

## SUPPORTING INFORMATION

### Supplementary information S1

#### S1.1: The detailed simulation of ammonia production from syngas HYSYS Documentation

The decision variables in this case are:

Reformer temperature: 900°C

Combuster temperature: 1400°C

Low temperature conversion reactor temperature (LTC): 160°C

Fluid package: Peng-Robinson

Component: Methane, Ethane, Propane, i-Butane, n-Butane, Nitrogen, CO, CO<sub>2</sub>, H<sub>2</sub>O,

Oxygen, Hydrogen, Ammonia, Methanol

#### Reactions:

Set-1

Rxn-1 Type: Equilibrium      Stoich Coeff

Methane                          -1

H<sub>2</sub>O                            -1

CO                                1

Hydrogen                        3

Rxn-2 Type: Equilibrium      Stoich Coeff

Ethane                           -1

H<sub>2</sub>O                            -2

CO                                2

Hydrogen                        5

Rxn-3 Type: Equilibrium      Stoich Coeff

Propane	-1
H <sub>2</sub> O	-3
CO	3
Hydrogen	7
Rxn-4 Type: Equilibrium	Stoich Coeff
i-Butane	-1
H <sub>2</sub> O	-4
CO	4
Hydrogen	9
Rxn-5 Type: Equilibrium	Stoich Coeff
n-Butane	-1
H <sub>2</sub> O	-4
CO	4
Hydrogen	9

### Set-2

Rxn-1 Type: Equilibrium	Stoich Coeff
CO	-2
Oxygen	-1
CO <sub>2</sub>	2
Rxn-2 Type: Equilibrium	Stoich Coeff
Hydrogen	-2
Oxygen	-1
H <sub>2</sub> O	2
Rxn-3 Type: Equilibrium	Stoich Coeff
Methane	-1

Oxygen	-2
H <sub>2</sub> O	2
CO <sub>2</sub>	1
Rxn-4 Type: Equilibrium	Stoich Coeff
Ethane	-2
Oxygen	-7
H <sub>2</sub> O	6
CO <sub>2</sub>	4
Rxn-5 Type: Equilibrium	Stoich Coeff
Propane	-1
Oxygen	-5
H <sub>2</sub> O	4
CO <sub>2</sub>	3

### Set-3

Rxn-1 Type: Equilibrium	Stoich Coeff
CO	-1
Hydrogen	-3
Methane	1
H <sub>2</sub> O	1
Rxn-2 Type: Equilibrium	Stoich Coeff
CO <sub>2</sub>	-1
Hydrogen	-4
Methane	1
H <sub>2</sub> O	2

### Set-4

Rxn-1 Type: Kinetic              Stoich Coeff

Ammonia                          2

Hydrogen                        -3

Nitrogen                        -1

Set-5

Rxn-1 Type: Equilibrium              Stoich Coeff

CO                                -1

H<sub>2</sub>O                            -1

CO<sub>2</sub>                            1

Hydrogen                        1

Streams:

HPSteam

Composition              Mole fraction

H<sub>2</sub>O                        1.0000

Temperature = 350 °C

Pressure = 120 bar

NaturalGas

Composition              Mole fraction

Methane                    0.9575

Ethane                      0.0267

Propane                    0.0065

i-Butane                    0.0010

n-Butane                    0.0011

Nitrogen                    0.0072

Temperature = 25 °C

Pressure = 35 bar

Air

Composition	Mole fraction
Nitrogen	0.7900
Oxygen	0.2100

Temperature = 800 °C

Pressure = 35 bar

Reformer\_Feed (decision variable)

Temperature = 900 °C

Combuster\_Feed (decision variable)

Temperature = 1400 °C

W\_in\_1

Composition	Mole fraction
H <sub>2</sub> O	1.0000

Temperature = 25 °C

Pressure = 1 bar

W\_out\_1

Composition	Mole fraction
H <sub>2</sub> O	1.0000

Temperature = 80 °C

Pressure = 1 bar

WSGR1\_Feed

Temperature = 450 °C

W\_in\_2

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 25 °C

Pressure = 1 bar

W\_out\_2

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 80 °C

Pressure = 1 bar

WSGR2\_Feed (decision variable)

Temperature = 160 °C

W\_in\_3

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 25 °C

Pressure = 1 bar

W\_out\_3

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 80 °C

Pressure = 1 bar

Separator1\_Feed

Temperature = 100 °C

Methanizer\_Feed

Temperature = 340 °C

W\_in\_5

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 25 °C

Pressure = 1 bar

W\_out\_5

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 80 °C

Pressure = 1 bar

Separator2\_Feed

Temperature = 40 °C

Make-up N2

Composition      Mole fraction

Nitrogen      1.0000

Temperature = 0 °C

Pressure = 140 bar

Molar Flow = 1000 kgmole/hr

ComP1\_out

Pressure = 80 bar

W\_in\_6

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 25 °C

Pressure = 1 bar

W\_out\_6

Composition Mole fraction

H<sub>2</sub>O 1.0000

Temperature = 80 °C

Pressure = 1 bar

Cool2\_out

Temperature = 90 °C

ComP2\_out

Pressure = 150 bar

W\_in\_7

Composition Mole fraction

H<sub>2</sub>O 1.0000

Temperature = 25 °C

Pressure = 1 bar

W\_out\_7

Composition Mole fraction

H<sub>2</sub>O 1.0000

Temperature = 80 °C

Pressure = 1 bar

Separator3\_Feed

Temperature = 40 °C

Feed\_1

Temperature = 450 °C

W\_in\_9

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 25 °C

Pressure = 1 bar

W\_out\_9

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 80 °C

Pressure = 1 bar

Product\_separator

Vapor-Phase Fraction = 1.0000

Recycle

Temperature = 20 °C

LN2\_in

Composition      Mole fraction

Nitrogen      1.0000

Temperature = -196.2 °C

Pressure = 1 bar

LN2\_out

Composition      Mole fraction

Nitrogen      1.0000

Temperature = -80 °C

Pressure = 1 bar

Liquid\_to\_separator

Temperature = -45 °C

Vessel:

Reformer

Reaction Set: Set-1

Combuster

Reaction Set: Set-2

HTC

Reaction Set: Set-5

LTC

Reaction Set: Set-5

Methanizer

Reaction Set: Set-3

For all plug flow reactors

Reaction Set: Set-4

Heater:

E-100

Inlet Stream: Feed

Outlet: Reformer\_Feed

Delta P: 0 bar

E-113

Inlet Stream: Heated\_re\_pro

Outlet: Combuster\_Feed

Delta P: 0 bar

E-104

Inlet Stream: SynGas\_Flow

Outlet: Methanizer\_Feed

Delta P: 0 bar

Heat Exchanger:

For all heat exchangers:

Heat Exchanger Model: Simple Weighted

Tube Side Delta P = 0 bar

Shell Side Delta P = 0 bar

Mixer:

MIX-100

Feed

Composition	Mole fraction
-------------	---------------

Methane	0.2522
Ethane	0.0070
Propane	0.0017
i-Butane	0.0003
n-Butane	0.0003
Nitrogen	0.0019
H <sub>2</sub> O	0.7366

MIX-101

Heated\_re\_pro

Composition	Mole fraction
-------------	---------------

Methane	0.0326
Nitrogen	0.1192
CO	0.1294
H <sub>2</sub> O	0.3066

Oxygen 0.0314

Hydrogen 0.3809

#### MIX-102

##### Feed\_ammonia

Composition Mole fraction

Methane 0.0147

Nitrogen 0.6462

H<sub>2</sub>O 0.0005

Hydrogen 0.3319

Ammonia 0.0066

#### MIX-103

32

Composition Mole fraction

Methane 0.0012

Nitrogen 0.2585

H<sub>2</sub>O 0.0027

Hydrogen 0.7376

#### MIX-104

##### Feed\_2

Composition Mole fraction

Methane 0.0189

Nitrogen 0.6882

H<sub>2</sub>O 0.0006

Ammonia 0.2922

#### MIX-105

Feed\_3

Composition	Mole fraction
Methane	0.0190
Nitrogen	0.6887
H <sub>2</sub> O	0.0006
Ammonia	0.2917

TEE:

TEE-100

Split Fraction

Quench1 = 0.9950

Quench2 = 0.0025

Quench3 = 0.0025

TEE-101

Split Fraction

Purge = 0.0100

Product to liquid = 0.9900

Recycle:

RCY-3

Inlet Stream: N2\_to\_Recycle

Outlet Stream: N2\_recycle

## **S1.2: The detailed simulation of methanol production with a recycle**

**HYSYS Documentation**

The decision variables in this case are:

Pressure of the equilibrium reactor (ERV-100): 70 bar

Temperature of the equilibrium reactor (ERV-100): 190 °C

Temperature of a separator (E-101): 60 °C

Recycle ratio (RCY-1): 1

Fluid package: Peng Robinson

Component: CO<sub>2</sub>, Hydrogen, Methanol, CO, H<sub>2</sub>O

### **Reactions:**

Set-1

Rxn-1 Type: Equilibrium      Stoich Coeff

CO <sub>2</sub>	-1
H <sub>2</sub> O	1
Methanol	1
Hydrogen	-3

Rxn-2 Type: Equilibrium      Stoich Coeff

CO	-1
Methanol	1
Hydrogen	-2

Rxn-3 Type: Equilibrium      Stoich Coeff

CO <sub>2</sub>	-1
CO	1
Methanol	1
Hydrogen	-1

Streams:

Hydrogen

Composition      Mole fraction

Hydrogen      1.0000

Temperature = 25 °C

Pressure = 20 bar

Carbon dioxide

Composition      Mole fraction

CO<sub>2</sub>      1.0000

Temperature = 40 °C

Pressure = 20 bar

Compressed feed (decision variable)

Pressure = 70 bar

Heated feed (decision variable)

Temperature = 190 °C

Water\_in

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 20 °C

Pressure = 1 bar

Water\_out

Composition      Mole fraction

H<sub>2</sub>O      1.0000

Temperature = 35 °C

Pressure = 1 bar

Cooled product (decision variable)

Temperature = 60 °C

Vessel:

ERV-100

Reaction Set: Set-1

Towers:

T-100

Number of stages: 10

Inlet Stream

Stream: Cooled product (decision variable)

Inlet Stage: 5\_Main Tower

Condenser: Full Reflux

Condenser Pressure = 4 bar

Condenser Delta P = 0 bar

Reboiler Pressure = 4 bar

Reboiler Delta P = 0 bar

Specifications:

Condenser Temperature = 25 °C

Reflux Ratio = 0.6

T-101

Number of stages: 10

Inlet Stream

Stream: Methanol-water

Inlet Stage: 5\_Main Tower

Condenser: Total

Condenser Pressure = 4 bar

Condenser Delta P = 0 bar

Reboiler Pressure = 4 bar

Reboiler Delta P = 0 bar

Specifications:

Comp Fraction

Stage: Condenser

Flow Basis: Mole Fraction

Phase: Liquid

Spec Value: 0.9950

Component: Methanol

Reflux Ratio = 30

Heater:

Inlet Stream: Mixed feed

Outlet: Heated feed

Delta P: 0 bar

Heat Exchanger:

For all heat exchangers:

Heat Exchanger Model: Simple Weighted

Tube Side Delta P = 0 bar

Shell Side Delta P = 0 bar

Mixer:

MIX-100

Feed

Composition              Mole fraction

Hydrogen 0.7500

CO<sub>2</sub> 0.2500

#### MIX-101

##### Mixed feed

Composition Mole fraction

Hydrogen 0.8053

CO<sub>2</sub> 0.1886

CO 0.0013

Methanol 0.0039

H<sub>2</sub>O 0.0009

#### MIX-102

##### Combined product

Composition Mole fraction

Hydrogen 0.0025

CO<sub>2</sub> 0.0154

CO 0.0000

Methanol 0.4911

H<sub>2</sub>O 0.4910

#### TEE:

#### TEE-100

##### Split Fraction

To recycle = 1.00

To mixer = 0.00

#### Recycle:

#### RCY-1

Inlet Stream: To recycle

Outlet Stream: Recycle

Valves:

VLV-101

Inlet stream: To mixer

Outlet stream:

Pressure = 4 bar

VLV-102

Inlet stream: Liquid\_product

Outlet stream

Pressure = 4 bar

**S1.3: The detailed simulation of CO<sub>2</sub> absorption by methanol via Rectisol**

**process HYSYS Documentation**

The decision variables in this case are:

Lean methanol temperature: -25.0°C

The 3<sup>rd</sup> stage separator pressure: 1.2 bar

Stripper reflux ratio: 5

Stripper inlet temperature: 40°C

Distillation reflux ratio: 1

Fluid package: PRSV

Component: Methanol, CO<sub>2</sub>, Ammonia, CO, Argon, Nitrogen, Hydrogen, H<sub>2</sub>O, Methane

Streams:

Syngas Feed

Composition	Mole fraction
-------------	---------------

CO <sub>2</sub>	0.4590
Ammonia	0.0001
CO	0.0052
Argon	0.0085
Nitrogen	0.4923
Hydrogen	0.0272
H <sub>2</sub> O	0.0027
Methane	0.0050

Temperature = 18.30 °C

Pressure = 17.24 bar

#### Lean Methanol

Composition	Mole fraction
Methanol	0.9998
H <sub>2</sub> O	0.0002

Temperature (decision variable) = -25 °C

Pressure = 17.20 bar

#### 5F (decision variable)

Temperature = 40 °C

#### Methanol

Composition	Mole fraction
Methanol	1.0000

Temperature = 21 °C

Pressure = 1.1 bar

#### NH-3

Composition	Mole fraction

Ammonia 1.0000

Temperature = -70 °C

Pressure = 1 bar

NH-4

Composition Mole fraction

Ammonia 1.0000

Temperature = -50 °C

Pressure = 1 bar

Towers:

Absorber

Number of stages: 15

Inlet Stream

Stream: 5B-3

Inlet Stage: 15\_Main Tower

Top Stage Inlet: Lean Methanol

Stripper

Number of stages: 10

Inlet Stream

Stream: 5F (decision variable)

Inlet Stage: 10\_Main Tower

Stream: 3C-3 (decision variable)

Inlet Stage: 11\_Main Tower

Condenser: Full Reflux

Condenser Pressure = 1.1 bar

Condenser Delta P = 0 bar

Reboiler Pressure = 1.1 bar

Reboiler Delta P = 0 bar

Specifications:

Comp Ratio = 0.9500

Reflux Ratio (decision variable) = 5

Distillation

Number of stages: 12

Inlet Stream

Stream: 2

Inlet Stage: 5\_Main Tower

Condenser: Full Reflux

Condenser Pressure = 3.4 bar

Condenser Delta P = 0 bar

Reboiler Pressure = 3.4 bar

Reboiler Delta P = 0 bar

Specifications:

Comp Ratio = 0.99

Reflux Ratio (decision variable) = 1

Heat Exchanger:

For all heat exchangers:

Heat Exchanger Model: Simple Weighted

Tube Side Delta P = 0 bar

Shell Side Delta P = 0 bar

Mixer:

MIX-100

6A-7

Composition Mole fraction

Methanol 0.9999

H<sub>2</sub>O 0.0001

MIX-101

1B

Composition Mole fraction

Methanol 0.1862

CO<sub>2</sub> 0.2004

Ammonia 0.0002

CO 0.0036

Argon 0.0041

Nitrogen 0.3376

Hydrogen 0.2593

H<sub>2</sub>O 0.0029

Methane 0.0059

MIX-102

4H

Composition Mole fraction

Methanol 0.0146

CO<sub>2</sub> 0.9476

Ammonia 0.0008

CO 0.0001

Argon 0.0006

Nitrogen 0.0344

Hydrogen      0.0001

Methane      0.0019

TEE:

TEE-100

Split Fraction

$6C = 0.9400$

$6D-1 = 0.0600$

Valve:

VLV-100

Inlet stream: 3A

Outlet stream: 2

Pressure = 3.4 bar

VLV-101

Inlet stream: 5C

Outlet stream: 5C-2

Pressure = 4.5 bar

VLV-102

Inlet stream: 5A

Outlet stream: 5A-2

Pressure = 10.5 bar

VLV-103

Inlet stream: 5D

Outlet stream: 5D-2

Pressure = 4.5 bar (decision variable)

Recycle:

RCY-1

Inlet Stream: 5B

Outlet Stream: 5B-2

RCY-2

Inlet Stream: 6D-1

Outlet Stream: 6D

RCY-3

Inlet Stream: 6E-1

Outlet Stream: Lean Methanol

RCY-4

Inlet Stream: 3C-2

Outlet Stream: 3C

## Supplementary information S2

### S2.1: Final data set of Case study I: ammonia production from syngas

Sample no.	Decision variables			Response Ammonia production cost
	x <sub>1</sub>	x <sub>2</sub>	x <sub>3</sub>	
1	1153.47	1522.43	190.06	576.03
2	989.12	1467.24	281.62	556.63
3	1164.99	1672.82	254.31	648.00
4	1124.42	1567.96	202.96	588.94
5	922.86	1406.41	205.68	505.25
6	1048.96	1547.33	264.13	585.45
7	1037.08	1505.91	167.29	549.42
8	1016.11	1603.51	162.43	583.59
9	976.84	1690.36	196.72	621.42
10	1095.54	1455.63	223.08	548.77
11	933.05	1417.36	173.66	506.26
12	906.22	1653.35	228.98	607.52
13	1189.02	1576.66	287.31	632.67
14	1180.29	1593.89	219.19	611.34
15	971.01	1620.26	245.53	599.96
16	1135.40	1495.11	270.62	583.39
17	1007.10	1665.00	271.47	633.36
18	1061.01	1536.71	248.98	577.83
19	1100.68	1481.80	184.73	552.14
20	955.61	1628.75	211.49	595.98
21	1074.02	1433.58	234.38	538.25
22	1121.60	1567.94	201.16	588.01
23	1114.70	1564.07	198.40	585.01
24	900.00	1432.03	160.00	507.48
25	1007.20	1666.77	275.99	636.49
26	1006.64	1659.79	272.91	631.79
27	900.00	1400.00	183.04	497.62
28	996.40	1468.40	283.43	559.07
29	990.83	1459.03	278.79	552.75
30	900.00	1400.00	177.05	497.13

**S2.2: Final data set of Case study II: methanol production via carbon dioxide hydrogenation**

Sample no.	Decision variables				Response Methanol production cost
	x <sub>1</sub>	x <sub>2</sub>	x <sub>3</sub>	x <sub>4</sub>	
1	68.43	201.98	62.00	0.6046	1618.57
2	57.86	201.15	65.57	0.1721	2898.02
3	55.86	193.07	70.48	0.1395	2760.07
4	53.27	191.74	79.37	0.4834	2001.59
5	58.77	194.46	74.66	0.9282	1090.09
6	57.50	207.15	67.57	0.5387	2084.13
7	52.28	208.60	67.01	0.0128	4381.01
8	59.75	202.47	77.17	0.0714	3133.65
9	52.09	202.88	78.28	0.8561	1330.76
10	63.86	194.20	72.25	0.4568	1836.09
11	50.06	200.68	64.56	0.3766	2663.30
12	63.43	206.21	61.16	0.8169	1329.13
13	66.12	196.73	76.52	0.3568	2020.91
14	54.46	209.62	71.58	0.5097	2337.28
15	60.69	190.78	78.95	0.7016	1416.77
16	62.18	196.04	60.13	0.8650	1182.66
17	50.88	198.26	70.79	0.3058	2758.26
18	61.03	190.33	66.12	0.6630	1475.46
19	64.87	203.78	76.19	0.9625	1042.72
20	53.93	199.99	63.15	0.1054	3290.48
21	66.77	198.71	69.36	0.6396	1534.88
22	69.29	207.04	68.78	0.4074	2073.98
23	67.25	208.23	75.44	0.2771	2465.39
24	61.46	205.53	73.76	0.2200	2757.53
25	56.66	195.45	63.60	0.7194	1493.37
26	65.43	197.38	68.18	0.9656	1023.04
27	55.05	204.88	62.47	0.1968	3153.04
28	68.94	192.66	73.35	0.7778	1239.14
29	52.70	209.22	66.89	0.0189	4355.37
30	52.44	208.65	66.68	0.0089	4386.29
31	70.00	190.00	80.00	1.0000	942.45
32	56.17	193.42	70.66	0.1289	2784.44
33	55.83	193.07	70.06	0.1238	2801.24
34	68.41	204.98	60.00	1.0000	1002.55
35	55.54	204.82	62.81	0.2136	3063.39
36	55.20	204.34	62.14	0.1939	3127.63
37	70.00	190.00	70.96	1.0000	950.13
38	52.02	203.43	78.36	0.8399	1375.90
39	51.43	203.04	78.12	0.8220	1423.52

40	70.00	207.99	76.01	1.0000	989.75
41	52.46	208.82	66.99	0.0167	4359.64
42	52.27	208.64	66.90	0.0026	4435.38
43	65.91	191.32	80.00	1.0000	952.13
44	68.48	201.93	61.83	0.6047	1617.03
45	68.11	201.56	61.67	0.5767	1667.13
46	67.24	194.77	60.00	1.0000	972.79

**S2.3: Final data set of Case study III: CO<sub>2</sub> absorption by methanol via Rectisol process**

Sample no.	Decision variables					Response Capture cost
	x <sub>1</sub>	x <sub>2</sub>	x <sub>3</sub>	x <sub>4</sub>	x <sub>5</sub>	
1	-49.23	1.229	8.771	16.72	6.136	112.46
2	-23.43	1.606	6.422	22.06	9.323	117.24
3	-46.37	1.479	16.311	26.65	9.631	176.00
4	-52.99	1.939	5.777	26.26	4.232	98.36
5	-43.91	1.304	9.989	27.30	5.244	105.41
6	-35.83	1.734	11.425	33.87	6.573	122.39
7	-29.26	1.774	16.645	29.45	5.769	136.68
8	-20.29	1.630	5.076	29.81	3.585	72.66
9	-25.61	1.724	15.599	31.89	9.765	154.00
10	-33.49	1.407	14.172	14.41	2.664	102.97
11	-26.56	1.499	14.933	37.13	1.862	90.03
12	-47.20	1.701	12.639	11.87	8.579	163.88
13	-36.66	1.753	15.806	38.20	7.604	151.40
14	-51.74	1.209	8.156	21.18	2.375	85.44
15	-21.51	1.571	19.422	28.41	2.183	115.72
16	-45.17	1.360	11.636	23.43	4.487	112.75
17	-54.88	1.318	6.779	32.88	8.186	117.28
18	-27.94	1.908	17.157	25.36	5.035	139.27
19	-28.85	1.545	10.494	34.67	6.920	109.08
20	-40.91	1.453	13.837	13.33	1.080	102.48
21	-41.45	1.405	19.922	31.09	6.322	156.90
22	-22.28	1.876	8.943	19.14	2.952	90.87
23	-37.87	1.639	9.499	15.73	8.247	129.13
24	-39.25	1.285	10.769	35.07	7.702	116.51
25	-32.00	1.967	18.855	24.06	3.465	145.87
26	-50.41	1.909	14.659	17.47	5.441	169.91
27	-31.20	1.999	7.858	14.24	4.605	100.30
28	-48.86	1.858	17.927	39.68	6.867	189.42
29	-30.46	1.260	6.016	20.01	3.300	70.23
30	-42.96	1.542	13.111	18.21	3.837	121.05
31	-53.77	1.450	13.157	10.62	8.903	170.07
32	-38.17	1.811	7.449	20.61	7.288	114.72
33	-44.51	1.678	12.252	36.21	9.039	151.20
34	-34.99	1.339	18.361	11.32	1.331	110.01
35	-24.48	1.821	17.773	38.30	1.602	110.28
36	-48.02	1.858	18.145	39.71	6.791	188.79
37	-48.63	1.844	17.895	39.53	6.679	187.08
38	-31.21	1.200	5.000	33.95	1.000	46.35
39	-28.21	1.560	10.533	34.84	7.057	110.19
40	-28.71	1.549	10.237	34.10	7.031	109.09

41	-20.00	1.200	5.000	23.67	1.000	52.59
42	-54.08	1.337	6.945	33.02	8.083	117.89
43	-54.86	1.322	6.803	32.38	8.018	116.86
44	-35.74	1.200	5.000	33.89	1.000	47.83
45	-34.31	1.351	18.645	11.61	1.513	112.37
46	-34.72	1.346	18.324	10.94	1.279	110.24
47	-20.00	1.281	5.000	39.31	1.000	46.12
48	-40.07	1.474	13.826	13.09	1.129	102.81
49	-40.84	1.455	13.619	12.96	1.042	99.59
50	-26.47	1.280	5.000	40.00	1.000	43.95
51	-24.38	1.829	17.729	38.81	1.694	111.06
52	-24.87	1.827	17.530	38.38	1.617	109.80
53	-37.16	1.511	5.000	40.00	1.000	50.04

## Supplementary information S3

### S3.1 Weights and biases of an artificial neural networks for training the data set of random sampling.

#### S3.1.1 Case study I: ammonia production from syngas

Mean square errors:

Data set	MSE
Training	1.52E-05
Validation	1.19E-04
Testing	4.52E-05

Weight 1,  $WI_{r,k}$

Neurons	Input nodes		
	1	2	3
1	-2.3682	0.6228	0.5254
2	-0.1803	-0.0498	-1.3409
3	0.1440	0.2659	-0.0401
4	-1.4446	1.7557	0.5200
5	-0.1177	0.1200	0.4391
6	-1.3274	0.0407	-1.3057
7	-0.2760	-1.7613	0.0743
8	2.0677	-1.8151	-0.6159

Weight 2,  $W2_r$

Neurons	Output node
1	-0.0416
2	-0.3629
3	2.3181
4	0.0745
5	0.8902
6	-0.0186
7	-0.0540
8	-0.1241

Bias 1,  $BI_r$

Neurons	Output node
1	2.3922
2	1.3427
3	-0.2083
4	-0.3426
5	1.4267
6	-0.1934
7	-1.8252
8	2.5504

Bias 2, B2	0.0129
------------	--------

### S3.1.2 Case study II: methanol production via carbon dioxide hydrogenation

Mean square errors:

Data set	MSE
Training	3.20E-07
Validation	8.24E-06
Testing	4.61E-06

Weight 1,  $WI_{r,k}$

Neurons	Input nodes			
	1	2	3	4
1	0.9948	0.6365	-0.1825	-0.1942
2	0.3067	0.2540	-0.2935	-2.6807
3	-0.9732	1.3545	1.0360	-1.0357
4	0.7542	-0.6835	0.0090	-0.7380
5	0.0794	-0.0215	-0.0181	0.7138
6	1.0944	-0.9190	0.0708	-0.6277
7	-0.2468	0.2019	-0.0045	-0.4551
8	-1.1972	0.5411	-0.0324	-1.2129

Weight 2,  $W2_r$

Neurons	Output node
1	0.0225
2	0.0272
3	-0.0055
4	0.0792
5	-0.3989
6	0.1319
7	2.1486
8	0.2470

Bias 1,  $BI_r$

Neurons	Output node
1	-0.8868
2	2.1283
3	1.4075
4	0.2115
5	-0.1466
6	1.9636
7	-1.0273
8	-2.7433

Bias 2,  $B2$  | 1.3462

### S3.1.3 Case study III: CO<sub>2</sub> absorption by methanol via Rectisol process

Mean square errors:

Data set	MSE
Training	2.85E-05
Validation	5.50E-05
Testing	4.22E-05

Weight 1,  $WI_{r,k}$

Neurons	Input nodes				
	1	2	3	4	5
1	-1.1612	0.4267	0.6170	0.0776	-0.0070
2	-2.0083	-0.0265	-0.0583	0.0438	-0.1383
3	0.0076	0.0483	-0.0250	0.0230	-0.1016
4	-0.1773	0.2575	0.0805	0.0104	-0.0002
5	2.2137	0.0507	0.0991	-0.0537	0.1723
6	0.1480	-0.3700	0.1323	-0.0025	-0.0004
7	-0.6150	0.1493	-0.2343	0.0470	0.0128
8	-1.7773	0.5226	2.2852	0.3430	-0.1023

Weight 2,  $W2_r$

Neurons	Output node
1	0.3551
2	-0.8543
3	-3.6878
4	2.6417
5	-0.6012
6	1.1263
7	-1.2372
8	-0.0256

Bias 1,  $BI_r$

Neurons	Output node
1	-1.5419
2	1.4949
3	-0.0233
4	-0.2838
5	-1.4584
6	0.6507
7	-1.7367
8	-2.5763

Bias 2, B2	-0.9123
------------	---------

**S3.2 Weights and biases of an artificial neural networks for training the data set of adaptive Latin hypercube sampling.**

**S3.2.1 Case study I: ammonia production from syngas**

Mean square errors:

Data set	MSE
Training	9.92E-07
Validation	2.85E-04
Testing	6.46E-04

Weight 1,  $W1_{r,k}$

Neurons	Input nodes		
	1	2	3
1	0.7357	-1.3657	2.1587
2	-2.0546	-0.9905	-1.7479
3	2.0853	0.3863	1.8296
4	1.6385	2.1145	0.0074
5	1.9052	-1.9173	-1.3953
6	1.7018	-2.2192	-0.4386
7	1.0337	1.9477	-0.0395
8	-2.0165	1.2170	0.9853

Weight 2,  $W2_r$

Neurons	Output node
1	-0.0577
2	-0.2594
3	-0.0703
4	0.3227
5	-0.1809
6	-0.0355
7	0.4293
8	0.2925

Bias 1,  $BI_r$

Neurons	Output node
1	-2.9187
2	2.0097
3	-1.4948
4	-0.6331
5	-0.1269
6	1.0142
7	2.1234
8	-3.1478

Bias 2, B2	0.1989
------------	--------

### S3.2.2 Case study II: methanol production via carbon dioxide hydrogenation

Mean square errors:

Data set	MSE
Training	3.06E-08
Validation	1.29E-04
Testing	1.02E-05

Weight 1,  $WI_{r,k}$

Neurons	Input nodes			
	1	2	3	4
1	-0.3066	-1.5063	-0.9558	0.7309
2	1.0728	-0.4369	0.0888	-1.6636
3	0.0529	-0.0215	0.0344	1.5948
4	0.4170	-1.7917	-0.8440	-1.9836
5	1.4311	-1.3899	1.1017	0.9473
6	-0.2295	0.2196	0.0183	-0.9931
7	2.1562	-0.3368	-0.8320	1.2068
8	-0.9796	0.7576	-0.3045	-1.2917

Weight 2,  $W2_r$

Neurons	Output node
1	-0.0626
2	-0.0206
3	-0.2198
4	0.0139
5	-0.0210
6	0.7670
7	-0.0847
8	0.6752

Bias 1,  $BI_r$

Neurons	Output node
1	-2.9615
2	-0.4146
3	-0.9196
4	0.5101
5	1.2467
6	-0.7789
7	3.0020
8	-3.3325

Bias 2, B2	0.6054
------------	--------

### S3.2.3 Case study III: CO<sub>2</sub> absorption by methanol via Rectisol process

Mean square errors:

Data set	MSE
Training	1.32E-04
Validation	4.27E-04
Testing	2.33E-03

Weight 1,  $WI_{r,k}$

Neurons	Input nodes				
	1	2	3	4	5
1	-2.0167	0.7220	-0.6211	-0.7957	-1.0699
2	-0.0506	0.3918	-0.0145	-1.3910	1.2934
3	-1.0740	0.0579	1.1195	-0.2202	-0.1242
4	0.4088	-0.3947	0.7916	0.9237	-1.1863
5	1.7848	-0.5047	-0.3678	1.4842	1.2589
6	0.2225	0.4808	0.9969	-0.0013	0.7223
7	0.3278	0.1813	0.4486	1.1427	-0.6860
8	-1.0223	0.9647	1.4222	0.1476	0.2411

Weight 2,  $W2_r$

Neurons	Output node
1	-0.3738
2	0.2561
3	0.4370
4	-0.2361
5	0.1715
6	0.2842
7	0.0372
8	0.3227

Bias 1,  $BI_r$

Neurons	Output node
1	2.9622
2	-2.1864
3	0.0097
4	-0.7930
5	0.4856
6	0.7373
7	2.5068
8	-1.8019

Bias 2, B2	0.5801
------------	--------