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# Fence Shaping of Substrate Integrated Fan-Beam Electric Dipole for High-Band 5G

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Received: 17 April 2019; Accepted: 13 May 2019; Published: 15 May 2019



**Abstract:** This work presents fence shaping for dipole antenna operating at 5G high-band frequencies. A via fence is employed around the dipole to suppress back radiation. By varying the geometric shape of the fence, the dipole's radiation characteristics can be controlled, which adds an additional degree of freedom to the design. This was investigated by studying different fence shapes, namely rectangular-, U-, and V-shaped fences. The wide bandwidth (higher than 6.5 GHz) centered around 28 GHz, and the stable radiation performance from 24 GHz to 32 GHz made the proposed structure capable of supporting multiple 5G frequency bands and the fence shaping help modulate the gain and HPBW of the dipole. All fabricated prototypes attained front-to-back radiation ratio (F/B) higher than 36 dB, with good gain/HPBW performances of 14.1 dBi/103.7°, 13.5dBi/118°, and 12.6 dBi/133° from the V-fence, U-fence, and rectangular fence 4 × 1 arrays, respectively.

**Keywords:** 5G; fence shaping; array; dipole; fan-beam; edge; via

## 1. Introduction

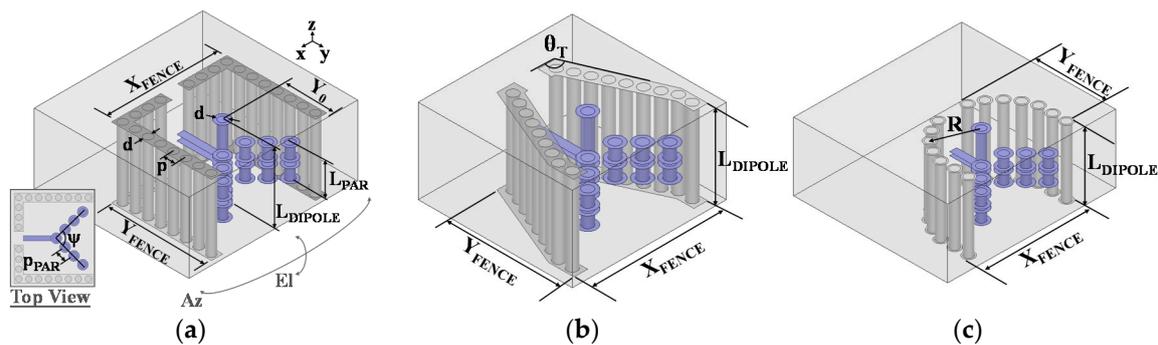
In wireless communication transceivers, high performance integrated antenna design is very critical for achieving a good signal-to-noise ratio performance [1]. Recently, antenna design for high-band 5G wireless has greatly attracted the attention of the research community in both industry and academia, owing to the promises of 5G to overcome the limited bandwidth and data rates of the 4G standard, together with the ability to support the expected mobile traffic explosion by 2020 [2–5].

Designing mmWave antennas is challenging, especially on the mobile device side, which is the target of this work. The free space path loss that accompanies mmWave communications is much higher than that with the current sub-6 GHz mobile standards, owing to the high frequency propagation [6]. This dictates the need for directional high gain antennas. In addition, for better coverage, a wide fan beam is required [7]. Moreover, the antenna needs to be implemented at the mobile device edge [8]. For area-limited mobile devices, implementing the array at the device's edge can result in an area-efficient full 3D space coverage, as opposed to planar structures [9,10] offering only sub-hemispherical coverage [11]. To summarize, for the mobile device mmWave edge antenna to be able to achieve good performance, it requires a gain higher than 10 dBi, a fan beam with HPBW in the elevation plane (HPBW<sub>EI</sub>) greater than 100° [8], together with compact size and high front-to-back radiation ratio (F/B) to avoid interaction with the RF transceiver circuits. Achieving all those requirements at the same time is challenging. The focus of this work was to develop and design an antenna that is capable of meeting all of those specifications simultaneously.

A couple of interesting edge-implemented antenna designs exist in the literature [12–15]. However, they suffer from some limitations. In Reference [12,13], a 28 GHz mesh grid array was presented.

They employed a large number of array elements, which requires a large number of phase shifters for beamsteering, which in turn complicates the design of the phase shifter RF chip and results in higher power consumption. In Reference [14], a Ka-band dipole array loaded horn antenna was introduced, which suffered low F/B and HPBW. A beamsteering phased array, implemented as 16 cavity-backed slot antennas, proposed in Reference [15] to operate in the 28 GHz band, suffered from degraded low F/B and HPBW. Hence, it can be concluded that the aforementioned structures are not able to achieve the high gain, HPBW, and F/B requirements simultaneously.

In Reference [16], the authors proposed a mm-Wave electric dipole surrounded by a rectangular fence to suppress back radiation that simultaneously achieved high gain, F/B, and HPBW in the elevation plane ( $HPBW_{EI}$ ). In fact, the fence did more than just suppressing the back radiation. Modulating the geometric shape of the fence helped control and improve the dipole's radiation performance. This is a property of the electric dipole which magneto-electric dipoles [17,18] cannot offer. Fence shaping adds more degrees of freedom, and gives more flexibility to the electric dipole design to satisfy different scenarios. In this work, the fence shaping capability of the electric dipole was studied and analyzed where different fence shapes (shown in Figure 1) were examined, namely, V-shaped and U-shaped fences, in addition to the conventional rectangular fence. The proposed structure features stable radiation pattern over a wide frequency range from 24 GHz to 32 GHz allowing it to support multiple 5G bands, more specifically, the 24 GHz, the 26 GHz, the 28 GHz and the 32 GHz frequency bands [19,20].



**Figure 1.** Electric dipole with different fence shapes implemented at the edge of Rogers RO5880 substrate. (a) Rectangular fence. (b) V-shaped fence. (c) U-shaped fence.

The rest of the paper is organized as follows; the conventional dipole antenna with rectangular fence is summarized in Section 2.1. The effect of fence shaping is introduced in Section 2.2, and the performance comparison between the different fences is presented in Section 2.3. Finally, the fabricated prototypes, measurement results, and comparison with the state-of-the-art structures are presented in Section 3.

## 2. Materials and Methods

### 2.1. Dipole with Conventional Rectangular Fence

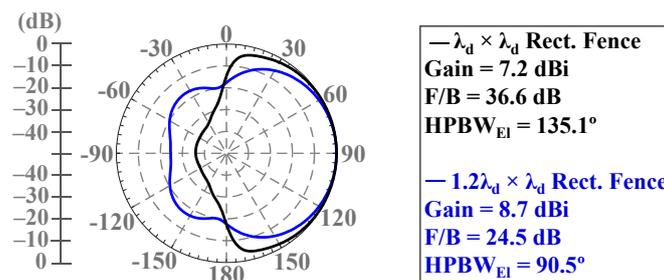
The geometry of the dipole with an  $X_{FENCE} \times Y_{FENCE}$  rectangular fence is shown in Figure 1a. For higher dipole gain, parasitic vias were employed ahead of the dipole. They were flared with angle  $\psi$  for  $HPBW_{EI}$  improvement. A detailed parametric study on the dipole was introduced in Reference [15]. To set a reference for this study, a summary of the optimized dipole parameters is provided in Table 1, achieving 7.2 dBi gain, 36.6 dB F/B, and  $135.1^\circ$   $HPBW_{EI}$ . Throughout this paper, the dipole parameters will be set as in Table 1 for optimal performance. The fence dimensions and shape had a great influence on the radiation performance of the antenna [21,22]. For example, higher gain was achieved by modulating the rectangular fence dimensions from  $X_{FENCE} \times Y_{FENCE} = \lambda_d \times \lambda_d$  to  $1.2\lambda_d \times \lambda_d$ , resulting in the gain increasing from 7.2 to 8.7 dBi. However, this came at the cost of

severe degradation in the  $HPBW_{EI}$  and F/B by  $44.6^\circ$  and 12.1 dB, respectively, as illustrated in Figure 2. Hence, simply changing the fence dimensions is sub-optimal. A better way to provide the required gain enhancement without sacrificing the  $HPBW_{EI}$  and F/B is fence shaping [23].

**Table 1.** Electric dipole design parameters.

$L_{DIPOLE}$	$Y_0$	$d$	$p$	$X_{FENCE}$	$Y_{FENCE}$	$L_{PAR}$	$\psi$	$P_{PAR}$
$0.7 \lambda_d$	$0.54 \lambda_d$	0.6 mm	0.83 mm	$\lambda_d^*$	$\lambda_d$	$0.26 \lambda_d$	$80^\circ$	0.8 mm

\*  $\lambda_d$ : The wavelength inside the RO5880 Slab at 28 GHz.



**Figure 2.** The radiation pattern of the rectangular fenced dipole with  $X_{FENCE} \times Y_{FENCE} = \lambda_d \times \lambda_d$  and  $1.2\lambda_d \times \lambda_d$ .

### 2.2. Dipole Shaped Fence

In this section, the fence shaping capability of the proposed electric dipole is introduced. The concept of fence shaping is presented with the aid of parametric study and electric field distribution on two case studies, namely the V-shaped and U-shaped fences, and compares their performance with the conventional rectangular fence case.

The geometry of the dipole with the fence tapered in a V-shaped fashion is shown in Figure 1b. The V-fence is defined by its size span  $X_{FENCE} \times Y_{FENCE}$  and the tapering angle ( $\theta_T$ ). The V-fence size  $X_{FENCE} \times Y_{FENCE}$  is set to  $\lambda_d \times \lambda_d$ , like the rectangular fence, for optimal performance. To get more insight into the design perspectives of the tapered V-fence, a parametric study was conducted on  $\theta_T$ . Figure 3 shows the simulated gain,  $HPBW_{EI}$ , and F/B plotted versus  $\theta_T$  at 28 GHz. As  $\theta_T$  increased beyond  $90^\circ$ —where  $\theta_T = 90^\circ$  corresponds to the rectangular fence case—the gain increases. This was accompanied by a decrease in the  $HPBW_{EI}$ . However, the decrease in the  $HPBW_{EI}$  as  $\theta_T$  increased was not steep where the  $HPBW_{EI}$  was still wide and greater than  $100^\circ$ , up to  $\theta_T = 125^\circ$ . For the different tapering angles of the V-fence, the antenna exhibited good F/B higher than 30 dB. The implemented dipole with V-fence prototype was designed with  $\theta_T = 115^\circ$  for optimal F/B, providing 37.6 dB F/B,  $108.2^\circ$   $HPBW_{EI}$ , and 8.9 dBi gain.

Compared to the  $1.2\lambda_d \times \lambda_d$  rectangular fence dipole, the  $115^\circ$  tapered V-fence dipole achieved 0.2 dBi higher gain, 13.1 dB higher F/B, and  $17.7^\circ$  higher  $HPBW_{EI}$ . This shows the effectiveness of shaping the dipole’s fence in achieving improved radiation performance, compared to just resizing the rectangular fence. Thus, when higher dipole gain is required, employing a  $115^\circ$  tapered V-fence is a better option than resizing the rectangular fence from  $\lambda_d \times \lambda_d$  to  $1.2\lambda_d \times \lambda_d$ . This can also be explained using the electric field distributions shown in Figure 4, where both the  $115^\circ$  tapered V-fence and the  $1.2\lambda_d \times \lambda_d$  rectangular fence dipoles had higher peak field intensity at the front face compared to the  $\lambda_d \times \lambda_d$  rectangular fence dipole, indicating higher gain. However, the  $115^\circ$  tapered V-fence dipole had lower field intensity at the back dipole face and more uniform field intensity along the z-axis of the front dipole face compared to the  $1.2\lambda_d \times \lambda_d$  rectangular fence dipoles, indicating lower back radiation (enhanced F/B) and higher  $HPBW_{EI}$ , respectively.

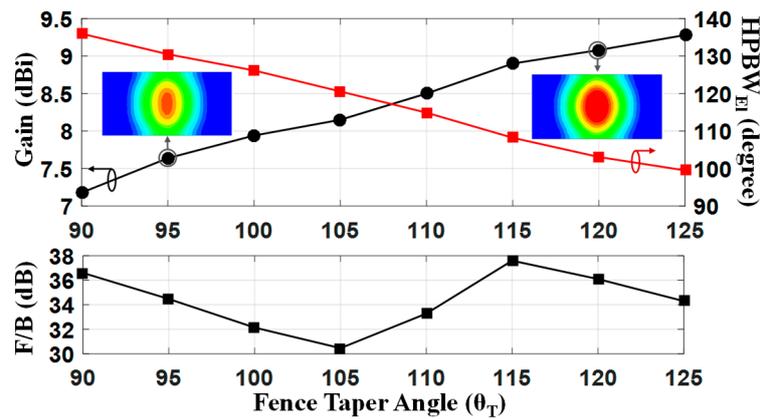


Figure 3. The simulated gain, HPBW<sub>EI</sub>, and F/B versus the V-fence taper angle at 28 GHz, and the electric field at the dipole front face at  $\theta_T = 95^\circ$  and  $120^\circ$ .

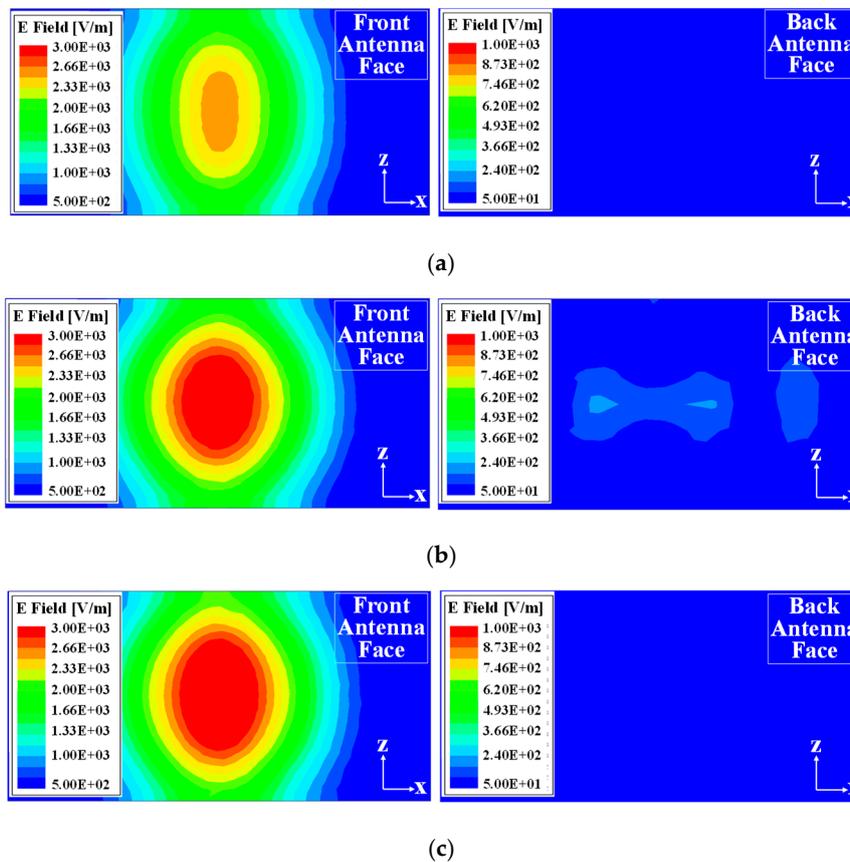
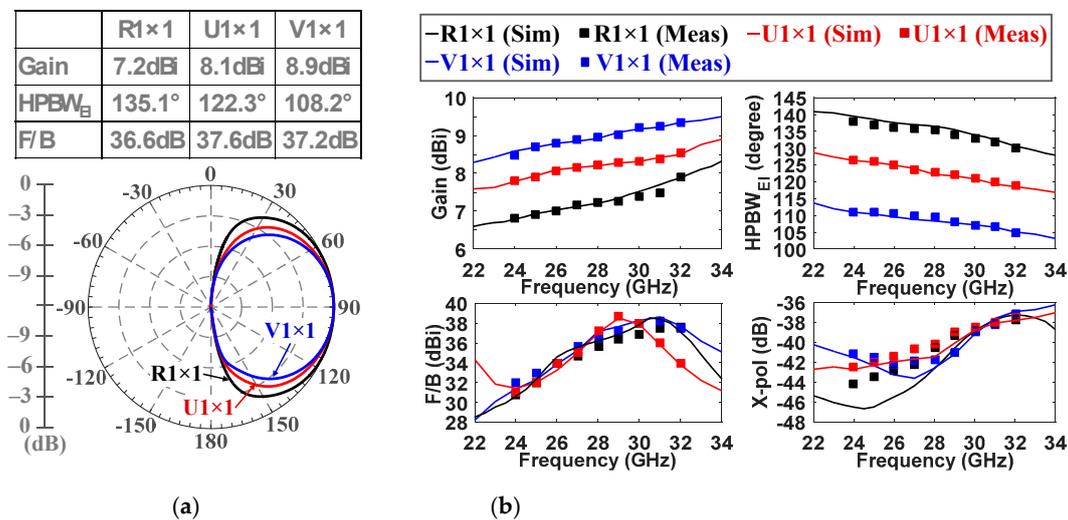


Figure 4. The electric field in the x-z plane at the front and back faces of the dipole antenna. (a) With the optimal  $\lambda_d \times \lambda_d$  rectangular fence. (b) With the  $1.2\lambda_d \times \lambda_d$  rectangular fence. (c) With the  $115^\circ$  tapered V-fence.

If an intermediate point between the  $\lambda_d \times \lambda_d$  rectangular fence and the  $115^\circ$  tapered V-fence dipole is required, a  $105^\circ$  tapered V-fence can be chosen, which achieved 8.1 dBi gain,  $120.5^\circ$  HPBW<sub>EI</sub>, and 30.4 dB F/B. However, a better fence can be designed for that case to provide enhanced F/B. Hence, a third fence shape with moderate tapering was investigated, namely, the U-shaped fence, which has a curved tapering, as shown in Figure 1c. The U-fence is defined by its size span  $X_{FENCE} \times Y_{FENCE}$  (set to  $\lambda_d \times \lambda_d$ ) and the curve radius ( $R$ ). By setting  $R$  to 3.2 mm for optimal performance, the U-fence dipole attained 37.2 dB F/B.

### 2.3. Performance Comparison of the Different Fence Shapes

In this section, the performance of the dipole with the different fence shapes is compared and discussed. For fair comparison, all the fences spanned the same size of  $X_{FENCE} \times Y_{FENCE} = \lambda_d \times \lambda_d$ . The simulated zoomed-in radiation patterns in the elevation plane for the  $\lambda_d \times \lambda_d$  rectangular fence, U-fence, and  $115^\circ$  tapered V-fence dipoles—denoted by  $R1 \times 1$ ,  $U1 \times 1$ , and  $V1 \times 1$ , respectively—are illustrated in Figure 5a. With increased fence tapering, as we went from the rectangular fence to the U-fence to the V-fence, the gain increased, while the  $HPBW_{EI}$  decreased with approximately no effect on the F/B, and in all cases a wide  $HPBW_{EI}$  greater than  $108^\circ$  was achieved. Hence, the proposed electric dipole provides an additional design degree of freedom for 5G handset device antennas, where the radiation pattern and gain can be controlled by amount of fence tapering. Another important advantage of the proposed structure is its stable radiation pattern over a wide bandwidth, ranging from 22.5 GHz to 34 GHz, which makes it capable of supporting multiple 5G frequency bands. Figure 5b provides the simulated/measured radiation performance of the dipole with its different fence shapes versus frequency. As can be noted, in addition to the high gain, HPBW, and F/B, the proposed vertically-polarized structure provides low cross-polarization (X-pol) levels.



**Figure 5.** (a) The simulated radiation pattern in the elevation plane for the dipole with rectangular ( $R1 \times 1$ ), U- ( $U1 \times 1$ ), and V-fence ( $V1 \times 1$ ) at 28 GHz. (b) The simulated and measured radiation performance of the electric dipole with the different fence shapes versus frequency.

The dipole feed is composed of a parallel strip line (PS), a substrate-integrated waveguide (SIW), and a SIW-to-PS transition. The bandwidth can be controlled by adjusting the dimensions of the SIW-to-PS transition. The 7 mm width SIW employs 0.6 mm diameter vias with 0.8 mm pitch. The SIW-to-PS transition is designed by gradually tapering the SIW width with a  $59^\circ$  tapering angle, using 4 vias with slightly higher pitch of 0.88 mm. It is also instructive to study the mutual coupling between the adjacent dipole array elements for the different fence shapes. Figure 6 provides the S12 plot of the two adjacent elements of the 4 port—a 4 element electric dipole array with different fence shapes, showing that the mutual coupling between the closest two dipole elements was less than  $-21$  dB for the  $\lambda_d \times \lambda_d$  rectangular fence, the U-fence, and the  $115^\circ$  tapered V-fence cases, indicating minimal interaction between the different dipole elements. However, the S12 degraded for the case of the  $1.2\lambda_d \times \lambda_d$  rectangular fence. This is another reason why it is better to use fence shaping over resizing the rectangular fence when a higher gain is required.

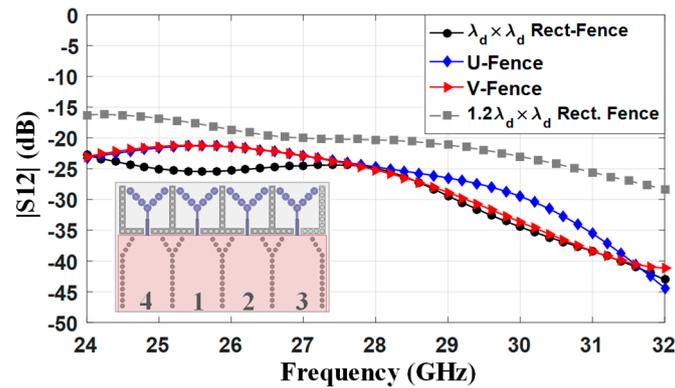


Figure 6. The simulated |S12| of the adjacent dipole array elements for the different fence shapes.

### 3. The Measurement and Simulated Results

The fabricated prototypes are shown in Figure 7, where a single element,  $2 \times 1$ , and  $4 \times 1$  arrays were fabricated for each of the  $\lambda_d \times \lambda_d$  rectangular fence, the U-fence, and the  $115^\circ$  V-fence dipoles. For the sake of testing the arrays, an SIW divider was employed. Practically, the SIW divider will not be needed where every antenna element is directly connected on the PCB to a pin of the RF phase shifter required to provide the appropriate phase shifting for beam steering. The measured/simulated radiation patterns of the fabricated prototypes are shown in Figure 8 at 28 GHz, where the  $4 \times 1$  array achieved a measured gain/HPBW<sub>EI</sub>/side-lobe level (SLL) of 12.6 dBi/133.1°/10.6 dB, 13.5 dBi/118°/14.6 dB and 14.2 dBi/104°/13.1 dB for the rectangular-, U-, and V-fences, respectively. The S11 parameters of the dipole with rectangular, U-, and V-shaped fences in Figure 9 show a simulated/measured bandwidth of 6.94/7.23 GHz, 6.6/6.5 GHz, and 6.4/6.42 GHz, respectively. Figure 10 shows the simulated and measured gain/directivity of the fabricated prototypes over the operating bandwidth. Table 2 provides a comparison of the proposed dipole array, with state-of-the-art mmWave linearly polarized mobile device antenna arrays showing superior performance from the proposed dipole.

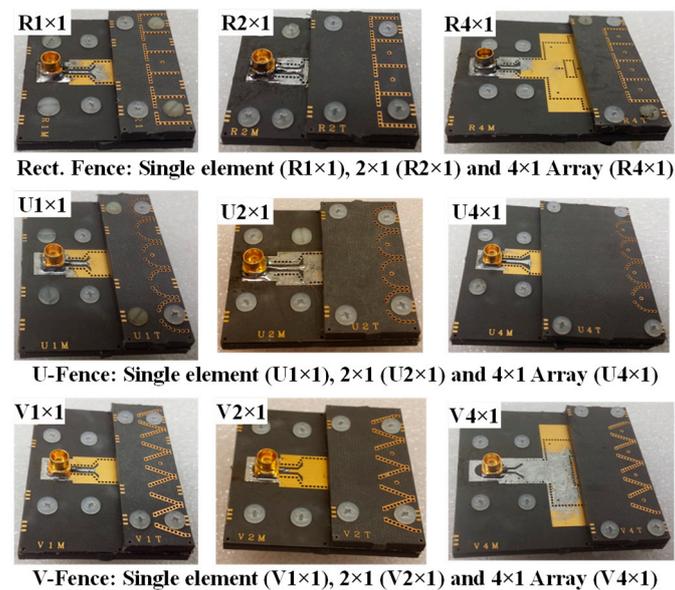


Figure 7. The fabricated antennas prototypes.

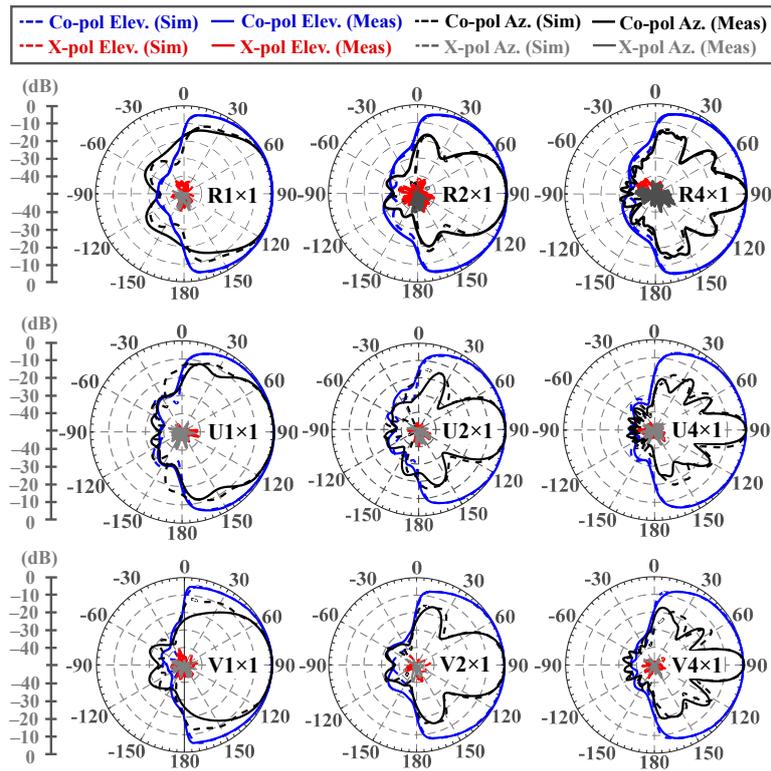


Figure 8. The simulated/measured radiation patterns at 28 GHz.

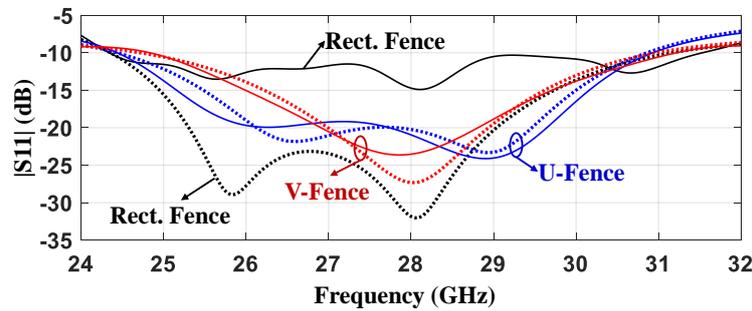


Figure 9. The measured (solid line) and simulated (dotted line)  $S_{11}$  plots for the single element dipoles.

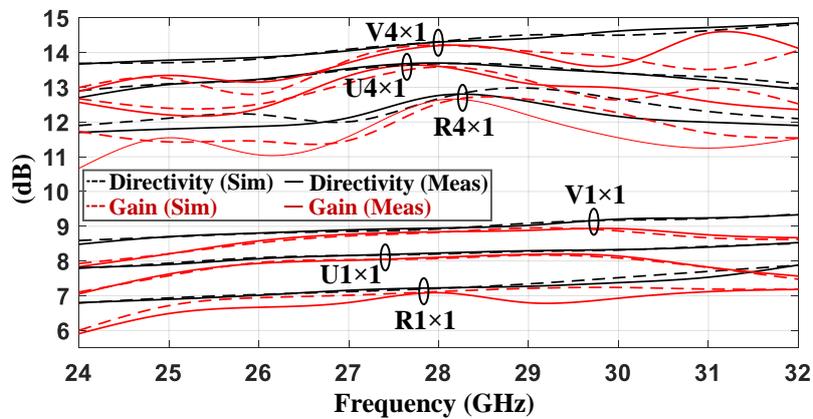


Figure 10. The simulated/measured gain/directivity versus frequency for the fabricated prototypes.

**Table 2.** Comparison with state-of-the-art 28 GHz linearly polarized mobile device antennas.

	Structure	BW (GHz)	Gain (dBi)	HPBW <sub>El</sub>	F/B (dB)	X-pol (dB)	Size
[12]	16 × 1 mesh grid array	3	10.9	109°	15	N/A	8.32λ <sub>d</sub> × 1.06λ <sub>d</sub> × 0.2λ <sub>d</sub>
[14]	11 dipoles + Horn	11	9–12	60°	10–20	<−25	4.5λ <sub>d</sub> × 6.57λ <sub>d</sub> × 0.86λ <sub>d</sub>
[15]	16 × 1 slot array	2.5	15	70°	10	N/A	7.1λ <sub>d</sub> × 0.21λ <sub>d</sub> × 0.55λ <sub>d</sub>
This Work	Rect-fence [16]	7.23	12.61	133.1°	36.6	<−39.8	3.84λ <sub>d</sub> × 0.94λ <sub>d</sub> × 0.67λ <sub>d</sub>
	U-fence	6.5	13.5	118°	36.1	<−41.1	4.36λ <sub>d</sub> × 0.95λ <sub>d</sub> × 0.67λ <sub>d</sub>
	V-fence	6.42	14.2	104°	36.2	<−41.3	4.33λ <sub>d</sub> × 0.97λ <sub>d</sub> × 0.67λ <sub>d</sub>

#### 4. Conclusions

In this work, fence shaping for substrate-integrated electric dipole antennae was presented. The concept of fence shaping and tapering was discussed with the aid of V-shaped fence and U-shaped fence dipole antennas, for which the performances were compared with the conventional rectangular fence dipole antenna. By fence shaping, as an additional degree of freedom in the design, one can modulate the radiation performance of the antenna while achieving a gain and HPBW<sub>El</sub> of at least 12.6 dBi and 104° from a 4 × 1 array, respectively. Overall, the proposed structure achieved excellent and stable radiation performance over a wide frequency bandwidth, making it suitable for multiple high-band 5G applications.

**Author Contributions:** The authors contributions towards this research article is as follows; conceptualization, W.E.-H., R.M. and P.M.; methodology, W.E.-H., R.M. and P.M.; validation, W.E.-H.; formal analysis, W.E.-H.; investigation, W.E.-H., R.M. and P.M.; resources, J.M and P.M. writing—original draft preparation, W.E.-H.; writing—review and editing, W.E.-H., R.M. and P.M.; supervision, R.M, M.H and P.M.; project administration, P.M.

**Funding:** This research was funded by TELUS Communications.

**Conflicts of Interest:** The authors declare no conflict of interest.

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