raw material is fed into a natural gas-fired rotary kiln to make this cement. The calcium silicate compositions produced in the rotary kiln are "clinker," or small granules with diameters ranging from 1 to 4 mm. After that, the clinker is processed into a powder with a mean particle size of around 12 mm. This substance is combined with aggregates, sand, and water to make concrete. When the concrete mixture is subjected to a high-concentration gaseous CO<sub>2</sub> atmosphere (60–90%) [98], the binder phases react, and CaCO<sub>3</sub> and SiO<sub>2</sub> are produced. Solidia Cement is a non-hydraulic binder made from the same PC raw material in existing cement kilns. The main distinction is that the Solidia binder is made with less limestone and lower kiln temperatures. As a result,  $CO_2$  emissions from cement manufacture are lowered (30% reduction). The binder, aggregates, sand, and water react with  $CO_2$  to form a durable matrix of the Solidia concrete solution. The curing process collects up to 300 kg of  $CO_2$  per ton of cement used. Compared to traditional cement and concrete products, Solidia cement and concrete products minimize  $CO_2$  emissions by 70% [87].

#### 3.2.4. Ion Exchange Implementation on CO<sub>2</sub>-Rich Streams

The critical challenge to the previous alkaline addition processes is maintaining alkalinity during carbonation. The Calera, Solidia and SkyMine<sup>TM</sup> process relying on the consumption of hydroxides or electrolysis is costly. Ion exchange processes provide an alternative method to adding stoichiometric inorganic bases (e.g., NaOH) to induce alkalinity for the consequent precipitation of CaCO<sub>3</sub>. This process proposes using regenerable ion exchange materials to increase the pH of CO<sub>2</sub>-rich solutions via ion exchange, providing alkalinity required for CO<sub>2</sub>-mineralization [99–101]. CO<sub>2</sub> exchanges protons with sodium from ion exchange materials to dissolve the CO<sub>2</sub> into bicarbonates that are then precipitated as carbonates. The reactions are carried out in columns filled with porous, solid media called zeolite [102]. In principle, ions exchange between an electrolyte solution and similarly charged ions immobilized in an ion exchange material through a stoichiometric reversible ion-exchange reaction (Figure 11). The goal is to develop a process cycle that can carbonate Ca in produced water while regenerating the ion exchange resins. However, the technical challenge is to regenerate the zeolite without using a base and using low energy-consumption steps [99,100].



Figure 11. Schematic of the ion exchange process.

Additionally,  $CO_2$  is produced during wastewater treatment on a considerably lesser scale than in anthropogenic activities such as agriculture, industry, or those that utilize fossil fuels, with an emission of 4.13 kg  $CO_2$  per m<sup>3</sup> of treated water [103]. In this way, this research aimed to absorb  $CO_2$  from the ambient air during the mineralization of municipal wastewater using a moisture-driven  $CO_2$  sorbent [104–107]. To complete the

 $CO_2$  capture–release cycle, a successful sorbent for direct air capture (DAC) must (1) have fast reaction kinetics, (2) be low in cost, and (3) be able to regenerate with a low-energy barrier. Because they must overcome a significant energy barrier to regenerate, most  $CO_2$ sorbents failed in the third category [108]. Temperature Swing Absorbents (TSV) or Pressure Swing Absorbents (PSV) such as hydroxides, oxides, or alkaline salts, for example, may easily scrub  $CO_2$  from the air. However, calcination necessitates heating the sorbent to high temperatures. It takes a lot of energy to overcome the binding energy and compensate for the heat losses that occur during the heating of bulk materials, and heat losses are difficult to avoid [109]. A new energy-efficient sorbent process captures  $CO_2$  by simply adjusting the amount of water on it. When the environment is dry, the sorbent binds  $CO_2$  from the air, and when the environment is wet, it desorbs  $CO_2$ . It uses a tenth of the energy of other  $CO_2$  sorbents on the market [108].

#### 3.2.5. Electrochemical Ocean Mineralization

Brine production/disposal and a huge carbon footprint resulting from energy usage are two major negative environmental implications of seawater desalination. Sequential  $CO_2$  mineralization appears to provide a possible solution to both problems. The impacts of critical reaction parameters in this method, such as extra agitation of the reactant phases, electrolytes, and the rate of  $CO_2$  microbubble injection, are reported in this study [110].

The electrochemical carbon dioxide removal process takes advantage of the natural carbonate cycle in the ocean to sequester  $CO_2$  on a large scale. Because  $CO_2$  is the dominant acid in the ocean system, increased pH results from CO<sub>2</sub> removal via photosynthesis or de-gassing; consequently, there is typically a nearly one-to-one correspondence between CO<sub>2</sub> reduction, alkalinity generation, and limestone precipitation in that sequential order. However, in the case of electrolysis, hydroxyl ions are generated directly from the electrolysis of water, so no  $CO_2$  is released; instead, a locally higher pH promotes  $CO_2$  dissolution and ionization to carbonate anions, which replace the precipitated-out carbonate anions. This process uses membranes composed of mechanically and chemically stable metallic materials [111]. Periodically, the membrane surface can be cleaned with either an acid solution or a knife to remove or dissolve any carbonates precipitated on the pores. Additionally, reversing the applied potential can be used to anodically generate O<sub>2</sub> and H<sup>+</sup> near the membrane surface, detaching or dissolving any carbonates deposited [112]. A solids collector system similar to that found in a rotary drum filter can be integrated into the membrane, and the precipitated solids will be discarded into the oceans (Figure 12). Electrolysis of OH<sup>-</sup> at the site of the Ca<sup>2+</sup> combination is advantageous, as it reduces the diffusion barrier for precipitation, and the presence of a substrate in the form of a membrane surface promotes nucleation. Thus, localized pH changes on membrane surfaces create favorable thermodynamic and kinetic conditions for CO<sub>2</sub> mineralization in a more sophisticated process.

Desalination plant energy consumption should be reduced from both an environmental and an economic standpoint [113–115]. Desalination, as with any other human-made activity, has had several environmental consequences. The major repercussions include the discharge of chemical-laden brine into the environment and the emission of GHGs into the atmosphere [115]. Combining saltwater desalination with salinity gradient-based power generation technologies (such as pressure retarded osmosis (PRO) [116,117]) generates pressure and thus energy by utilizing the salinity difference between a relatively fresh impaired water supply and seawater. The PRO system has a lot of benefits. When compared to an optimized reverse osmosis (RO) system (i.e., a RO with an energy recovery device), energy production from PRO reduces RO energy usage even more. Another significant benefit of this system is that the brine produced during the RO process is diluted back to seawater concentration, reducing the negative environmental impact of seawater RO brine disposal on marine ecology and habitats.



**Figure 12.** A schematic of localized OH<sup>-</sup> generation on membrane surfaces using the electrochemical process to induce carbonate precipitation.

Furthermore, the impaired water and RO product water are in different circuits, ensuring that the inadequate water does not contact the drinking water. Finally, because the draw solution in the RO-PRO system is an open loop, pollutants are unlikely to accumulate [117]. Electrodialysis is projected to reduce energy consumption and brine salinity [118,119]. Nonetheless, contemporary desalination facilities use much non-renewable energy, and the CO<sub>2</sub> produced by such sources contributes significantly to global climate change [120]. A desalination plant requires energy for seawater input, pretreatment, demineralization, brine disposal, and outfall [115]. The least energy-intensive demineralization process is RO, while the demineralization step consumes the most energy [121]. Raluy et al. [122] compared the number of contaminants produced by multi-stage flash (MSF), multiple-effect distillation (MED), and RO demineralization procedures. RO needs 4 kWh of energy and generates 1.78 kg of CO<sub>2</sub> to produce 1 m<sup>3</sup> of demineralized water. The energy consumption of seawater RO, according to Panagopoulos, is 3–9 kWh/m<sup>3</sup> water [123]. According to Jia et al., RO uses 5 kWh to produce 1 m<sup>3</sup> water [28]. New energy recovery systems have lowered the energy need for RO compared to conventional demineralization processes [124]. Assuming 100% RO technology and removing other energy-intensive procedures, the CO<sub>2</sub> emission still exceeds 170 k ton/day based on the global desalination capacity of 95.37 million m<sup>3</sup>/day [125]. Seawater desalination plants, fortunately, are frequently located near fossil power plants, simplifying the energy supply chain [126]. This shows that desalination brine might be used to mineralize CO<sub>2</sub>, effectively accomplishing two goals simultaneously.

#### 3.3. Constraints of CO<sub>2</sub> Mineralization Process for Global Scale Application

Mineral carbonation offers the safest and most stable and permanent method of  $CO_2$  storage [16–18,61,68,76]. This stability is confirmed by the carbon distribution and storage of carbonates such as limestone (CaCO<sub>3</sub>) in the Earth's lithosphere, as shown in Figure 13. A large  $CO_2$  sequestration potential is provided by the resources of this process, up to 410,000 Gt C [16].



**Figure 13.** Global carbon reservoirs (GtC) and their net fluxes (GtC per year), adapted from Sanna et al. [16].

Mineral carbonation is still considered an immature technology in terms of technology, market acceptance, economics, and impact assessments [63]. The mineralization processes should be introduced with technical solutions which fulfill the relevant engineering requirements and are in accordance with the public acceptance criteria [50,127,128]. These areas need to be adequately addressed if  $CO_2$  mineralization is established globally. Table 5 summarizes precursor-based barriers faced in mineral carbonation approaches. Below are the significant constraints of this process, which act as a hindrance to its global application [15–17,127]. Three key factors are the primary cause of obstruction in the carbonation process:

- Competitive reactions—Refers to hydration tendency of solids versus carbonates. Highly hydratable Ca-rich solids demonstrate poor carbonation potential compared to fully hydrated Ca-rich solids, e.g., Ca(OH)<sub>2</sub>.
- Formation of surface-passivating films—Refers to the formation of dense calcite films (physical barriers) on carbonating surfaces, causing hindrance to the reactant solid in contacting CO<sub>2</sub>. For example, this factor is attributed to the fractional carbonation (<10%) of a highly hydratable solid (CaO is attributed to this factor).
- Presence of water—Refers to the inhibition of carbonation due to condensation of water within the micro or mesoporous solid pores. This causes the hindering of the transport of vapor-phase CO<sub>2</sub> into the microstructure. This is observed during carbonation with precast sections.

The potential energy penalty is used to drive the mineral carbonation process [67]. This energy is needed for three aspects, which differ in their importance corresponding to the metal oxides' source:

- Preparation and activation of the solid reactants (mining, transport, and grinding included)
- Processing, recycling, and possible losses of additives and catalysts; and
- Disposal of carbonates and byproducts

Currently, additional energy consumption is observed along with additional  $CO_2$  production compared to other storage options. Studies suggest that 60–180% more energy is required for a full CCS system with mineral carbonation than those power plants without CCS [62]. Carbonation processing limitations due to the complexity of carbonation processing are associated with two key factors:

- Requirement for alkaline precursors, which are neutralized progressively after contact with CO<sub>2</sub>. This is problematic due to high-temperature activation in the production of alkaline precursors and reactants [50,99–101,127].
- Sustained elevated pH levels in the solution are needed to promote carbonate precipitation. This is because increasing pH diminishes CaCO<sub>3</sub> solubility. Moreover, acidity is induced by CO<sub>2</sub>'s dissolution in water, thus requiring alkaline buffering to sustain the precipitation of carbonates [76,100].

**Table 5.** Summary of precursor-based barriers faced in mineral carbonation approaches. Adapted with permission from Ref. [127]. Copyright 2022 The National Academies Press.

Input	Key Barriers			
Mature OPC-based concrete	It takes years for carbonation to occur under mass transfer (diffusion) control at ambient conditions.			
Fresh OPC-based concrete	Slow reaction rates, the limited concentration of carbon dioxide in the slurry, and presence of moisture, hindering carbonation.			
Low-rank calcium silicates	Requires a high concentration of CO <sub>2</sub> to hasten the reaction kinetics sufficiently.			
Hydrated lime	Requires the maintenance of slightly above-ambient temperature conditions.			
Industrial wastes	Heterogeneity accounts for broad variations in reaction kinetics with substantially lower CO <sub>2</sub> uptake.			

The current need is the development of chemical additives, which may affect both kinetic and thermodynamic reaction controls, resulting in enhancing carbonation rates [58]. The mineral carbonation process poses serious environmental concerns associated with large-scale mining, ore preparation, and waste product disposal. These processes may contribute directly to potential soil, water, and air pollution. These environmental impacts are the major hindrance in achieving public acceptance of the mineralization process [62]. Relatively little research is available on CO<sub>2</sub> mineralization, its economic viability, and feasibility [128]. The different process designs for mineral carbonation have great potential for improvement and development, as stated in various literature [16–18,50,99–101,127]. Further research can be conducted to evaluate, understand, and improve the necessity of heat activation for various mineral resources used for this method. The potential of mineral carbonation products to be used as industrial feedstock can be evaluated for residual silica (or silicate) and Mg/Ca carbonate. Thus, the economic competitiveness of CO<sub>2</sub> mineralization can be explored by working towards the improvement of its product value [63]. Moreover, the concerns regarding the large-scale energy requirements, scale mining, and associated environmental concerns need to be preemptively dealt with to ensure public acceptance of this process. Therefore, research needs to be done to evaluate the natural mineral reserves needed for this process. Additionally, it would help to examine the optimization of costs, power generation, mining, product disposal, and their transport in accordance with a site-specific manner [63]. Below, some of the potential future scopes for the future of this industry are outlined:

- 1. To tackle future challenges, an efficient and well-designed process plant that fulfills the efficient mass transfer among phases such as gas–liquid–solid (high fixation of CO<sub>2</sub> with low energy consumption) is required [3,7,15–17,21,36].
- 2. The integration of mineral carbonation should be processed with waste treatments to reduce the total cost, such as reducing SO<sub>2</sub>, CO<sub>2</sub>, fly ash stabilization, flue gas, and alkaline wastewater neutralization [76,80,100,101,127].
- 3. Prior to the CO<sub>2</sub> mineral carbonation, valued elements should be extracted and recovered. These might include aluminum, iron, or sodium [67].
- 4. In the engineering industry, carbonated fly ash should be given more attention [17,67,92].

5. Systematic analysis should consider the operation and capital costs for the profit gain from CO<sub>2</sub> reduction and waste utilization [74].

## 4. Conclusions

The societal consequences of rising carbon dioxide levels are grave, and actions to mitigate them are critical to maintaining our standard of living. To summarize, this work's analysis highlights the massive (but not insurmountable) scale of the  $CO_2$  problem. The scope of this work precludes an in-depth examination of the mechanisms for CO<sub>2</sub> management. It began with an overview of the global greenhouse gas crisis, followed by a discussion of the current industrial technologies deployed to address the crisis. To reduce the emission of  $CO_2$ , various countries have considered and adopted different approaches. These have included promoting energy conservation, using low-carbon fuels, using renewable energy, promoting CSS, and promoting geoengineering approaches. The industrial technologies to mitigate carbon dioxide emissions have been described throughout this paper. They include carbon capture, sequestration, and amine absorption techniques. CCS is the most widely used approach; however, CCS is expensive and fraught with risk. The mineralization concept was then introduced as an alternate method for permanently carbonating  $CO_2$  into valuable goods. This paper also represented the significance of carbon dioxide mineralization as an effective alternative for carbon capture and sequestration techniques. The present procedures and technologies for CO<sub>2</sub> carbonation, including direct and indirect carbonation and certain industrial instances, were explored in length. Additionally, the constraints and difficulties associated with carbon mineralization were discussed. This technology is faced with certain constraints regarding its global-scale application. This process's potential scope is diverse, though it mainly focuses on utilizing industrial wastes and other alkalinity sources as feedstock for the carbonation process.

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## References

- Pachauri, R.K.; Allen, M.R.; Barros, V.R.; Broome, J.; Cramer, W.; Christ, R.; Church, J.A.; Clarke, L.; Dahe, Q.; Dasgupta, P. Climate Change 2014: Synthesis Report. Contribution of Working Groups I, II and III to the Fifth Assessment Report of the Intergovernmental Panel on Climate Change; IPCC: Geneva, Switzerland, 2014.
- Metz, B.; Davidson, O.; De Coninck, H.; Loos, M.; Meyer, L. IPCC Special Report on Carbon Dioxide Capture and Storage; Intergovernmental Panel on Climate Change: Geneva, Switzerland, 2005.
- Leung, D.Y.C.; Caramanna, G.; Maroto-Valer, M.M. An Overview of Current Status of Carbon Dioxide Capture and Storage Technologies. *Renew. Sustain. Energy Rev.* 2014, 39, 426–443. [CrossRef]
- 4. Ritchie, H.; Roser, M. CO<sub>2</sub> and Greenhouse Gas Emissions. *Our World Data* **2020**, 1.
- 5. Nakicenovic, N.; Alcamo, J.; Davis, G.; de Vries, B.; Fenhann, J.; Gaffin, S.; Gregory, K.; Grubler, A.; Jung, T.Y.; Kram, T. Special *Report on Emissions Scenarios*; Lawrence Berkeley National Laboratory: Berkeley, CA, USA, 2000.
- Yang, H.; Xu, Z.; Fan, M.; Gupta, R.; Slimane, R.B.; Bland, A.E.; Wright, I. Progress in Carbon Dioxide Separation and Capture: A Review. J. Environ. Sci. 2008, 20, 14–27. [CrossRef]
- 7. IEA. CO2 Status Report; IEA International Energy Agency: Paris, France, 2019.
- 8. Mach, K.; Mastrandrea, M. *Climate Change 2014: Impacts, Adaptation, and Vulnerability*; Cambridge University Press: Cambridge, UK; New York, NY, USA, 2014; Volume 1.
- Alshammari, Y.M. Achieving Climate Targets via the Circular Carbon Economy: The Case of Saudi Arabia. C—J. Carbon Res. 2020, 6, 54. [CrossRef]
- 10. Mansouri, N.Y.; Alma, A.; Al-Saud, N.T.; Alshalan, M.S.; Benlahrech, M.; Kobayashi, Y.; Sedaou, R.; Toyoda, M.; Yaroshenko, L. A carbon management system of innovation: Towards a circular carbon economy. *G20 Insights* **2020**, *10*, 12.
- 11. Alatawi, H.; Darandary, A. *The Saudi Move into Hydrogen: A Paradigm Shift;* Instant Insight; King Abdullah Petroleum Studies and Research Center (KAPSARC): Riyadh, Saudi Arabia, 2020.
- 12. Herzog, H.J. What Future for Carbon Capture and Sequestration? Environ. Sci. Technol. 2001, 35, 148A–153A. [CrossRef]

- 13. Alshammari, Y.M.; Hellgardt, K. A New HYSYS Model for Underground Gasification of Hydrocarbons under Hydrothermal Conditions. *Int. J. Hydrogen Energy* **2014**, *39*, 12648–12656. [CrossRef]
- 14. Romanov, V.; Soong, Y.; Carney, C.; Rush, G.E.; Nielsen, B.; O'Connor, W. Mineralization of Carbon Dioxide: A Literature Review. *ChemBioEng Rev.* 2015, 2, 231–256. [CrossRef]
- 15. Wang, F.; Deng, S.; Zhang, H.; Wang, J.; Zhao, J.; Miao, H.; Yan, J. A comprehensive review on high-temperature fuel cells with carbon capture. *Appl. Energy* **2020**, *275*, 115342. [CrossRef]
- Sanna, A.; Uibu, M.; Caramanna, G.; Kuusik, R.; Maroto-Valer, M.M. A Review of Mineral Carbonation Technologies to Sequester CO<sub>2</sub>. Chem. Soc. Rev. 2014, 43, 8049–8080. [CrossRef]
- 17. Woodall, C.M.; McQueen, N.; Pilorgé, H.; Wilcox, J. Utilization of Mineral Carbonation Products: Current State and Potential. *Greenh. Gases Sci. Technol.* **2019**, *9*, 1096–1113. [CrossRef]
- De Oliveira Costa Souza Rosa, C.; da Silva Christo, E.; Costa, K.A.; dos Santos, L. Assessing Complementarity and Optimising the Combination of Intermittent Renewable Energy Sources Using Ground Measurements. J. Clean. Prod. 2020, 258, 120946. [CrossRef]
- 19. Blomen, E.; Hendriks, C.; Neele, F. Capture Technologies: Improvements and Promising Developments. *Energy Procedia* 2009, 1, 1505–1512. [CrossRef]
- 20. Davidson, R.M. Post-Combustion Carbon Capture from Coal Fired Plants-Solvent Scrubbing; IEA Clean Coal Centre: London, UK, 2007.
- 21. Ciferno, J.P.; Fout, T.E.; Jones, A.P.; Murphy, J.T. Capturing Carbon from Existing Coal-Fired Power Plants. *Chem. Eng. Prog.* 2009, 105, 33.
- 22. Dincer, I.; Colpan, C.O.; Kizilkan, O. *Exergetic, Energetic and Environmental Dimensions*; Academic Press: Cambridge, MA, USA, 2017. [CrossRef]
- 23. De Visser, E.; Hendriks, C.; Barrio, M.; Mølnvik, M.J.; de Koeijer, G.; Liljemark, S.; Le Gallo, Y. Dynamis CO<sub>2</sub> Quality Recommendations. *Int. J. Greenh. Gas Control* **2008**, *2*, 478–484. [CrossRef]
- Olajire, A.A. CO<sub>2</sub> Capture and Separation Technologies for End-of-Pipe Applications—A Review. *Energy* 2010, 35, 2610–2628. [CrossRef]
- 25. Kanniche, M.; Gros-Bonnivard, R.; Jaud, P.; Valle-Marcos, J.; Amann, J.M.; Bouallou, C. Pre-Combustion, Post-Combustion and Oxy-Combustion in Thermal Power Plant for CO<sub>2</sub> Capture. *Appl. Therm. Eng.* **2010**, *30*, 53–62. [CrossRef]
- 26. Nord, L.O.; Anantharaman, R.; Bolland, O. Design and Off-Design Analyses of a Pre-Combustion CO<sub>2</sub> Capture Process in a Natural Gas Combined Cycle Power Plant. *Int. J. Greenh. Gas Control* **2009**, *3*, 385–392. [CrossRef]
- European Environment Agency. COM 80 Final—A Framework Strategy for a Resilient Energy Union with a Forward-Looking Climate Change Policy. 2015. Available online: https://www.eea.europa.eu/policy-documents/com-2015-80-final (accessed on 21 May 2022).
- 28. Mitsubishi Power. Available online: https://power.mhi.com/news/20180308.html (accessed on 21 May 2022).
- Fusina Combined Cycle Project: Planning to Run on Pure Hydrogen—Modern Power Systems. Available online: https://www. modernpowersystems.com/features/featurefusina-combined-cycle-project-planning-to-run-on-pure-hydrogen/ (accessed on 21 May 2022).
- 30. Siemens, Engie, Euro Universities Create Hydrogen Gas Turbine Demonstrator Project. Available online: https://www.powereng.com/gas/siemens-engie-euro-universities-create-hydrogen-gas-turbine-demonstrator-project/ (accessed on 21 May 2022).
- Bartocci, P.; Abad, A.; Cabello, A.; Zampilli, M.; Buia, G.; Serra, A.; Colantoni, S.; Taiana, A.; Bidini, G.; Fantozzi, F. Technical Economic and Environmental Analysis of Chemical Looping versus Oxyfuel Combustion for NGCC Power Plant. *E3S Web Conf.* 2021, 312, 08019. [CrossRef]
- Buhre, B.J.P.; Elliott, L.K.; Sheng, C.D.; Gupta, R.P.; Wall, T.F. Oxy-Fuel Combustion Technology for Coal-Fired Power Generation. Prog. Energy Combust. Sci. 2005, 31, 283–307. [CrossRef]
- Khila, Z.; Baccar, I.; Jemel, I.; Houas, A.; Hajjaji, N. Energetic, Exergetic and Environmental Life Cycle Assessment Analyses as Tools for Optimization of Hydrogen Production by Autothermal Reforming of Bioethanol. *Int. J. Hydrogen Energy* 2016, 41, 17723–17739. [CrossRef]
- Cabral, R.P.; Heldebrant, D.J.; Mac Dowell, N. A Techno-Economic Analysis of a Novel Solvent-Based Oxycombustion CO<sub>2</sub> Capture Process. Ind. Eng. Chem. Res. 2019, 58, 6604–6612. [CrossRef]
- 35. Kolster, C.; Mechleri, E.; Krevor, S.; Dowell, N.M. The Role of CO<sub>2</sub> Purification and Transport Networks in Carbon Capture and Storage Cost Reduction. *Int. J. Greenh. Gas Control* **2017**, *58*, 127–141. [CrossRef]
- Cabral, R.P.; Dowell, N.M. A Novel Methodological Approach for Achieving £/MWh Cost Reduction of CO<sub>2</sub> Capture and Storage (CCS) Processes. *Appl. Energy* 2017, 205, 529–539. [CrossRef]
- 37. Li, F.; Luo, S.; Sun, Z.; Bao, X.; Fan, L.S. Role of Metal Oxide Support in Redox Reactions of Iron Oxide for Chemical Looping Applications: Experiments and Density Functional Theory Calculations. *Energy Environ. Sci.* **2011**, *4*, 3661–3667. [CrossRef]
- Zafar, Q.; Mattisson, T.; Gevert, B. Integrated Hydrogen and Power Production with CO<sub>2</sub> Capture Using Chemical-Looping Reforming Redox Reactivity of Particles of CuO, Mn<sub>2</sub>O<sub>3</sub>, NiO, and Fe<sub>2</sub>O<sub>3</sub> Using SiO<sub>2</sub> as a Support. *Ind. Eng. Chem. Res.* 2005, 44, 3485–3496. [CrossRef]
- Adanez, J.; Abad, A.; Garcia-Labiano, F.; Gayan, P.; de Diego, L.F. Progress in Chemical-Looping Combustion and Reforming Technologies. Prog. Energy Combust. Sci. 2012, 38, 215–282. [CrossRef]

- 40. Erlach, B.; Schmidt, M.; Tsatsaronis, G. Comparison of Carbon Capture IGCC with Pre-Combustion Decarbonisation and with Chemical-Looping Combustion. *Energy* **2011**, *36*, 3804–3815. [CrossRef]
- Czakiert, T.; Krzywanski, J.; Zylka, A.; Nowak, W. Chemical Looping Combustion: A Brief Overview. *Energies* 2022, 15, 1563. [CrossRef]
- 42. Zerobin, F.; Penthor, S.; Bertsch, O.; Pröll, T. Fluidized Bed Reactor Design Study for Pressurized Chemical Looping Combustion of Natural Gas. *Powder Technol.* 2017, 316, 569–577. [CrossRef]
- 43. Eret, P. A Cost-Effective Compressed Air Generation for Manufacturing Using Modified Microturbines. *Appl. Therm. Eng.* **2016**, 107, 311–319. [CrossRef]
- 44. Timilsina, G.R. Are Renewable Energy Technologies Cost Competitive for Electricity Generation? *Renew. Energy* 2021, 180, 658–672. [CrossRef]
- Liguori, S.; Wilcox, J. Design Considerations for Postcombustion CO<sub>2</sub> Capture with Membranes. In *Current Trends and Future Developments on (Bio-) Membranes*; Chapter, 14; Basile, A., Favvas, E.P., Eds.; Elsevier: Amsterdam, The Netherlands, 2018; pp. 385–413. [CrossRef]
- 46. Wang, X.; Song, C. Carbon Capture from Flue Gas and the Atmosphere: A Perspective. *Front. Energy Res.* **2020**, *8*, 560849. [CrossRef]
- Rackley, S. Overview of Carbon Capture and Storage. In *Carbon Capture Storage*; Elsevier: Amsterdam, The Netherlands, 2017; pp. 23–36.
- 48. Madejski, P.; Chmiel, K.; Subramanian, N.; Kuś, T. Methods and Techniques for CO<sub>2</sub> Capture: Review of Potential Solutions and Applications in Modern Energy Technologies. *Energies* **2022**, *15*, 887. [CrossRef]
- 49. Tramošljika, B.; Blecich, P.; Bonefačić, I.; Glažar, V. Advanced Ultra-Supercritical Coal-Fired Power Plant with Post-Combustion Carbon Capture: Analysis of Electricity Penalty and CO<sub>2</sub> Emission Reduction. *Sustainability* **2021**, *13*, 801. [CrossRef]
- 50. La Plante, E.C.; Simonetti, D.A.; Wang, J.; Al-Turki, A.; Chen, X.; Jassby, D.; Sant, G.N. Saline Water-Based Mineralization Pathway for Gigatonne-Scale CO<sub>2</sub> Management. *ACS Sustain. Chem. Eng.* **2021**, *9*, 1073–1089. [CrossRef]
- 51. Rubin, E.S.; Davison, J.E.; Herzog, H.J. The Cost of CO<sub>2</sub> Capture and Storage. *Int. J. Greenh. Gas Control* **2015**, *40*, 378–400. [CrossRef]
- 52. Huang, X.; Ai, N.; Li, L.; Jiang, Q.; Wang, Q.; Ren, J.; Wang, J. Simulation of CO<sub>2</sub> Capture Process in Flue Gas from Oxy-Fuel Combustion Plant and Effects of Properties of Absorbent. *Separations* **2022**, *9*, 95. [CrossRef]
- 53. Khan, M.N.; Chiesa, P.; Cloete, S.; Amini, S. Integration of Chemical Looping Combustion for Cost-Effective CO<sub>2</sub> Capture from State-of-the-Art Natural Gas Combined Cycles. *Energy Convers. Manag.* X **2020**, *7*, 100044. [CrossRef]
- 54. Fan, J.; Hong, H.; Jin, H. Power Generation Based on Chemical Looping Combustion: Will It Qualify to Reduce Greenhouse Gas Emissions from Life-Cycle Assessment? *ACS Sustain. Chem. Eng.* **2018**, *6*, 6730–6737. [CrossRef]
- 55. Doughty, C.; Freifeld, B.M.; Trautz, R.C. Site Characterization for CO<sub>2</sub> Geologic Storage and vice versa: The Frio Brine Pilot, TX, USA as a Case Study. *Environ. Geol.* **2008**, *54*, 1635–1656. [CrossRef]
- Gibson-Poole, C.M.; Svendsen, L.; Underschultz, J.; Watson, M.N.; Ennis-King, J.; Van Ruth, P.J.; Nelson, E.J.; Daniel, R.F.; Cinar, Y. Site Characterisation of a Basin-Scale CO<sub>2</sub> Geological Storage System: Gippsland Basin, Southeast Australia. *Environ. Geol.* 2008, 54, 1583–1606. [CrossRef]
- 57. Anwar, M.N.; Fayyaz, A.; Sohail, N.F.; Khokhar, M.F.; Baqar, M.; Khan, W.D.; Rasool, K.; Rehan, M.; Nizami, A.S. CO<sub>2</sub> Capture and Storage: A Way forward for Sustainable Environment. *J. Environ. Manag.* **2018**, 226, 131–144. [CrossRef] [PubMed]
- 58. Herzog, H.; Golomb, D. Carbon Capture and Storage from Fossil Fuel Use. Encycl. Energy 2004, 1, 277–287. [CrossRef]
- 59. Celia, M.A.; Nordbotten, J.M. Practical Modeling Approaches for Geological Storage of Carbon Dioxide. *Ground Water* **2009**, 47, 627–638. [CrossRef] [PubMed]
- 60. Fang, Y.; Baojun, B.; Dazhen, T.; Dunn-Norman, S.; Wronkiewicz, D. Characteristics of CO<sub>2</sub> Sequestration in Saline Aquifers. *Pet. Sci.* **2010**, *7*, 83–92. [CrossRef]
- Van Der Zwaan, B.; Smekens, K. CO<sub>2</sub> Capture and Storage with Leakage in an Energy-Climate Model. *Environ. Model. Assess.* 2009, 14, 135–148. [CrossRef]
- 62. Mazzotti, M.; Abanades, J.C.; Allam, R.; Lackner, K.S.; Meunier, F.; Rubin, E.; Sanchez, J.C.; Yogo, K.; Zevenhoven, R. Mineral Carbonation and Industrial Uses of Carbon Dioxide. In *IPCC Special Report on Carbon Dioxide Capture and Storage*; Cambridge University Press: Cambridge, UK, 2005.
- 63. Rubin, E.; De Coninck, H. IPCC Special Report on Carbon Dioxide Capture and Storage. In *TNO* (2004): Cost Curves for CO<sub>2</sub> Storage; Cambridge University Press: Cambridge, UK, 2005; p. 14.
- 64. National Academies of Sciences, Engineering, and Medicine. Negative emissions technologies and reliable sequestration: A research agenda. In *Negative Emissions Technologies and Reliable Sequestration: A Research Agenda*; European Commission: Brussels, Belgium, 2018.
- Garcia Moretz-Sohn Monteiro, J.; Goetheer, E.; Schols, E.; van Os, P.; Pérez Calvo, J.F.; Hoppe, H.; Bharadwaj, H.S.; Roussanaly, S.; Khakharia, P.; Feenstra, M.; et al. Post-Capture CO<sub>2</sub> Management: Options for the Cement Industry. *Zenodo*. 14 April 2018. [CrossRef]
- 66. Jimoh, O.A.; Ariffin, K.S.; Hussin, H.B.; Temitope, A.E. Synthesis of Precipitated Calcium Carbonate: A Review. *Carbonates Evaporites* **2018**, *33*, 331–346. [CrossRef]

- Dindi, A.; Quang, D.V.; Vega, L.F.; Nashef, E.; Abu-Zahra, M.R.M. Applications of Fly Ash for CO<sub>2</sub> Capture, Utilization, and Storage. J. CO2 Util. 2019, 29, 82–102. [CrossRef]
- Liu, Q.; Maroto-Valer, M.M.; Sanna, A. Mineral Carbonation Technology Overview. CO2 Sequestration Ex-Situ Miner. *Carbonation* 2017, 1–15.
- 69. Mercedes, M.V. *Developments and Innovation in Carbon Dioxide* (CO<sub>2</sub>) *Capture and Storage Technology*; Elsevier: Amsterdam, The Netherlands, 2010. [CrossRef]
- Blondes, M.S.; Merrill, M.D.; Anderson, S.T.; DeVera, C.A. Carbon Dioxide Mineralization Feasibility in the United States; US Geological Survey: Reston, VA, USA, 2019. [CrossRef]
- Huijgen, W.J.J.; Comans, R.N.J.; Witkamp, G.J. Cost Evaluation of CO<sub>2</sub> Sequestration by Aqueous Mineral Carbonation. *Energy Convers. Manag.* 2007, 48, 1923–1935. [CrossRef]
- 72. Abdelshafy, A.; Walther, G. Coupling Carbon Capture and Utilization with the Construction Industry: Opportunities in Western Germany. *J. CO2 Util.* **2022**, *57*, 101866. [CrossRef]
- 73. Gerdemann, S.J.; O'Connor, W.K.; Dahlin, D.C.; Penner, L.R.; Rush, H. Ex Situ Aqueous Mineral Carbonation. *Environ. Sci. Technol.* **2007**, *41*, 2587–2593. [CrossRef]
- 74. Ji, L.; Yu, H. Carbon dioxide sequestration by direct mineralization of fly ash. In *Carbon Dioxide Sequestration in Cementitious Construction Materials*; Woodhead Publishing: Sawston, UK, 2018; pp. 13–37. [CrossRef]
- Verduyn, M.; Geerlings, H.; van Mossel, G.; Vijayakumari, S. Review of the Various CO<sub>2</sub> Mineralization Product Forms. *Energy* Procedia 2011, 4, 2885–2892. [CrossRef]
- Pan, S.Y.; Chiang, A.; Chang, E.E.; Lin, Y.P.; Kim, H.; Chiang, P.C. An Innovative Approach to Integrated Carbon Mineralization and Waste Utilization: A Review. *Aerosol Air Qual. Res.* 2015, 15, 1072–1091. [CrossRef]
- Fernández Bertos, M.; Li, X.; Simons, S.J.R.; Hills, C.D.; Carey, P.J. Investigation of Accelerated Carbonation for the Stabilisation of MSW Incinerator Ashes and the Sequestration of CO<sub>2</sub>. *Green Chem.* 2004, *6*, 428–436. [CrossRef]
- Saito, T.; Sakai, E.; Morioka, M.; Otsuki, N. Carbonation of γ-Ca<sub>2</sub>SiO<sub>4</sub> and the Mechanism of Vaterite Formation. *J. Adv. Concr. Technol.* 2010, *8*, 273–280. [CrossRef]
- Zaelke, D.; Young, O.; Andersen, S.O. Scientific Synthesis of Calera Carbon Sequestration and Carbonaceous By-Product Applications; Scientific American: Valencia, CA, USA, 2011; pp. 1–64.
- 80. Jones, J.D. Removing carbon dioxide from waste streams through co-generation of carbonate and/or bicar-bonate minerals. U.S. Patent 7727374, 1 June 2010.
- 81. Jones, J.; Barton, C.; Clayton, M.; Yablonsky, A.; Legere, D. *SkyMine Carbon Mineralization Pilot Project*; Skyonic Corporation: Austin, TX, USA, 2010.
- 82. Kim, J.; Kim, S.-Y.; Bae, J.; Shinn, Y.-J.; Ahn, E.; Lee, J.-W. Analysis of Patent Trends on the CCUS Technologies. *Econ. Environ. Geol.* **2020**, *53*, 491–504.
- 83. Walters, J. SkyMine Beneficial CO<sub>2</sub> Use Project; Skyonic Corporation: Austin, TX, USA, 2016. [CrossRef]
- 84. Damiani, D.; Litynski, J.T.; McIlvried, H.G.; Vikara, D.M.; Srivastava, R.D. The US Department of Energy's R&D Program to Reduce Greenhouse Gas Emissions through Beneficial Uses of Carbon Dioxide. *Greenh. Gases Sci. Technol.* **2012**, *2*, 9–16.
- Plaza, M.G.; Martínez, S.; Rubiera, F. CO<sub>2</sub> Capture, Use, and Storage in the Cement Industry: State of the Art and Expectations. Energies 2020, 13, 5692. [CrossRef]
- Quinn, S.; Sahu, S. Compositions and Methods for Controling Setting of Carbonatable Calcium Silicate Cements Containing Hydrating Materials. U.S. Patent 10196311, 15 February 2019.
- Meyer, V.; de Cristofaro, N.; Bryant, J.; Sahu, S. Solidia Cement an Example of Carbon Capture and Utilization. *Key Eng. Mater.* 2018, 761, 197–203. [CrossRef]
- 88. Xi, F.; Davis, S.J.; Ciais, P.; Crawford-Brown, D.; Guan, D.; Pade, C.; Shi, T.; Syddall, M.; Lv, J.; Ji, L. Substantial Global Carbon Uptake by Cement Carbonation. *Nat. Geosci.* **2016**, *9*, 880–883. [CrossRef]
- Leemann, A.; Hunkeler, F.; Widmer, H. Assessing the CO<sub>2</sub>-Binding of Concrete during Its Service Life. In Proceedings of the SynerCrete'18 International Conference on Interdisciplinary Approaches for Cement-Based Materials and Structural Concrete, Funchal, Portugal, 24–26 October 2018.
- Madlool, N.A.; Saidur, R.; Hossain, M.S.; Rahim, N.A. A Critical Review on Energy Use and Savings in the Cement Industries. *Renew. Sustain. Energy Rev.* 2011, 15, 2042–2060. [CrossRef]
- Mehdipour, I.; Falzone, G.; Prentice, D.; Neithalath, N.; Simonetti, D.; Sant, G. The Role of Gas Flow Distributions on CO<sub>2</sub> Mineralization within Monolithic Cemented Composites: Coupled CFD-Factorial Design Approach. *React. Chem. Eng.* 2021, 6, 494–504. [CrossRef]
- 92. Wei, Z.; Wang, B.; Falzone, G.; La Plante, E.C.; Okoronkwo, M.U.; She, Z.; Oey, T.; Balonis, M.; Neithalath, N.; Pilon, L.; et al. Clinkering-Free Cementation by Fly Ash Carbonation. *J. CO2 Util.* **2018**, *23*, 117–127. [CrossRef]
- 93. Puerta-Falla, G.; Balonis, M.; Falzone, G.; Bauchy, M.; Neithalath, N.; Sant, G. Monovalent Ion Exchange Kinetics of Hydrated Calcium-Alumino Layered Double Hydroxides. *Ind. Eng. Chem. Res.* **2017**, *56*, 63–74. [CrossRef]
- Mehdipour, I.; Falzone, G.; La Plante, E.C.; Simonetti, D.; Neithalath, N.; Sant, G. How Microstructure and Pore Moisture Affect Strength Gain in Portlandite-Enriched Composites That Mineralize CO<sub>2</sub>. ACS Sustain. Chem. Eng. 2019, 7, 13053–13061. [CrossRef]

- 95. Falzone, G.; Mehdipour, I.; Neithalath, N.; Bauchy, M.; Simonetti, D.; Sant, G. New Insights into the Mechanisms of Carbon Dioxide Mineralization by Portlandite. *AIChE J.* **2021**, *67*, e17160. [CrossRef]
- Sant, G.N. Upcycled "CO<sub>2</sub>-Negative" Concrete for Construction Functions; University of California: Los Angeles, CA, USA, 2021. [CrossRef]
- 97. Sahu, S.; Meininger, R.C. Sustainability and Durability of Solidia Cement Concrete. Concr. Int. 2020, 42, 29–34.
- Atakan, V.; Sahu, S.; Quinn, S.; Hu, X.; DeCristofaro, N. Why CO<sub>2</sub> Matters-Advances in a New Class of Cement. ZKG Int. Dtsch.-Engl. Ausg. 1995 2014, 3, 60–63.
- 99. Alturki, A.A. Integration of Sorption Enhanced Operations into Sustainable Processes; University of California: Los Angeles, CA, USA, 2020.
- Bustillos, S.; Alturki, A.; Prentice, D.; La Plante, E.C.; Rogers, M.; Keller, M.; Ragipani, R.; Wang, B.; Sant, G.; Simonetti, D.A. Implementation of Ion Exchange Processes for Carbon Dioxide Mineralization Using Industrial Waste Streams. *Front. Energy Res.* 2020, *8*, 352. [CrossRef]
- 101. Implementation of Ion Exchange Processes on Industrial Waste Streams for CO2 Mineralization. Available online: https://aiche.confex.com/aiche/2019/meetingapp.cgi/Paper/564092 (accessed on 16 December 2021).
- 102. Alturki, A.A. A Single Component Adsorption of Alcohols in Zeolites; University of California: Los Angeles, CA, USA, 2017.
- Kampschreur, M.J.; Temmink, H.; Kleerebezem, R.; Jetten, M.S.M.; van Loosdrecht, M.C.M. Nitrous Oxide Emission during Wastewater Treatment. Water Res. 2009, 43, 4093–4103. [CrossRef] [PubMed]
- 104. Lackner, K.S. Capture of Carbon Dioxide from Ambient Air. Eur. Phys. J. Spec. Top. 2009, 176, 93–106. [CrossRef]
- Wang, T.; Lackner, K.S.; Wright, A. Moisture Swing Sorbent for Carbon Dioxide Capture from Ambient Air. *Environ. Sci. Technol.* 2011, 45, 6670–6675. [CrossRef]
- 106. Shi, X.; Xiao, H.; Lackner, K.S.; Chen, X. Capture CO<sub>2</sub> from Ambient Air Using Nanoconfined Ion Hydration. *Angew. Chem. Int. Ed.* **2016**, *55*, 4026–4029. [CrossRef]
- Shi, X.; Xiao, H.; Liao, X.; Armstrong, M.; Chen, X.; Lackner, K.S. Humidity Effect on Ion Behaviors of Moisture-Driven CO<sub>2</sub> Sorbents. J. Chem. Phys. 2018, 149, 164708. [CrossRef]
- 108. Shi, X.; Xiao, H.; Azarabadi, H.; Song, J.; Wu, X.; Chen, X.; Lackner, K.S. Sorbents for the Direct Capture of CO<sub>2</sub> from Ambient Air. Angew. Chem. Int. Ed. 2020, 59, 6984–7006. [CrossRef]
- 109. Yusuf, Z.; Cameron, J. Decarbonization Reactions between Sodium Metaborate and Sodium Carbonate. *Ind. Eng. Chem. Res.* 2004, 43, 8148–8154. [CrossRef]
- Bang, J.-H.; Chae, S.-C.; Song, K.; Lee, S.-W. Optimizing Experimental Parameters in Sequential CO<sub>2</sub> Mineralization Using Seawater Desalination Brine. *Desalination* 2021, 519, 115309. [CrossRef]
- 111. Aicher, T. Renewable Hydrogen Technologies. Production, Purification, Storage, Applications, and Safety. *Energy Technol.* **2015**, *3*, 90–91. [CrossRef]
- Hashaikeh, R.; Lalia, B.S.; Kochkodan, V.; Hilal, N. A Novel In Situ Membrane Cleaning Method Using Periodic Electrolysis. J. Membr. Sci. 2014, 471, 149–154. [CrossRef]
- 113. Park, K.; Kim, J.; Yang, D.R.; Hong, S. Towards a Low-Energy Seawater Reverse Osmosis Desalination Plant: A Review and Theoretical Analysis for Future Directions. *J. Membr. Sci.* **2020**, *595*, 117607. [CrossRef]
- Zohrabian, A.; Plata, S.L.; Kim, D.M.; Childress, A.E.; Sanders, K.T. Leveraging the Water-Energy Nexus to Derive Benefits for the Electric Grid through Demand-Side Management in the Water Supply and Wastewater Sectors. *Wiley Interdiscip. Rev. Water* 2021, 8, e1510. [CrossRef]
- Elsaid, K.; Sayed, E.T.; Abdelkareem, M.A.; Baroutaji, A.; Olabi, A.G. Environmental Impact of Desalination Processes: Mitigation and Control Strategies. *Sci. Total Environ.* 2020, 740, 140125. [CrossRef] [PubMed]
- 116. Achilli, A.; Prante, J.L.; Hancock, N.T.; Maxwell, E.B.; Childress, A.E. Experimental Results from RO-PRO: A Next Generation System for Low-Energy Desalination. *Environ. Sci. Technol.* **2014**, *48*, 6437–6443. [CrossRef]
- Prante, J.L.; Ruskowitz, J.A.; Childress, A.E.; Achilli, A. RO-PRO Desalination: An Integrated Low-Energy Approach to Seawater Desalination. *Appl. Energy* 2014, 120, 104–114. [CrossRef]
- Wang, Q.-W.; Yang, G.-P.; Zhang, Z.-M.; Jian, S. Perfluoroalkyl Acids in Surface Sediments of the East China Sea. *Environ. Pollut.* 2017, 231, 59–67. [CrossRef]
- Jang, J.; Kang, Y.; Han, J.-H.; Jang, K.; Kim, C.-M.; Kim, I.S. Developments and Future Prospects of Reverse Electrodialysis for Salinity Gradient Power Generation: Influence of Ion Exchange Membranes and Electrodes. *Desalination* 2020, 491, 114540. [CrossRef]
- Jia, X.; Klemeš, J.J.; Varbanov, P.S.; Wan Alwi, S.R. Analyzing the Energy Consumption, GHG Emission, and Cost of Seawater Desalination in China. *Energies* 2019, 12, 463. [CrossRef]
- 121. Voutchkov, N. Energy Use for Membrane Seawater Desalination—Current Status and Trends. *Desalination* **2018**, 431, 2–14. [CrossRef]
- 122. Raluy, G.; Serra, L.; Uche, J. Life Cycle Assessment of MSF, MED and RO Desalination Technologies. *Energy* **2006**, *31*, 2361–2372. [CrossRef]
- Panagopoulos, A. A Comparative Study on Minimum and Actual Energy Consumption for the Treatment of Desalination Brine. Energy 2020, 212, 118733. [CrossRef]

- 124. Mansour, T.M.; Ismail, T.M.; Ramzy, K.; Abd El-Salam, M. Energy Recovery System in Small Reverse Osmosis Desalination Plant: Experimental and Theoretical Investigations. *Alex. Eng. J.* **2020**, *59*, 3741–3753. [CrossRef]
- 125. Jones, E.; Qadir, M.; van Vliet, M.T.H.; Smakhtin, V.; Kang, S. The State of Desalination and Brine Production: A Global Outlook. *Sci. Total Environ.* **2019**, 657, 1343–1356. [CrossRef] [PubMed]
- 126. Papapetrou, M.; Cipollina, A.; La Commare, U.; Micale, G.; Zaragoza, G.; Kosmadakis, G. Assessment of Methodologies and Data Used to Calculate Desalination Costs. *Desalination* **2017**, *419*, 8–19. [CrossRef]
- 127. National Academies of Sciences, Engineering, and Medicine. *Gaseous Carbon Waste Streams Utilization: Status and Research Needs;* National Academies Press: Washington, DC, USA, 2019.
- 128. Kainiemi, L.; Eloneva, S.; Toikka, A.; Levänen, J.; Järvinen, M. Opportunities and Obstacles for CO<sub>2</sub> Mineralization: CO<sub>2</sub> Mineralization Specific Frames in the Interviews of Finnish Carbon Capture and Storage (CCS) Experts. *J. Clean. Prod.* 2015, 94, 352–358. [CrossRef]