



Article Soil Erosion Prediction Based on Moth-Flame Optimizer-Evolved Kernel Extreme Learning Machine

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Abstract: Soil erosion control is a complex, integrated management process, constructed based on unified planning by adjusting the land use structure, reasonably configuring engineering, plant, and farming measures to form a complete erosion control system, while meeting the laws of soil erosion, economic and social development, and ecological and environmental security. The accurate prediction and quantitative forecasting of soil erosion is a critical reference indicator for comprehensive erosion control. This paper applies a new swarm intelligence optimization algorithm to the soil erosion classification and prediction problem, based on an enhanced moth-flame optimizer with sinecosine mechanisms (SMFO). It is used to improve the exploration and detection capability by using the positive cosine strategy, meanwhile, to optimize the penalty parameter and the kernel parameter of the kernel extreme learning machine (KELM) for the rainfall-induced soil erosion classification prediction problem, to obtain more-accurate soil erosion classifications and the prediction results. In this paper, a dataset of the Vietnam Son La province was used for the model evaluation and testing, and the experimental results show that this SMFO-KELM method can accurately predict the results, with significant advantages in terms of classification accuracy (ACC), Mathews correlation coefficient (MCC), sensitivity (sensitivity), and specificity (specificity). Compared with other optimizer models, the adopted method is more suitable for the accurate classification of soil erosion, and can provide new solutions for natural soil supply capacity analysis, integrated erosion management, and environmental sustainability judgment.

Keywords: sine–cosine algorithm; moth-flame algorithm; kernel extreme learning machine; parameter optimization; soil erosion prediction

1. Introduction

With over 98.8% of the world's human food coming from the land and less than 1.2% from marine, aquatic ecosystems, protecting arable land and maintaining soil fertility is vital to human well-being [1,2]. Soil erosion is one of the most critical threats to the world's food production [3–5]. Globally, about ten million hectares of arable land are lost each year due to soil erosion, resulting in less arable land available for world food production [6]. The loss of arable land is a serious problem; according to the World Health Organization, and Food and Agriculture Organization of the United Nations (FAO) reports, two-thirds of the global population is still undernourished [7]. Soil erosion is the process



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). by which soil particles and surface appurtenances are eroded, moved, and deposited by the interaction of a number of factors [8]. Soil erosion can be divided into hydraulic erosion, cultivation erosion, wind erosion, freeze–thaw erosion, and gravity erosion [9,10]. Soil erosion leads to numerous serious hazards, directly causing soil acidification, soil sanding, soil consolidation, and water pollution.

In contrast, soil erosion will diminish the productivity of terrestrial ecosystems; soil erosion will result in increased water runoff, which decreases water infiltration and the soil's water storage capacity. In addition, during erosion, organic matter and essential plant nutrients are reduced, and the depth of the soil nutrient layer is reduced; all these changes can depress plant growth, and decrease valuable biota and the overall biodiversity of the soil [11–13]. These factors interact to create soil erosion, which is a major environmental problem shared globally. China is one of the countries with the most serious soil erosion, with 4.92 million km² of soil erosion nationwide, accounting for 51% of the total land area, including 1.79 million km² of hydraulic erosion, accounting for 36% of the total soil erosion area [11]. The most significant threat to soil erosion in the country is hydraulic erosion. The main cause of hydraulic erosion is rainfall, where raindrops hit the soil and loosen the soil particles, and where the soil tilt deviates by a percentage of 2%; the soil starts to move downhill, and the impact of erosion is felt on all slopes, with more topsoil being carried away as water moves downslope into valleys and streams, causing erosion [14]. The accurate prediction of soil erosion is key to help address soil conservation and management efforts, and is an important guide to quantitative soil erosion prediction, soil and water planning, and other integrated soil erosion management.

There are many causes of soil erosion, such as geological features, climate, soil, vegetation, hydrology, and many other factors that influence it. A large number of research scholars, at home and abroad, have conducted studies on soil erosion, and the models that are currently available, such as the universal soil loss equation (USLE) model [15], Revised Universal Soil Loss Equation (RUSLE) model [16], AGricultural Non-Point Source Pollution (AGNPS) model [17], Annualized Agricultural Non-Point Source Pollutant (AnnGNPS) model [18], water erosion prediction project (WEPP) model [19], and artificial neural network (ANN) model [20,21] and Artificial Neural Network (ANN) model [22-24], etc. Traditional models have poor computational accuracy and robustness, and do not meet the criteria of real needs. It can be observed that the research into soil erosion has moved from simple models to machine learning models, and in recent years there have been many new machine learning classification methods for soil erosion problem prediction. Dinh et al. [25,26] proposed the following two methods: the first is a proposed method for predicting soil erodibility based on a combination of multivariate adaptive regression splines and the social spider algorithm; the other is a method for predicting soil erodibility based on adaptive differential evolution and support vector classification. Fathizad et al. [27] put forward a random forest model with a set of covariates that were used to model the spatial and temporal dynamics of soil quality in the central Iranian desert, where the coefficient of determination between the soil quality index and the covariates was set to 0.69. Chen et al. [28] developed the different predictive performance of the boosted linear model (BLM), boosted regression tree, boosted generalized linear model, and deep boosting models, for piping erosion susceptibility mapping in Zarandieh watershed, which is located in the Markazi province of Iran. Chowdhuri [29] investigated gully erosion susceptibility maps using the machine learning algorithms, including the boosted regression tree, Bayesian additive regression tree, support vector regression, and the ensemble of the SVR-Bee algorithm. Lee et al. [30] used decision tree, K-nearest neighbors, random forest, gradient boosting, extreme gradient boost, and the deep neural network to evaluate the rainfall erosivity factor estimation. Nguyen et al. [31] proposed multivariate adaptive regression splines and random forest, and the boosting method includes cubist and gradient boosting machines.

Although research in machine learning has been carried out in various fields for many years, it is evident, in the soil erosion classification problem, that its application is still in relatively simple machine learning classification, such as support vector machine (SVM) [32], k-Nearest Neighbor (KNN) [33], Random Forest (RF) [34], Gradient boosting (GB) [35] and Extreme Gradient Boost (EGB) [36] etc. The KELM is a recent classification prediction model proposed by G. Huang et al. [37] in 2011. The extreme learning machine introduces the idea of the kernel, which guarantees a better generalization performance, similar to SVM but with better generalization ability than SVM. It is a derivative of Extreme Learning Machine (ELM) [38], a class of machine learning systems or methods built on Feedforward Neuron Network for supervised and unsupervised learning problems. Shan et al. [39] suggested a hybrid artificial fish particle swarm optimizer and KELM for the type-II diabetes predictive model. Cai et al. [40] proposed Label Rectification Learning through KELM. Zhang et al. [41] presented a prospective bankruptcy prediction model based on LSEOFOA and KELM. Yu et al. [42] proposed an improved butterfly optimizer algorithm optimized KELM model that was used to timely and accurately offered a dependable basis for identifying the rolling bearing condition in the real production application. Shan et al. [43] proposed that WEMFO was also applied to train KELM; the resultant optimized WEMFO-KELM model was used to solve six clinical disease classification problems.

As we can observe from the above study, machine learning is constrained by parameter settings. Swarm intelligence optimization algorithms are usually used as a good candidate to optimize the parameters of individual machine learning classifiers, to obtain higher classification accuracy. The swarm intelligence optimization algorithm simulates the behavior of groups of insects, animals, birds, and fish, which cooperatively search for food [44–49]. Each group member constantly changes the direction of their search by learning from its own experience and the experience of other members [50–59]. Any algorithm or distributed problem-solving strategy inspired by insect groups or other mechanisms of animal social behavior is part of swarm intelligence [60–63]. These optimizers can be generally classified based on many criteria [64,65]. The classical group-wise optimization algorithms are the firefly algorithm (FA) [66], Runge Kutta method (RUN) (https://aliasgharheidari.com/ RUN.html (accessed on 25th August 2021)) [67], gravitational search algorithm (GSA) [68], whale optimizer (WOA) [69,70], moth-flame optimizer (MFO) [69], bat algorithm (BA) [71], Harris hawks optimizer (HHO) (https://aliasgharheidari.com/HHO.html (accessed on 25 August 2021)) [72], fruit fly optimization algorithm (FOA) [73–75], slime mould algorithm (SMA) (https://aliasgharheidari.com/SMA.html (accessed on 25 August 2021)) [76], Hunger games search (HGS) (https://aliasgharheidari.com/HGS.html (accessed on 25 August 2021)) [77], differential evolution (DE) [78], continuous ant colony optimization (ACOR) [79], multi-verse optimizer (MVO), particle swarm optimizer (PSO) [80,81], simulated annealing algorithm (SA) [82,83], sine cosine algorithm (SCA) [69], and grasshopper optimization algorithm(GOA) [69,84], etc. However, we should notice that some of these methods' originality, such as GWO, BAT, and FA, is not high and criticized in several papers [44,85,86]. Meanwhile, there are many corresponding improvement algorithms, such as enhanced comprehensive learning particle swarm optimizer(GCLPSO) [87], random spare ant colony optimization (RCACO) [88], enhanced whale optimizer with associative learning (BMWOA) [89], enhanced GWO with a new hierarchical structure (IGWO) [48], hybridizing grey wolf optimization (HGWO) [90], boosted GWO (OBLGWO) [91] and ant colony optimizer with random spare strategy and chaotic intensification strategy (CCACO) [88], etc. MFO is a novel meta-heuristic algorithm for solving optimization problems. The main inspiration for this optimization is the method of navigation used by moths in nature, namely, lateral orientation. Night moths fly by maintaining a fixed angle relative to the moon, which is a very efficient mechanism for moving long distances in a straight line. The MFO algorithm is widely used in many engineering and optimization problems, but the principles and structure of the MFO algorithm are relatively simple [92,93]; it suffers from the pool exploration problem and is prone to falling into local or deceptive optimization (LO) during successive iterations. Many researchers have recently worked on adding improved mechanisms based on the MFO algorithm to address these problems. This paper uses a novel SMFO [94] algorithm that introduces a sine-cosine strategy into

MFO, thus further improving the detection capability. The exploratory and exploitative nature of the method and the convergence pattern are significantly improved, and are validated in engineering optimization problems.

The framework of this paper is schematically shown in Figure 1 below. This paper uses the SMFO-KELM approach, choosing a dataset of 236 samples from the Son La province of Vietnam, and constructing a prediction and validation model using ten explanatory factors as features. Firstly, we use the five-fold crossover method for optimizing the parameter settings of the KELM; secondly, we use the ten-fold crossover validation method for classifying soil erosion predictions; and finally, we compare six original algorithm models, such as BA-KELM models, and four improved algorithm models, such as CLOFOA-KELM. The experimental results show that the adopted SMFO-KELM method can obtain much higher soil erosion classification prediction results.



Figure 1. The framework of this paper.

In summary, the main contributions of this paper are as follow:

1. A new and improved swarm intelligence optimization algorithm SMFO combined with the machine learning model KELM is proposed.

2. SMFO is applied for the first time, applied to optimize and determine key parameters in KELM.

The first application of SMFO-KELM to a soil erosion classification prediction model.

4. SMFO-KELM classification prediction results of soil erosion are significantly higher than other algorithms, in the following four aspects: accuracy, Matthews correlation coefficient, sensitivity, and specificity.

The chapters of this paper are structured as follows: Section 2 presents the materials and methods, mainly including the methods SMFO, KELM, and the dataset. Section 3 presents the experimental results and evaluation indicators. Section 4 is the discussion and outlook section.

2. Materials and Methods

2.1. Dataset

This paper uses a soil dataset from two limited experimental areas eroded by heavy rainfall in the north-western city of Vietnam—Son La Province, during three years from 2009 to 2011 [26], shown in Appendix A Table A1. The area has a tropical monsoon climate with higher levels of soil erosion from heavy rainfall than at other latitudes, so the area chosen as the site for the experiment has apparent contrasting data. The 4 m \times 18 m plots were selected as unit plots, and there are 24 such plots; the shape of the plots was chosen randomly without restriction. In order to ensure the accuracy of data acquisition, the explanatory factor data were acquired using surface runoff subsurface set water pipes, OC measurements with the carbonate component removed followed by a C/N analyzer, transect methods for coverage, and interpolation techniques for residues, respectively. Cultivation methods, fertilizer application, and soil conservation measures are all based

on the traditional farming practices of local farmers. Based on the multi-model for soil erosion prediction as a comprehensive reference and the experimentally obtained data, the following ten explanatory variables were identified as explanatory factors for conducting soil erosion classification, as shown in Table 1 below.

Factors	Unit	Variables	Min	Max	Mean	Std.
EI30	%	X ₁	0.00	3008.93	134.77	385.10
Slope degree	%	X ₂	24.83	34.77	28.85	2.39
OC topsoil	%	X3	0.89	2.79	1.86	0.56
pH topsoil	%	X_4	5.13	7.06	5.75	0.56
Bulk density	g/cm ³	X_5	1.23	1.58	1.39	0.08
Topsoil porosity	- %	X ₆	46.34	59.48	52.36	3.15
Topsoil texture (silt fraction)	%	X ₇	31.35	37.71	33.82	1.48
Topsoil texture (clay fraction)	%	X_8	18.61	38.35	30.03	4.67
Topsoil texture (sand fraction)	%	X9	29.66	46.51	36.15	4.12
Soil cover rate	%	X ₁₀	1.05	99.71	53.51	25.36

Where EI30 is the extended peak rate of disengagement and runoff over 30 min. The following formula gives the storm energy *E*:

$$E = 1099[1 - 0.72\exp(-1.27i)] \tag{1}$$

where *i* is the 30-min maximum intensity. The multiplication of *E* and I 30 provided the dynamic rainfall energy (EI), a combination of the total and peak intensities in each storm. This number represents the combination of particles detachment and transport capabilities.

Slope degree is the degree of slope in the terrain, i.e., the length and gradient of the slope. It is a key factor in soil erosion. The steeper and longer the slope, the more runoff accumulation it causes and the greater the probability of soil erosion. These data were collected using a Nikon Forestry (550) inclinometer to measure the slope of the plots.

Soil erodibility is also affected by permeability, structure, organic materials, and pH value. Two simple soil characteristics, OC (organic carbon) and pH, were used to apply interpretive parameters to soil erodibility. OC was obtained with a C/N analyzer (minus HCL), and pH was measured with a glass electrode using water-to-soil ratio of 2.5:1.

Bulk density, topsoil porosity, topsoil texture (silt fraction, clay fraction, sand fraction), and soil cover rate are important influencing factors normally used by traditional models [95].

In the model prediction of soil erodibility, we ultimately aim to classify the samples (related to each vector of the value of explanatory variables) into two categories, namely, the following: "erosion category" or "non-erosion category". To ensure the accuracy of the experimental classification, we used the same criteria for soil loss as in [96], with samples that lost more than 3 tons of soil per hectare being defined as 'erosive' and vice versa as 'non-erodible'. The experimental data consisted of 236 data samples, with 50% erosion and 50% non-erosion.

2.2. KELM

Kernel function-based extreme learning machine (KELM), the extreme learning machine (ELM) algorithm, was combined with a kernel function to replace the feature mapping of the implicit layer in ELM with a kernel function to form a kernel function-based ELM algorithm. Because of the kernel function, the data features were up-dimensioned and therefore could be divided more precisely.

ELM is a novel fast learning algorithm of single hidden-layer neural networks that randomly initialize the input weights and biases, and obtains the corresponding output weights. For every single hidden-layer neural network, assume that there are *N* arbitrary

samples (x_i, t_i) , where $X_i = [x_{i1}, x_{i2}, \dots, x_{in}]^T \in \mathbb{R}^n$, $t_i = [t_{i1}, t_{i2}, \dots, t_{im}]^T \in \mathbb{R}^m$. A single hidden *L* layer neural network with one hidden layer node can be represented as follows:

$$\sum_{i=1}^{L} \beta_i g(W_i \cdot X_j + b_i) = o_j, i = 1, 2, \cdots, N; j = 1, 2, \cdots, N$$
(2)

where g(x) is the activation function, $W_i = [w_{i,1}, w_{i,2}, \cdots, w_{i,n}]^T$ is the input weight, β_i is the output weight and b_i is the bias of the *i*th hidden-layer unit. $W_i \cdot X_j$ denotes the inner product of W_i and X_j .

Minimal error in the output is the goal of single hidden-layer neural network learning, expressed as follows:

$$\sum_{j=1}^{N} ||o_j - t_j|| = 0$$
(3)

 β_i , w_i , and b_i exist, such that the following applies:

$$\sum_{i=1}^{L} \beta_i g(W_i \cdot X_j + b_i) = t_j \ j = 1, 2, \cdots, N$$
(4)

It can be matrixed as follows:

$$I\beta = T \tag{5}$$

where *H* is the hidden-layer node output, β is the weight of output, and *T* is the output of desired.

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$$H(W_{1}, W_{2}, \cdots, W_{L}, b_{1}, b_{2}, \cdots, b_{L}, X_{1}, X_{2}, \cdots, X_{L}) = \begin{bmatrix} g(W_{1} \cdot X_{1} + b_{1}) & \cdots & g(W_{L} \cdot X_{1} + b_{L}) \\ \vdots & \ddots & \vdots \\ g(W_{1} \cdot X_{N} + b_{1}) & \cdots & g(W_{L} \cdot X_{N} + b_{L}) \end{bmatrix}_{N \times L}$$
(6)

where $\beta = [\beta_{1m}, \beta_{2m}, \cdots, \beta_{Lm}]^T$, $T = [t_{1m}, t_{2m}, \cdots, t_{Nm}]^T$.

In order to be able to train a single hidden-layer neural network, we want to obtain \hat{W}_i , \hat{b}_i , and the following:

$$||H(\hat{W}_{i},\hat{b}_{i})\hat{\beta}_{i} - T|| = \min_{W,b,\beta} ||H(W_{i},b_{i})\beta_{i} - T||$$
(7)

where $i = 1, 2, \dots, N$, which is equivalented to minimizing the loss function.

$$E = \sum_{j=1}^{N} \left(\sum_{i=1}^{L} \beta_i g \left(W_i \cdot X_j + b_i \right) - t_j \right)^2$$
(8)

Some traditional gradient descent-based algorithms can solve such problems, but the basic gradient-based learning algorithms require all parameters to be adjusted during the iterative process. In the ELM algorithm, once the input weights W_i and the bias of the hidden layer b_i are determined randomly, the output matrix of the hidden layer H is determined uniquely. Training a single hidden-layer neural network could be transformed into solving a linear system $H\beta = T$. Moreover, the output weights β can be determined as follows:

$$\hat{\beta} = H^+ T \tag{9}$$

where H^+ is the Moore–Penrose generalized inverse of the matrix. Meanwhile, there is $H^+ = H^T (HH^T)^{-1}$. Moreover, it can be shown that the norm of the resulting solution $\hat{\beta}$ is minimal and unique. As a result, it can help achieve a powerful performance in generalization and significantly increase learning speed.

Kernel-based ELM was proposed in order to improve the ability of the ELM to generalize and outperform the least square-based ELM, and it is proposed to add a positive constant *C* to the diagonal of H^T , which is used to calculate the output weight β , we have the following:

$$\beta = H^T \left(\frac{I}{C} + HH^T\right)^{-1} T \tag{10}$$

where the coefficient *C* is the penalty parameter, whereas *I* is the identities matrix. Hence, the output function is defined below:

$$f(x) = h(x)H^T \left(\frac{I}{C} + HH^T\right)^{-1} T$$
(11)

A kernel matrix of the ELM is obtained by the following:

$$\Omega_{ELM} = HH^T : \ \Omega_{ELMi,j} = h(x_i)h(x_j) = K(x_i, x_j)$$
(12)

where $K(x_i, x_j)$ is one kind of kernel function. For the output function, then there is the following:

$$f(x) = \begin{bmatrix} K(x, x_1) \\ \vdots \\ K(x, x_N) \end{bmatrix}^{-1} \left(\frac{I}{C} + \Omega_{EML}\right)^{-1} T$$
(13)

The kernel implementation of the ELM, called KELM, has better stability and generalization capabilities than the basic ELM. The structure of the KELM model is schematically shown in Figure 2, where the kernel function acts as an alternative feature mapping function used to achieve the same mapping from the information input to the feature space. Hence, the neural network's output is independent of the feature mapping of the hidden layer, but depends on the kernel function, which is explicitly provided. Both the feature mapping of the hidden layer and the dimensionality of the feature space are not pre-defined.



Figure 2. The structure diagram of the KELM model.

In this paper, use the Gaussian kernel function as the kernel function of KELM with the following formula:

$$K(u,v) = exp\left(-\gamma ||u-v||^2\right)$$
(14)

the penalty parameter *C* and the kernel parameter γ are two critical parameters in the KELM model. The penalty parameter *C* defines the balancing act between the minimal

fitting error and the model's sophistication, and the kernel parameter γ determines the nonlinear mapping from the input space to a specific high-dimensional hidden-layer feature space. In general, these two main parameters can be optimized by using appropriate optimization algorithms in order to improve the performance of KELM better.

KELM is widely used to solve problems in areas such as parameter optimization and model prediction because of its significant advantages in learning speed and generalization ability.

2.3. SMFO

2.3.1. MFO

The basic MFO was proposed in 2015 [47], intended to be a swarm intelligence optimization algorithm based on moths' spiral flight path mechanism in flight.

MFO is an evolution of the moth lateral positioning navigation mechanism found in nature. At night, moths fly using the distant moon as a reference, which can be considered as parallel light, and the moths adjust their flight direction according to the direction of the light to the angle between themselves. Due to the proximity of the artificial flame, the moths fly at a fixed angle to the flame, and the distance between the moth and the flame changes continuously, eventually producing a flight path that spirals closer to the flame [97]. The MFO algorithm has strong parallel optimization capabilities and good overall properties for non-convex functions; the MFO algorithm can explore the search space extensively and find regions with a greater probability of global optimality, as non-convex functions have a large number of local optimality points [98–100].

By definition, moths and flames are two important components of the MFO algorithm. We can observe this from Figure 3 above. The moths fly in *d*-dimensional hyper plane (d = 1, 2, 3), search agents store their position in the matrix \vec{M} , and store the fitness value of each moth in array *OM*. The flames are the best position that the moth had reached so far, then they are stored in matrix \vec{F} . The fitness values of flames are stored in array *OF*. Every moth updates its position depend on its flame, then the equation is as follows:

$$\vec{M}_i = \vec{S} \left(\vec{M}_i, \vec{F}_j \right) \tag{15}$$

where M_i indicate the *i*-th moth, F_j is the *j*-th flame after sorting, and S is the spiral function. This spiral function should fulfill the conditions below:

(1) The vector position of the initial point of the *S* function needs to be given first before the MFO algorithm can perform the corresponding calculation.

(2) Before the end of each iteration of the MFO algorithm, the *S* function should preserve the location of the optimal solution found in this iteration.

(3) The function's magnitude is between the upper bound vector *ub* and the lower bound vector *lb*. Considering these points, the equation is defined as follows:

$$\vec{S}\left(\vec{M}_{i},\vec{F}_{j}\right) = \vec{D}_{i} \cdot e^{bt} \cdot \cos(2\pi t) + \vec{F}_{j}$$
(16)

where *b* is logarithmic helix shape constant, *t* is values in the range [-1,1], D_i is the distance of the *i*-th moth to the *j*-th flame, it can be calculated as follows:

$$\vec{D}_i = \left| \vec{F}_j - \vec{M}_i \right| \tag{17}$$

The *t* parameter determines the step size of the moth's next movement. Equation (16) has limitations, as it only defines how the moth flies towards the flame, which makes the MFO algorithm easily fall into a local optimum. To avoid this problem, an adaptive update of the flame is required, and the number of flames is gradually reduced, reducing the

computation time and improving the operation efficiency. The updated formula of the flame is shown in Equation (18) as follows:

$$flame_{no} = \operatorname{round}\left(N - k * \frac{N-1}{T}\right)$$
 (18)

where k is the number of current iterations, N is the maximum flame counts, and T indicates the maximum iterations. When the end-of-iteration condition is satisfied, the best moth is returned as the best obtained value.



Figure 3. The flight path of moths.

2.3.2. SMFO

SMFO [94] improves the global exploration capability of MFO by incorporating the SCA, which increases the diversity of initial solutions and frees the solutions from local distress. At the same time, the adjustment parameters in the positive cosine strategy increase the accuracy of the optimal solution.

The core of the sine and cosine strategy (SCA) is to modify the position of the initial state through the change in the mathematical function [101–103], which is shown in Figure 4. The update of individual positions in the population relies on changes in the value of the sine and cosine function to randomly update the position of each individual in each iteration by using a multi-parameter adjustment, to ensure that the population remains diverse in the early stages and that individuals tend to localize in the later stages, eventually converging to the optimal solution. During each iteration, the state of the individual is updated using the following formula:

$$\overrightarrow{X}_{i}^{t+1} = \begin{cases} \overrightarrow{X}_{i}^{t} + r_{1} \times \sin(r_{2}) \times |r_{3}\overrightarrow{P}_{i}^{t} - \overrightarrow{X}_{i}|, r_{4} < 0.5\\ \overrightarrow{P}_{i}^{t} - \overrightarrow{X}_{i}^{t} + r_{1} \times \cos(r_{2}) \times |r_{3}\overrightarrow{P}_{i}^{t} - \overrightarrow{X}_{i}|, r_{4} \ge 0.5 \end{cases}$$

$$(19)$$

where X_i^{i} is the position of the location of the current solution in *i*-th dimension at *t*-th iteration (solution), P_i^{i} is the position of the location of the current optimal solution in *i*-th dimension at *t*-th iteration (destination), whereas $| \cdot |$ denotes the absolute value.



Figure 4. The basic principle of sine-cosine strategy.

The parameter r_1 defines whether the next position is searched between the solution and the destination or beyond. It enhances the MFO algorithm global exploration capability. Parameter r_2 determines the next position update step. r_3 is a random weight with a range of values that decide the impact of the target destination on the current solution. r_4 is the random probability of switching between the sine and cosine function. The recurring pattern of sine and cosine functions makes one solution relocate around another. To ensure the use of the space that is identified between the two solutions, Equation (20) is introduced as follows:

$$r_1 = a - t \frac{u}{T} \tag{20}$$

where *t* is the current number of iterations, *T* is the maximum number of iterations, and *a* is a constant, generally set to 2. This formula can adaptively adapt the size of the parameters for the exploration to gradually converge to the global optimum.

2.4. SMFO-KELM for Soil Erosion Prediction Method

The performance of models in machine learning is often closely related to hyperparameters. Initially, the "optimal" hyperparameter is usually found by manual trial to find the best hyperparameter. However, the approach is inefficient, so swarm intelligence optimization has been proposed to find the optimal hyperparameters. From the experiments mentioned above comparing SMFO with other swarm intelligence optimization algorithms, it can be observed that the proposed SMFO is significantly better than other similar algorithms, in terms of exploration and detection capability, with competitive convergence and balance effect, and it has undeniable advantages in the optimization of SMFO in engineering problems [94]. The penalty parameters and kernel parameters of the SMFO optimized machine learning method kernel extreme learning machine are used to make more-accurate classification predictions for soil erosion classification prediction. Figure 5 shows the proposed SMFO-KELM soil erosion classification prediction model flowchart, which is mainly applied in the following two processes: model optimization and classification evaluation. As with the machine learning validation approach, to obtain reliable and unbiased results, the validation of the classification evaluation model uses a ten-fold crossover to evaluate the classifier's performance, where nine are the test set, and one is the validation set. At the same time, the process of optimizing the two parameters of the classifier uses a five-fold crossover validation, where five are the test set, and five are the validation set. This experimental scheme can help to obtain unbiased estimates of generalization accuracy and reliable results. The final evaluation of the metrics is carried out by accuracy (ACC), Matthews correlation coefficient (MCC), sensitivity, specificity. Due to random sampling, single 10-fold cross-validation will not be representative of the accuracy of the classification. Therefore, the results of 10 10-fold crossover runs are run for all methods to be averaged as the final result of the evaluation.

Two hundred and thirty-six soil erosion binary classification datasets from Son La city of Vietnam were used to evaluate the SMFO-KELM model with ten explanatory factors of EI30, slope degree, OC topsoil, pH topsoil, bulk density, topsoil porosity, topsoil texture (silt fraction), topsoil texture (clay fraction), topsoil texture (sand fraction), and soil cover rate as factors for classification assessment and SMFO for the KELM hyperparameter selection stage optimization of the penalty parameter c and the kernel parameter γ .



Figure 5. Soil erosion prediction model flowchart based on SMFO-KELM.

2.5. Experimental Environment

To ensure the fairness and validity of the experiments [62,64,104,105], all the algorithms involved in the comparison in all experiments were conducted under the same experimental conditions. The population size was set to 20, the maximum number of evaluations MaxFEs was uniformly set to 100, and all algorithms were tested 30 times independently to reduce the influence of random conditions. The searching spaces of the two hyperparameters in KELM were set to $C \in \{2^{-15}, \dots, 2^{15}\}$ and $\gamma \in \{2^{-15}, \dots, 2^{15}\}$. All experimental results were evaluated using box plots with the following four metrics: ACC, MCC, sensitivity, and specificity.

All experiments were performed on a computer with a 3.40 GHz Intel[®] Core i7 processor and 16 GB RAM; the coding was conducted using Matlab2018b.

2.6. Measures for Performance Evaluation

For a binary classification problem, the actual values are only positive and negative, and the actual predicted results will only have two values, 0 and 1. If an instance is positive and is predicted to be positive, it is true positive; if it is negative and is predicted to be positive, it is false positive, and if it is negative and is predicted to be negative, it is a true negative, and if it is positive and is predicted to be negative, it is a false negative. The most widely used classifications based on the above are ACC, MCC, sensitivity, and specificity [106,107], which are used to assess the quality of the binary classification and evaluate the proposed method's performance.

$$ACC = \frac{TP + TN}{TP + FP + FN + TN} \times 100\%$$
(21)

$$MCC = \frac{TP \times TN - FP \times FN}{\sqrt{(TP + FP) \times (TP + FN) \times (TN + FP) \times (TN + FN)}} \times 100\%$$
(22)

$$sensitivity = \frac{TP}{TP + FN} \times 100\%$$
(23)

$$specificity = \frac{TN}{FP + TN} \times 100\%$$
(24)

The MCC is essentially a correlation coefficient between the actual classification and the predicted classification, which can range from a value of 1, which indicates a perfect prediction of the subject, to a value of 0, which indicates that the prediction is not a good random prediction, and -1, which means that the predicted classification and the actual classification do not agree at all. Sensitivity (also known as true positive rate) is the proportion of samples that are positive that are judged to be positive, and specificity (also known as true negative rate) is the proportion of samples that are actually negative that are judged to be negative.

3. Results

Figure 6 shows the results of a comparison between SMFO-KELM and the six classical primitive optimization algorithm classifiers MFO-KELM, BA-KELM, GSA-KELM, MVO-KELM, GOA-KELM, and WOA-KELM, on a two-classification dataset of 236 features, consisting of 10 features in the Son La province. These boxplots show that SMFO-KELM obtained the best performance, in terms of ACC, MCC, sensitivity, and specificity. The values obtained by BA-KELM, for all four metrics, ranked last. Furthermore, MVO-KELM produced lower values for all four metrics, in terms of ACC, MCC, and specificity, except for sensitivity, which means that MVO-KELM may be less effective in predicting soil erosion than the other comparative methods. Furthermore, WOA-KELM produced better means than BA-KELM, MFO-KELM, GSA-KELM, GOA-KELM, and MVO-KELM, in terms of ACC, MCC, and specificity.

Figure 7 shows the performance of SMFO-KELM against four other advanced and improved algorithmic classifiers in four metrics. It can be observed, very clearly, that SMFO-KELM performs better than the other competitors in all four metrics. Except for SMFO-KELM, HGWO-KELM outperformed the other ACC, MCC, and sensitivity competitors, followed by OBLGWO-KELM, IGWO-KELM, and CLOFOA-KELM, who achieved average values, in terms of ACC, MCC, sensitivity, and specificity, which were lower than the other classifiers. This shows that the CLOFOA-ELM classifier is not a good choice for soil erosion classification problems.



Figure 6. Boxplot of SMFO-KELM and its classical primitive algorithm competitors of ACC, MCC, sensitivity, and specificity on Son La dataset.



Figure 7. Boxplot of SMFO-KELM and its advanced algorithm competitors of ACC, MCC, sensitivity, and specificity on Son La dataset.

It is clear from Figures 6–8 that the SMFO-KELM classifier generally outperforms the other competing models in comparing classical optimized and advanced algorithmic classifiers, since the SMFO optimizer that was used has the highest optimization power. All the experimental results can be viewed in Appendix A Table A2. The improved KELM using HGWO does not achieve champion classification performance; nevertheless, it is a second-top optimizer in the competition. As per the features of the proposed model, the efficacy of the proposed MFO method can be further investigated in dealing with more complex problems, such as social recommendation and QOS-aware service composition [108–110], energy storage planning and scheduling [111], image editing [112–114], service ecosystem [115,116], epidemic prevention and control [117,118], active surveillance [119], large scale network analysis [120], pedestrian dead reckoning [121], and evaluation of human lower limb motions [122].





4. Conclusions

The use of swarm intelligence optimization algorithms to optimize machine learning parameters is becoming more widely used in the study of classification problems. These types of machine learning algorithms perform better than the original machine learning models. This paper proposes a robust and accurate machine learning method, SMFO-KELM, effectively solving the soil erosion prediction problem. The model's main idea is to apply a new and improved MFO algorithm, SMFO, by optimizing the penalty parameter c of the KELM and the generalization capability of the kernel parameter γ classifier. The improved SMFO is proposed after integrating the positive cosine mechanism in the original MFO. This approach provides higher performance, in terms of consistency in global optimization, improves the balance between exploration and exploitation, and increases the convergence speed.

From the results of the experiments in this paper, it can be concluded that, for the discrete soil data classification problem, the SMFO-KELM model is significantly superior compared to the MFO-KELM model. It can be observed that the positive cosine strategy that was used by SMFO in the improvement strategy, has a positive effect on optimizing the kernel limit learning machine parameter optimization; comparing this with other algorithms, such as BA-KELM, CLOFOA-KELM, IGWO-KELM, and OBLGWO-KELM models, it can be observed that SMFO-KELM outperforms several other classifier models in solving soil erosion classification problems in four commonly used performance metrics. Therefore, it can be derived that the usability of SMFO-KELM has been extended, and

the proposed method can be considered as a valuable early warning tool for soil erosion prediction systems, helping land management agencies to make scientifically accurate decisions.

In addition, soil erosion prediction models can be combined with other optimization algorithms, and the SMFO used can also be used for parameter tuning of other machine learning models, such as KNN, support vector machine, and convolutional neural networks, and can also be applied to deal with pest and disease image segmentation, feature selection problems. Other potential applications, such as fertilizer effect function optimization, reservoir regulation optimization, and combined irrigation and groundwater optimal allocation, are also exciting topics for green sustainability in agricultural engineering. More agricultural engineering optimization problems will continue to be investigated in the future.

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Informed Consent Statement: Informed consent was obtained from all subjects involved in the study.

Data Availability Statement: The data of the study can be gotten from the published paper.

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Conflicts of Interest: The authors declare no conflict of interest.

No.	a1	a2	
 1	2044.01	27.93	

Appendix A

Table A1. Soil erosion data.

No.	a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	Туре
1	2044.01	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	42.09	1
2	975.56	29.57	1	5.8	1.46	55.26	31.35	30.43	38.21	25.91	1
3	2044.01	28.17	1.2	6.59	1.37	51.75	34.93	27.57	37.5	60.19	1
4	975.56	28.17	1.2	6.59	1.37	51.75	34.93	27.57	37.5	8.98	1
5	2044.01	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	54.96	1
6	1138.37	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	29.74	1
7	975.56	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	18.01	1
8	2044.01	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	51.12	1
9	2044.01	29.57	1	5.8	1.46	55.26	31.35	30.43	38.21	44.35	1
10	1138.37	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	23.59	1
11	975.56	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	9.65	1
12	976.92	28.17	1.2	6.59	1.37	51.75	34.93	27.57	37.5	5.99	1
13	975.56	34.77	1.42	6.72	1.37	51.87	32.73	24.33	42.93	29.9	1
14	975.56	29.8	1.53	7.06	1.58	59.48	36.31	18.61	45.08	30.56	1
15	3008.93	28.63	2.39	5.2	1.44	54.49	34.73	28.89	36.37	53.9	1
16	1270.46	28.63	2.32	5.2	1.44	54.49	34.73	28.89	36.37	10.54	1
17	1472.5	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	4.85	1
18	2044.01	34.77	1.42	6.72	1.37	51.87	32.73	24.33	42.93	47.03	1
19	1138.37	29.57	1	5.8	1.46	55.26	31.35	30.43	38.21	31.98	1

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	No.	a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	Type
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	1270 46	28 47	2.08	5 36	1 25	47 09	31 47	34 59	33.93	12 33	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	2044.01	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	59.98	1
21 975.56 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 7.65 1 25 1138.37 28.17 1.2 6.59 1.37 51.75 34.03 27.57 37.5 37.5 37.6 51.85 1.66 1.86 1.44 65.08 51.87 30.15 35.29 44.96 1.1 21 20.46 2.22.7 5.54 1.3 49.07 33.33 30.15 35.23 42.07 1.1 29 120.64 2.62.7 2.41 5.23 1.32 51.87 32.33 40.33 42.93 44.29 1.1 21 138.37 28.17 1.2 6.59 1.37 51.87 34.93 2.757 37.5 1.497 1 21 138.37 28.17 1.2 6.59 1.37 51.75 34.93 2.757 37.5 6.67 1 1 53.12 33.93 2.46.7 1.497 1	22	975.56	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	26.91	1
24 3008.93 26.27 21.85 52.33 1.32 49.92 32.44 31.09 36.49 60.88 1 25 113.53 28.17 12.6 59 1.37 51.75 31.93 30.15 35.92 44.96 1 26 2044.01 29.8 1.33 7.06 1.58 59.48 36.31 18.61 45.08 65.48 1 29 975.56 41.17 0.99 5.89 1.34 50.62 32.41 31.09 36.49 13.33 30.35 22.07 1 30 1138.57 28.17 1.2 6.59 1.37 51.75 34.93 22.75 37.5 1.47 1 31 635.09 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 6.74 1 35 263.04 28.17 1.2 6.59 1.37 51.75 34.93 20.57 9.73 1.73 1.12 <t< td=""><td>23</td><td>975.56</td><td>29.6</td><td>1.46</td><td>6.68</td><td>1.41</td><td>53.12</td><td>33.19</td><td>20.29</td><td>46.51</td><td>7.65</td><td>1</td></t<>	23	975.56	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	7.65	1
25 1138.37 28.17 1.27 51.75 34.93 27.57 37.5 27.69 1 26 20440 29.8 133 7.06 1.58 59.48 30.15 35.92 44.96 1 27 3008.93 28.03 2.27 5.54 1.3 49.07 33.93 30.15 35.92 44.96 1 28 127.04 6.22 1.37 51.87 32.73 24.33 42.93 44.29 1 30 1188.37 28.17 1.32 6.59 1.37 51.75 34.93 27.57 37.5 1.497 1 31 308.93 28.47 2.25 5.36 1.25 47.09 31.47 34.59 33.93 28.667 1 34 685.09 29.4 2.48 5.36 1.25 47.09 31.47 34.59 33.93 3.66.7 1 35 65.02 2.84 2.049 3.41 33.33 3.	24	3008.93	26.27	2.18	5.23	1.32	49.92	32.41	31.09	36.49	60.88	1
26 2044.01 29.8 1.53 7.06 1.58 59.48 56.31 18.61 45.08 65.48 1 27 30.083 28.01 2.27 5.54 1.7 0.99 5.56 3.17 0.99 5.89 1.34 50.62 3.41 53.33 30.35 2.207 1 30 1138.37 34.77 1.42 6.72 1.37 51.87 34.93 2.757 37.14 9.1 31 685.09 2.84.7 2.35 5.36 1.25 47.09 31.47 34.59 33.93 58.07 1 33 3008.93 2.84.7 2.26 5.36 1.25 47.09 31.47 34.59 33.93 32.66 7.1 34 685.02 2.84.17 1.2 6.59 1.37 51.75 34.93 27.57 3.73 3.66 7.97 1 35 2.04.01 34.17 0.29 2.637 2.96 1.46 6.68	25	1138.37	28.17	1.2	6.59	1.37	51.75	34.93	27.57	37.5	27.69	1
27 3008.93 28.03 2.27 5.54 1.3 49.07 33.93 30.15 35.92 44.96 1 28 12704 26.27 24.1 5.10 34.49 13.33 12.7 10 1133.3 14.7 0.99 5.89 1.34 50.62 34.31 35.33 30.35 22.07 1.33 42.93 14.29 1 31 685.09 28.17 1.2 6.59 1.37 51.75 34.99 24.95 40.05 21.1 1 34 685.09 28.47 2.35 5.36 1.25 47.09 31.47 34.59 33.93 58.07 1 35 263.04 28.47 2.08 5.36 1.25 47.09 31.47 34.59 33.93 24.66 1 1 34.7 34.59 3.57 35.9 7.35 9.73 1 36 90.35.8 28.17 1.2 6.59 1.37 51.49 31.1	26	2044.01	29.8	1.53	7.06	1.58	59.48	36.31	18.61	45.08	65.48	1
28 1270.46 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 13.13 1 30 1138.37 24.77 1.42 6.72 1.37 51.87 32.73 24.33 42.93 44.29 1 31 685.09 28.17 1.33 6.38 1.48 55.8 34.99 24.95 40.05 21.1 1 32 3008.93 28.47 2.35 5.36 1.25 47.09 31.47 34.59 33.93 58.07 1 34 685.00 28.47 2.08 5.36 1.25 47.09 31.47 34.59 33.93 26.66 1 35 263.04 28.17 1.2 6.59 1.37 51.75 34.93 2.75 3.75 9.73 1 36 147.25 28.63 2.32 1.32 4.92 3.24 3.109 36.49 1.875 1 37 294.6 1.46<	27	3008.93	28.03	2.27	5.54	1.3	49.07	33.93	30.15	35.92	44.96	1
29 975.56 34.17 0.99 5.89 1.34 50.62 34.31 35.33 0.35 22.07 1 31 685.09 28.17 1.42 6.52 1.37 51.87 34.93 27.57 37.5 14.97 1 32 138.7 28.17 1.23 6.58 1.48 55.8 34.99 24.95 40.05 21.1 1 33 3008.93 28.47 2.35 6.56 1.25 47.09 31.47 34.59 33.93 58.07 1 36 550.22 28.47 2.08 5.36 1.25 47.09 31.47 34.59 33.93 24.66 1 37 2044.01 34.17 0.99 53.88 1.44 54.49 34.31 35.33 30.35 65.79 1 40 192.8 26.27 2.41 5.23 5.2 1.44 54.33 31.99 24.95 40.05 19 1 41 <td>28</td> <td>1270.46</td> <td>26.27</td> <td>2.41</td> <td>5.23</td> <td>1.32</td> <td>49.92</td> <td>32.41</td> <td>31.09</td> <td>36.49</td> <td>13.13</td> <td>1</td>	28	1270.46	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	13.13	1
30 1138.37 34.77 1.42 6.72 1.37 51.87 32.73 24.33 44.29 1 31 685.09 28.17 1.23 6.38 1.48 55.8 34.99 24.95 30.05 21.1 1 33 3008.93 28.47 2.35 5.36 1.25 47.09 31.47 34.59 33.93 58.07 1 34 685.09 28.6 1.46 6.68 1.41 53.12 54.99 2.757 37.5 6.74 1 35 203.04 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 6.74 1 36 450.2 28.417 1.2 6.59 1.37 51.75 34.93 27.57 37.5 9.73 1 40 192.8 2.22 2.41 5.32 1.32 49.29 2.49 40.05 19 1 41 260.7 2.96 1.46	29	975.56	34.17	0.99	5.89	1.34	50.62	34.31	35.33	30.35	22.07	1
31 685.09 28.17 1.12 6.59 1.37 51.75 34.93 27.57 37.5 14.97 1 33 3008.93 28.47 2.35 5.36 1.25 47.09 31.47 34.95 40.05 12.75 1 34 685.09 26.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 1.275 1 35 263.04 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 6.74 1 36 550.22 28.47 2.08 5.36 1.25 41.41 50.42 34.31 35.33 30.33 65.79 1.3 37 2044.01 34.17 0.59 1.37 51.75 34.93 2.757 37.5 9.73 1.8 40 192.8 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 1.8.7 1.1 43 1338 70.12 1.83 1.42 52.69 3.147 55.47 33.47	30	1138.37	34.77	1.42	6.72	1.37	51.87	32.73	24.33	42.93	44.29	1
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33 3008.93 28.47 2.35 5.36 1.25 47.09 31.47 34.47 34.93 33.93 88.07 1 34 685.09 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 12.75 1 35 263.04 28.47 2.08 5.36 1.25 47.09 31.47 34.93 3.03 24.66 1 37 2044.01 34.17 0.29 36.37 3.69 1 39 973.58 28.17 1.2 6.59 1.37 51.75 34.93 2.25 9.73 1 40 192.8 26.27 2.41 5.23 1.32 3.19.2 3.24 1.86 5.8 3.499 2.495 40.05 19 1 41 280.7 9.28 1.33 1.06 6.68 1.44 5.49 3.473 3.069 3.5.4 12.06 1 44 88 2.93	32	1138.37	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	21.1	1
34 685.09 29.6 1.46 6.68 1.41 53.12 33.19 20.29 4.651 1.275 1 35 263.04 28.17 1.2 6.59 1.37 51.75 34.93 32.57 33.93 24.66 1 36 550.22 28.47 2.08 5.2 1.44 54.49 34.31 35.33 30.35 65.79 1 38 1472.5 28.63 2.22 2.44 54.49 34.73 21.89 36.37 3.69 1 40 192.8 26.27 2.44 54.39 32.24 32.41 31.09 36.49 18.75 1 41 2503.7 2.96 1.46 6.68 1.41 53.12 33.19 20.29 46.51 86.7 1 42 68.09 28.17 1.33 6.38 1.44 54.49 34.73 30.69 58.4 64.3 1 43 1138.37 3.73 1.06 <td>33</td> <td>3008.93</td> <td>28.47</td> <td>2.35</td> <td>5.36</td> <td>1.25</td> <td>47.09</td> <td>31.47</td> <td>34.59</td> <td>33.93</td> <td>58.07</td> <td>1</td>	33	3008.93	28.47	2.35	5.36	1.25	47.09	31.47	34.59	33.93	58.07	1
$ \begin{array}{ccccccccccccccccccccccccccccccccccc$	34	685.09	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	12.75	1
36 550.22 28.47 2.08 5.36 1.25 47.09 31.47 34.33 30.33 56.79 1 38 1472.5 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 3.69 1 39 973.58 28.17 1.2 6.59 1.37 51.75 34.93 27.77 37.5 9.73 1 40 192.8 26.27 2.41 5.22 1.44 54.49 34.73 28.69 36.37 1.86 41 2503.7 22.6 1.46 6.68 1.41 53.12 33.47 30.69 35.84 12.06 1 43 1138.37 30.2 1.28 5.85 1.49 34.73 28.49 36.37 21.08 1 44 88 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 6.43 1 45 50.42 2.83.7 1.05	35	263.04	28.17	1.2	6.59	1.37	51.75	34.93	27.57	37.5	6.74	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	36	550.22	28.47	2.08	5.36	1.25	47.09	31.47	34.59	33.93	24.66	1
38 1472.5 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 3.69 1 40 192.8 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 18.75 1 41 2503.7 29.6 1.46 6.68 1.41 53.12 31.9 20.9 46.51 86.7 1 42 6850 28.17 1.33 6.38 1.48 55.8 34.99 24.95 40.05 19 1 43 1138.37 30.2 1.28 5.85 1.44 52.67 34.73 28.89 36.37 21.08 1 45 550.22 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 21.08 1 46 2044.01 33.73 1.06 6.95 1.57 59.38 37.71 19.51 42.77 61.2 1 47 97.692	37	2044.01	34.17	0.99	5.89	1.34	50.62	34.31	35.33	30.35	65.79	1
39 973.58 28.17 1.2 6.59 1.37 51.75 34.93 2.757 37.5 9.73 1 40 192.8 26.27 2.41 5.23 1.32 4992 32.41 31.09 36.49 18.75 1 41 2503.7 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 86.7 1 42 685.09 28.17 1.33 6.38 1.44 55.46 34.99 24.95 40.05 19 1 44 88 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 6.43 1 45 1138.37 31.17 0.99 5.89 1.44 50.62 36.19 2.795 35.86 82.31 1 48 1138.37 31.17 0.99 5.89 1.44 50.62 36.19 2.795 35.86 82.31 1 50 2503.7	38	1472.5	28.63	2.32	5.2	1.44	54.49	34.73	28.89	36.37	3.69	1
	39	973.58	28.17	1.2	6.59	1.37	51.75	34.93	27.57	37.5	9.73	1
$ \begin{array}{ccccccccccccccccccccccccccccccccccc$	40	192.8	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	18.75	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	41	2503.7	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	86.7	1
431138.3730.21.285.851.452.6936.1927.9535.8635.061448827.930.895.831.4755.4733.4730.6935.8412.06145550.2228.632.325.21.4454.4934.7328.8936.3721.081462044.0133.731.066.951.5759.3837.7119.5142.7761.2147976.9227.930.895.831.4755.6733.4730.6935.846.431481138.3729.81.537.061.5859.4836.3118.6145.0827.731502503.730.21.285.851.452.6936.1927.9535.8682.31151973.5828.171.336.381.4855.834.9924.9540.0518.13152973.5829.61.466.681.4153.1233.4730.6935.8486.5153976.9228.171.336.381.4855.834.9924.9540.0517.521542503.727.930.895.831.4755.4733.4730.6935.8486.51553008.9328.371.955.151.2346.3433.0730.6935.8486.51553004.29.6 <t< td=""><td>42</td><td>685.09</td><td>28.17</td><td>1.33</td><td>6.38</td><td>1.48</td><td>55.8</td><td>34.99</td><td>24.95</td><td>40.05</td><td>19</td><td>1</td></t<>	42	685.09	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	19	1
448827.930.895.831.4755.4733.4730.6935.8412.06145550.2228.632.325.21.4454.4934.7328.8936.3721.081462044.0133.731.066.951.5759.3837.7119.5142.7761.2147976.9227.930.895.831.4755.4733.4730.6935.846.431481138.3734.170.995.891.3450.6234.3135.3330.3526.561502503.730.21.285.851.452.6936.1927.9535.8682.31151973.5829.61.466.681.4153.1233.1920.2946.518.29153976.9228.171.336.381.4855.834.9924.9540.0517.521542503.727.930.895.831.4755.4733.4730.6935.8486.51553008.9328.371.955.151.2346.3433.0732.0934.8466.18156550.2226.272.415.231.3249.9232.4131.0936.4926.25157976.922.961.466.681.4153.1231.1920.2946.515.11582503.7	43	1138.37	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	35.06	1
45550.2228.632.325.21.1454.4934.7328.8936.3721.081462044.0133.731.066.951.5759.3837.7119.5142.7761.2147976.9227.930.895.831.4755.4733.4730.6935.846.431481138.3729.81.537.061.5859.4836.3118.6145.0827.731502503.730.21.285.851.452.6936.1927.9535.8682.31151973.5828.171.336.381.4855.834.9924.9540.0518.13152973.5829.61.466.681.4153.1233.1920.2946.518.29153976.9228.171.336.381.4755.4733.4730.6935.8486.51553008.9328.371.955.151.2346.3433.0732.0934.8466.18156550.2226.272.415.231.3249.9231.1920.2946.515.11582503.729.651.466.681.4153.1233.1920.2946.515.1157976.9229.61.466.681.4153.1231.9920.2946.515.1159263.042	44	88	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	12.06	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	45	550.22	28.63	2.32	5.2	1.44	54.49	34.73	28.89	36.37	21.08	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	46	2044.01	33.73	1.06	6.95	1.57	59.38	37.71	19.51	42.77	61.2	1
481138.3734.170.995.891.3450.6234.3135.3330.3526.561491138.3729.81.537.061.5859.4836.3118.6145.0827.731502503.730.21.285.851.452.6936.1927.9535.8682.31151973.5828.171.336.381.4855.834.9924.9540.0518.13152973.5829.61.466.681.4153.1233.1920.2946.518.291542503.727.930.895.831.4755.4733.4730.6935.8486.5156550.2226.272.415.231.3249.9232.4131.0936.4926.25157976.9229.61.466.681.4153.1233.1920.2946.515.11582503.729.5715.81.4655.2631.3530.4338.2182.9160306.152.8632.325.21.4454.4934.7328.8936.3716.56161180.822.8632.325.21.4454.4934.7328.8936.3716.561621969.3928.632.395.21.4454.4934.7328.8936.3716.56163685.092.	47	976.92	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	6.43	1
49 1138.37 29.8 1.53 7.06 1.58 59.48 36.31 18.61 45.08 27.73 1 50 2503.7 30.2 1.28 5.85 1.4 52.69 36.19 27.95 35.86 82.31 1 51 973.58 28.17 1.33 6.38 1.48 55.8 34.99 24.95 40.05 17.52 1 53 976.92 28.17 1.33 6.38 1.48 55.4 34.99 24.95 40.05 17.52 1 54 2503.7 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 86.5 1 55 3008.93 28.37 1.95 5.15 1.23 46.34 33.07 32.09 34.84 66.18 1 56 550.22 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 26.25 1 58 2503.7 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21	48	1138.37	34.17	0.99	5.89	1.34	50.62	34.31	35.33	30.35	26.56	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	49	1138.37	29.8	1.53	7.06	1.58	59.48	36.31	18.61	45.08	27.73	1
51 973.58 28.17 1.33 6.38 1.48 55.8 34.99 24.95 40.05 18.13 1 52 973.58 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 8.29 1 53 976.92 28.17 1.33 6.38 1.48 55.8 34.99 24.95 40.05 17.52 1 54 2503.7 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 86.5 1 55 3008.93 28.37 1.95 5.15 1.23 46.34 33.07 32.09 34.84 66.18 1 56 550.22 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 26.25 1 57 976.92 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 5.1 1 58 2503.7 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 82.9 1 60 306.15 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 11.66 1 61 180.82 28.63 2.39 5.2 1.44 54.49 34.73 28.89 36.37 87.25 1 63 685.09 29.87 1 5.8 59.48 36.31 18.61 45.08 29.65 </td <td>50</td> <td>2503.7</td> <td>30.2</td> <td>1.28</td> <td>5.85</td> <td>1.4</td> <td>52.69</td> <td>36.19</td> <td>27.95</td> <td>35.86</td> <td>82.31</td> <td>1</td>	50	2503.7	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	82.31	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	51	973.58	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	18.13	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	52	973.58	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	8.29	1
54 2503.7 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 86.5 1 55 3008.93 28.37 1.95 5.15 1.23 46.34 33.07 32.09 34.84 66.18 1 56 550.22 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 26.25 1 57 976.92 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 5.1 1 58 2503.7 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 82.9 1 60 306.15 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 11.06 1 61 180.82 28.63 2.39 5.2 1.44 54.49 34.73 28.89 36.37 16.56 1 62 1969.39 28.63 2.39 5.2 1.44 54.49 34.73 28.89 36.37 </td <td>53</td> <td>976.92</td> <td>28.17</td> <td>1.33</td> <td>6.38</td> <td>1.48</td> <td>55.8</td> <td>34.99</td> <td>24.95</td> <td>40.05</td> <td>17.52</td> <td>1</td>	53	976.92	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	17.52	1
55 3008.93 28.37 1.95 5.15 1.23 46.34 33.07 32.09 34.84 66.18 1 56 550.22 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 26.25 1 57 976.92 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 5.1 1 58 2503.7 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 82.9 1 60 306.15 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 11.06 1 61 180.82 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 87.25 1 63 685.09 29.8 1.53 7.06 1.58 59.48 36.31 18.61 45.08 29.65 1 64 3008.93 24.83 2.2 5.97 1.37 51.79 34.35 34.25 31.4 59.03 1 65 976.92 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 7.23 1 67 976.52 29.57 1 5.8 1.46 55.87 33.29 32.17 34.54	54	2503.7	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	86.5	1
56 550.22 26.27 2.41 5.23 1.32 49.92 32.41 31.09 36.49 26.25 1 57 976.92 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 5.1 1 58 2503.7 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 82.9 1 60 306.15 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 11.06 1 61 180.82 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 87.25 1 63 685.09 29.8 1.53 7.06 1.58 59.48 36.31 18.61 45.08 29.65 1 64 3008.93 24.83 2.2 5.97 1.37 51.79 34.35 34.25 31.4 59.03 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 <td>55</td> <td>3008.93</td> <td>28.37</td> <td>1.95</td> <td>5.15</td> <td>1.23</td> <td>46.34</td> <td>33.07</td> <td>32.09</td> <td>34.84</td> <td>66.18</td> <td>1</td>	55	3008.93	28.37	1.95	5.15	1.23	46.34	33.07	32.09	34.84	66.18	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	56	550.22	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	26.25	1
58 2503.7 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 82.9 1 59 263.04 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 5.74 1 60 306.15 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 11.06 1 61 180.82 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 16.56 1 63 685.09 29.8 1.53 7.06 1.58 59.48 36.31 18.61 45.08 29.65 1 64 3008.93 24.83 2.2 5.97 1.37 51.79 34.35 34.25 31.4 59.03 1 65 976.92 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84	57	976.92	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	5.1	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	58	2503.7	29.57		5.8	1.46	55.26	31.35	30.43	38.21	82.9	1
60 506.15 26.65 2.52 5.2 1.44 54.49 54.73 26.89 56.37 11.06 1 61 180.82 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 16.56 1 62 1969.39 28.63 2.39 5.2 1.44 54.49 34.73 28.89 36.37 87.25 1 63 685.09 29.8 1.53 7.06 1.58 59.48 36.31 18.61 45.08 29.65 1 64 3008.93 24.83 2.2 5.97 1.37 51.79 34.35 34.25 31.4 59.03 1 65 976.92 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 7.23 1 67 973.58 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 10.45 1 68 152.99 27.57 2.07 5.13 1.48 55.87 33.29 32.17 34.54 70.78 1 69 2503.7 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 89.3 1 70 89.52 29.6 1.46 6.68 1.41 53.12 33.19	59	263.04	29.6	1.46	6.68 E 0	1.41	53.12	33.19	20.29	46.51	5.74	1
61 180.82 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 16.56 1 62 1969.39 28.63 2.39 5.2 1.44 54.49 34.73 28.89 36.37 87.25 1 63 685.09 29.8 1.53 7.06 1.58 59.48 36.31 18.61 45.08 29.65 1 64 3008.93 24.83 2.2 5.97 1.37 51.79 34.35 34.25 31.4 59.03 1 65 976.92 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 10.45 1 68 152.99 27.57 2.07 5.13 1.48 55.87 33.29 32.17 34.54 70.78 1 69 2503.7 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 89.3 1 70 89.52 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 6.37 1 71 3008.93 28 1.95 5.13 1.37 51.53 33.07 31.51 35.42 64.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28	60	306.13	28.63	2.32	5.Z	1.44	54.49	34.73 24.72	20.09	30.37	11.00	1
62 1969.39 20.65 2.39 3.2 1.44 54.49 54.73 20.89 30.57 67.25 1 63 685.09 29.8 1.53 7.06 1.58 59.48 36.31 18.61 45.08 29.65 1 64 3008.93 24.83 2.2 5.97 1.37 51.79 34.35 34.25 31.4 59.03 1 65 976.92 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 7.23 1 67 973.58 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 10.45 1 68 152.99 27.57 2.07 5.13 1.48 55.87 33.29 32.17 34.54 70.78 1 69 2503.7 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 89.3 1 70 89.52 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 6.37 1 71 3008.93 28 1.95 5.13 1.37 51.53 33.07 31.51 35.42 64.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28	61	100.82	20.03	2.32	5.2	1.44	54.49	34.73 24.72	20.09	30.37 26.27	10.30	1
63 663.09 27.8 1.33 7.06 1.36 59.48 30.31 18.01 43.08 29.63 1 64 3008.93 24.83 2.2 5.97 1.37 51.79 34.35 34.25 31.4 59.03 1 65 976.92 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 7.23 1 67 973.58 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 10.45 1 68 152.99 27.57 2.07 5.13 1.48 55.87 33.29 32.17 34.54 70.78 1 69 2503.7 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 89.3 1 70 89.52 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 6.37 1 71 3008.93 28 1.95 5.13 1.37 51.53 33.07 31.51 35.42 64.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 15.06 1 73 973.58 29.57 1 5.8 1.46 55.26 31.35 30.43	62	1969.39	20.03	2.39	5.Z 7.06	1.44	50.49	34.73 26.21	20.09	30.37 45.08	07.23 20.65	1
64 5003.93 24.83 2.2 5.97 1.37 51.79 54.33 54.23 51.4 59.05 1 65 976.92 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 7.23 1 67 973.58 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 10.45 1 68 152.99 27.57 2.07 5.13 1.48 55.87 33.29 32.17 34.54 70.78 1 69 2503.7 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 89.3 1 70 89.52 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 6.37 1 71 3008.93 28 1.95 5.13 1.37 51.53 33.07 31.51 35.42 64.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 15.06 1 73 973.58 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 26.16 1 74 3008.93 27.9 2.34 5.5 1.34 50.69 35.81 29.23	63	2008 02	29.0 24.82	1.55	7.00	1.30	59.40 51.70	24.25	24.25	45.00	29.03	1
63 976.92 29.57 1 5.8 1.46 55.26 51.33 50.43 58.21 24.94 1 66 263.04 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 7.23 1 67 973.58 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 10.45 1 68 152.99 27.57 2.07 5.13 1.48 55.87 33.29 32.17 34.54 70.78 1 69 2503.7 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 89.3 1 70 89.52 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 6.37 1 71 3008.93 28 1.95 5.13 1.37 51.53 33.07 31.51 35.42 64.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 15.06 1 73 973.58 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 26.16 1 74 3008.93 27.9 2.34 5.5 1.34 50.69 35.81 29.23 34.95 61.5 1 75 685.09 27.93 0.89 5.83 1.47 55.47 33.47 30.69	65	076.02	24.03	2.2 1	5.97	1.37	55.26	21 25	20.42	28.21	24.04	1
66 203.04 27.93 0.89 5.83 1.47 50.47 50.47 50.69 50.64 7.25 1 67 973.58 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 10.45 1 68 152.99 27.57 2.07 5.13 1.48 55.87 33.29 32.17 34.54 70.78 1 69 2503.7 28.17 1.2 6.59 1.37 51.75 34.93 27.57 37.5 89.3 1 70 89.52 29.6 1.46 6.68 1.41 53.12 33.19 20.29 46.51 6.37 1 71 3008.93 28 1.95 5.13 1.37 51.53 33.07 31.51 35.42 64.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 15.06 1 73 973.58 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 26.16 1 74 3008.93 27.9 2.34 5.5 1.34 50.69 35.81 29.23 34.95 61.5 1 75 685.09 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 16.08 1 76 184.93 28.63 2.32 5.2 1.44 54.49 34.73 $28.$	66	970.92 263.04	29.37	1 0.80	5.83	1.40 1.47	55.20	31.55	30.45	35.84	24.94 7 22	1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	67	203.04	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	10.45	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	68	152.99	27.93	2.07	5.03	1.47	55.87	33.47	32 17	34 54	70.78	1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	60 69	2503.7	27.57	1.07	6 59	1.40	51.75	3/ 93	27 57	37.5	89.3	1
70 50.52 12.50 1.40 50.60 1.41 50.12 50.17 20.27 40.51 60.57 1 71 3008.93 28 1.95 5.13 1.37 51.53 33.07 31.51 35.42 64.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 15.06 1 73 973.58 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 26.16 1 74 3008.93 27.9 2.34 5.5 1.34 50.69 35.81 29.23 34.95 61.5 1 75 685.09 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 16.08 1 76 184.93 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 18.07 1 77 89.52 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 <td>70</td> <td>89.52</td> <td>20.17</td> <td>1.2</td> <td>6.68</td> <td>1.57</td> <td>53.12</td> <td>33.19</td> <td>20.29</td> <td>46 51</td> <td>6 37</td> <td>1</td>	70	89.52	20.17	1.2	6.68	1.57	53.12	33.19	20.29	46 51	6 37	1
71 5000.75 20 1.95 5.15 1.67 51.55 50.67 51.51 50.42 61.44 1 72 192.8 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 15.06 1 73 973.58 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 26.16 1 74 3008.93 27.9 2.34 5.5 1.34 50.69 35.81 29.23 34.95 61.5 1 75 685.09 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 16.08 1 76 184.93 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 18.07 1 77 89.52 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 8.04 1	70	3008.93	29.0	1.40	5.13	1.11	51 53	33.07	31 51	35.42	64 44	1
72 73 973.58 29.57 1 5.8 1.46 55.26 31.35 30.43 38.21 26.16 1 74 3008.93 27.9 2.34 5.5 1.34 50.69 35.81 29.23 34.95 61.5 1 75 685.09 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 16.08 1 76 184.93 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 18.07 1 77 89.52 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 8.04 1	72	192.8	28.63	2.32	52	1 44	54 49	34 73	28.89	36 37	15.06	1
74 3008.93 27.9 2.34 5.5 1.34 50.69 35.81 29.23 34.95 61.5 1 75 685.09 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 16.08 1 76 184.93 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 18.07 1 77 89.52 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 8.04 1	73	973 58	29.55	1	5.8	1 46	55 26	31 35	30.43	38 21	26.16	1
75 685.09 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 16.08 1 76 184.93 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 18.07 1 77 89.52 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 16.08 1	74	3008.93	27.9	2.34	5.5	1.10	50.20	35.81	29.23	34 95	61 5	1
76 184.93 28.63 2.32 5.2 1.44 54.49 34.73 28.89 36.37 18.07 1 77 89.52 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 8.04 1	75	685.09	27.93	0.89	5.83	1.54	55 47	33 47	30.69	35.84	16.08	1
77 89.52 27.93 0.89 5.83 1.47 55.47 33.47 30.69 35.84 8.04 1	76	184 93	28.63	2.32	5.2	1.44	54 49	34.73	28.89	36.37	18.07	1
	77	89.52	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	8.04	1

Table A1. Cont.

Table A1. Cont.

No.	a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	Туре
78	973.58	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	27.24	1
79	263.04	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	17.64	1
80	2503.7	34.77	1.42	6.72	1.37	51.87	32.73	24.33	42.93	87	1
81	685.09	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	29.52	1
82	976.92	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	25.61	1
83	973.58	29.8	1.53	7.06	1.58	59.48	36.31	18.61	45.08	30.44	1
84	3008.93	27.57	2.07	5.13	1.48	55.87	33.29	32.17	34.54	58.33	1
85	550.22	24.83	2.66	5.97	1.37	51.79	34.35	34.25	31.4	38.42	1
86	973.58	34.17	0.99	5.89 E E 4	1.34	50.62	34.31	35.33 20.15	30.35	22.25	1
8/	1270.46	28.03	2.38	5.54	1.3	49.07 54.40	33.93	30.15	35.92 26.27	30.71 52.7	1 1
00 80	685.00	20.03	2.32	5.2	1.44 1.46	55 26	34.75 31.35	20.09	30.37 38.21	32.7 27.86	1
90	85 74	29.57	2 32	5.0	1.40	54 49	34 73	28.89	36.37	13 55	1
91	1472.5	28.47	2.02	5.36	1.11	47.09	31.47	34.59	33.93	873	1
92	685.09	34.77	1.42	6.72	1.37	51.87	32.73	24.33	42.93	34.51	1
93	82.99	27.57	2.08	5.13	1.48	55.87	33.29	32.17	34.54	41.51	1
94	75.09	28.63	2.32	5.2	1.44	54.49	34.73	28.89	36.37	2.63	1
95	976.92	34.17	0.99	5.89	1.34	50.62	34.31	35.33	30.35	21.36	1
96	88	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	9.56	1
97	550.22	28.03	2.38	5.54	1.3	49.07	33.93	30.15	35.92	38.42	1
98	3008.93	26.33	2.79	5.91	1.37	51.75	34.69	34.29	31.01	66.21	1
99	184.93	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	22.5	1
100	89.52	28.17	1.2	6.59	1.37	51.75	34.93	27.57	37.5	7.48	1
101	192.8	28.03	2.38	5.54	1.3	49.07	33.93	30.15	35.92	34.01	1
102	550.22	28	2.14	5.13	1.37	51.53	33.07	31.51	35.42	29.34	1
103	82.99	28.47	2.15	5.36	1.25	47.09	31.47	34.59	33.93	30.78	1
104	973.58	34.77	1.42	6.72 E 9E	1.37	51.87	32.73 26.10	24.33	42.93	30.48	1
105	00 88	30.2 28.17	1.20	5.65 6.59	1.4	52.69	30.19	27.90	37.5	27.09	1
100	270.98	28.17	2 35	5.36	1.57	47.09	31.47	27.57	33.93	54 14	1
107	88	29.57	1	5.8	1.46	55.26	31.35	30.43	38.21	26.64	1
109	862.96	28.63	2.39	5.2	1.44	54.49	34.73	28.89	36.37	41.05	1
110	388.7	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	86.91	1
111	263.04	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	25.93	1
112	89.52	34.77	1.42	6.72	1.37	51.87	32.73	24.33	42.93	28.75	1
113	88	34.77	1.42	6.72	1.37	51.87	32.73	24.33	42.93	31.63	1
114	685.09	34.17	0.99	5.89	1.34	50.62	34.31	35.33	30.35	23.51	1
115	263.04	29.57	1	5.8	1.46	55.26	31.35	30.43	38.21	25.19	1
116	862.96	28.47	2.35	5.36	1.25	47.09	31.47	34.59	33.93	46.59	1
117	85.74	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	16.88	1
118	388.7	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	86.43	1
119	136.44	33.73	1.06	6.95 6.05	1.57	59.38 50.28	37.71	19.51	42.77	59.12 66.70	2
120	0.13	33.73 26.27	1.00	5.90 5.23	1.37	09.00 19.97	37.71	31.00	42.77	00.79	2
121	51 22	20.27	1.46	6.68	1.52	53 12	33 19	20.29	46 51	32.25	2
122	152 99	32.33	2.64	5.6	1.11	53 11	33 21	35.47	31.32	78.9	2
124	0.01	26.5	2.3	5.39	1.38	52.05	32.65	29.37	37.98	76.61	2
125	248.37	28.03	2.38	5.54	1.3	49.07	33.93	30.15	35.92	67.52	2
126	0.07	26.5	2.3	5.39	1.38	52.05	32.65	29.37	37.98	89.2	2
127	0.01	29.8	1.13	5.7	1.34	50.58	31.99	38.35	29.66	78.39	2
128	0.06	27.9	2.34	5.5	1.34	50.69	35.81	29.23	34.95	78.29	2
129	1.59	28.03	2.25	5.54	1.3	49.07	33.93	30.15	35.92	42.49	2
130	0.02	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	12.47	2
131	2.09	29.8	1.13	5.7	1.34	50.58	31.99	38.35	29.66	78.27	2
132	6.82	28.63	2.39	5.2	1.44	54.49	34.73	28.89	36.37	88.05	2
133	0.01	27.57	2.08	5.13	1.48	55.87	33.29	32.17	34.54	54.61	2
134	4.61	29.8	1.13	5.7	1.34	50.58	31.99	38.35	29.66	74.21	2
135	41.92	27.9	2.34	5.5	1.34	50.69	35.81	29.23	34.95	94.48	2

No.	a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	Type
100	0.12	24.17	0.00	5 00	1.04	50 (2	24.21	25.00	20.25	(0.42	
130	0.13	34.17 27.0	0.99	5.69	1.34	50.62 50.60	34.31 25.91	33.33 20.22	30.33 24.05	00.45	2
137	0.53	27.9	2.30	6.59	1.34	51.75	34.03	29.23	37.5	13 56	2
130	0.13	20.17	2.08	5.36	1.57	47.09	31.75	27.57	33.03	13.30	2
139	299 78	20.47	2.00	6.95	1.23	59 38	37.47	19 51	40 77	87.63	2
140	0.01	29.8	1.00	7.06	1.57	59.30	36 31	19.51	45.08	60.71	2
141	6 79	26.33	2 36	7.00 5.91	1.30	51.40	34 69	34.29	40.00 31.01	68 94	2
142	46 34	20.00	1.42	672	1.37	51.75	32 73	24.33	42.93	29.89	2
143	0.01	26.5	2 33	5 39	1.37	52.05	32.65	29.37	37.98	17 34	2
145	0.01	20.0 28.47	2.00	5.36	1.50	47.09	31.47	34 59	33.93	50.56	2
146	10.42	32.33	2.10	5.6	1.20	53 11	33 21	35.47	31.32	12.61	2
147	0.27	28.63	2.39	5.2	1 44	54 49	34 73	28.89	36.37	79.4	2
148	0.36	29.8	1.53	7.06	1.58	59.48	36.31	18.61	45.08	31.35	2
149	6.67	29.57	1.00	5.8	1.46	55.26	31.35	30.43	38.21	45.21	2
150	299.78	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	85.91	2
151	9.59	28.03	2.38	5.54	1.3	49.07	33.93	30.15	35.92	33.71	2
152	2.59	24.83	2.2	5.97	1.37	51.79	34.35	34.25	31.4	90.72	2
153	6.42	29.8	1.53	7.06	1.58	59.48	36.31	18.61	45.08	69.61	2
154	25.4	30.27	1.24	5.72	1.45	54.87	33.43	27.21	39.36	68.61	2
155	3.38	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	49.22	2
156	12.41	28.63	2.39	5.2	1.44	54.49	34.73	28.89	36.37	28.42	2
157	89.52	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	26.26	2
158	152.99	27.9	2.34	5.5	1.34	50.69	35.81	29.23	34.95	73.49	2
159	15.22	26.33	2.79	5.91	1.37	51.75	34.69	34.29	31.01	94.25	2
160	202.32	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	25.35	2
161	115.94	30.27	1.24	5.72	1.45	54.87	33.43	27.21	39.36	64.78	2
162	3.91	28.03	2.25	5.54	1.3	49.07	33.93	30.15	35.92	66.79	2
163	61.6	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	40.05	2
164	0.24	28.47	2.08	5.36	1.25	47.09	31.47	34.59	33.93	28.69	2
165	0	29.57	1	5.8	1.46	55.26	31.35	30.43	38.21	24.7	2
166	0.07	28.63	2.36	5.2	1.44	54.49	34.73	28.89	36.37	80.3	2
167	0.03	24.83	2.2	5.97	1.37	51.79	34.35	34.25	31.4	95.27	2
168	21.94	28.47	2.08	5.36	1.25	47.09	31.47	34.59	33.93	63.41	2
169	51.22	28.17	1.33	6.38	1.48	55.8	34.99	24.95	40.05	28.54	2
170	550.22	28.37	2.05	5.15	1.23	46.34	33.07	32.09	34.84	40.79	2
171	4.21	33.73	1.06	6.95	1.57	59.38	37.71	19.51	42.77	19.05	2
172	64.15	30.27	1.24	5.72	1.45	54.87	33.43	27.21	39.36	70.53	2
173	54.17	34.17	0.99	5.89	1.34	50.62	34.31	35.33	30.35	59.86	2
174	385.11	27.57	2.11	5.13	1.48	55.87	33.29	32.17	34.54	71.11	2
175	0.01	28	1.95	5.13	1.37	51.53	33.07	31.51	35.42	48.2	2
176	0.03	27.57	2.11	5.13	1.48	55.87	33.29	32.17	34.54	28.77	2
177	0.01	29.8	1.13	5.7	1.34	50.58	31.99	38.35	29.66	80.55	2
178	6.42	29.57	1	5.8	1.46	55.26	31.35	30.43	38.21	47.99	2
179	0.01	28.47	2.35	5.36	1.25	47.09	31.47	34.59	33.93	86.16	2
180	0.02	27.93	0.89	5.83	1.47	55.47	33.47	30.69	35.84	22.84	2
181	248.37	24.83	2.66	5.97	1.37	51.79	34.35	34.25	31.4	68.24	2
182	0.13	33.73	1.06	6.95	1.57	59.38	37.71	19.51	42.77	47.47	2
183	1.96	28.63	2.39	5.2	1.44	54.49	34.73	28.89	36.37	10.46	2
184	295.82	26.33	2.79	5.91	1.37	51.75	34.69	34.29	31.01	89.38	2
185	22.45	28.03	2.27	5.54	1.3	49.07	33.93	30.15	35.92	57.02	2
186	0.01	26.5	2.33	5.39	1.38	52.05	32.65	29.37	37.98	45.64	2
187	131.01	32.33	2.64	5.6 E 01	1.41	53.11	33.21	35.47	31.32	62.69	2
100	25.82	20.33	2.38	0.91 6 29	1.37	51./5 EE 9	34.69 24.00	34.29 24.05	31.01 40.05	45.64	2
109	0.13	20.17	1.33	0.3ð	1.48	55.8 F2 11	34.99 22.21	24.93 25.47	40.05	40.41	2
190	0.01	3∠.33 27 ⊑7	2.3 2.07	5.0 5.12	1.41	33.11 55.97	33.∠1 22.20	33.47 23.17	31.3Z	97.92 81.04	2
171 10 0	0.03	20.2	2.07	5.13	1.4ð 14	52.67	35.29 36 10	32.17 27.05	34.34 35.94	01.94 47.0	∠ 2
174	0.14	30.Z	1.40	5.05	1.4	52.09	30.19	21.90	33.00	4/.7	4

Table A1. Cont.

No.	a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	Туре
193	0.72	26.27	2.41	5.23	1.32	49.92	32.41	31.09	36.49	24.38	2
194	0.01	28.03	2.27	5.54	1.3	49.07	33.93	30.15	35.92	70.92	2
195	0.01	32.33	2.29	5.6	1.41	53.11	33.21	35.47	31.32	80.56	2
196	0.38	27.9	2.18	5.5	1.34	50.69	35.81	29.23	34.95	66.79	2
197	0.01	26.33	2.36	5.91	1.37	51.75	34.69	34.29	31.01	63.38	2
198	57.23	29.8	1.13	5.7	1.34	50.58	31.99	38.35	29.66	82.15	2
199	0.53	26.5	2.33	5.39	1.38	52.05	32.65	29.37	37.98	25.72	2
200	6.74	29.6	1.46	6.68	1.41	53.12	33.19	20.29	46.51	17.21	2
201	1.36	26.33	2.79	5.91	1.37	51.75	34.69	34.29	31.01	41.61	2
202	0.01	28.37	2.05	5.15	1.23	46.34	33.07	32.09	34.84	83.99	2
203	0.03	30.27	1.24	5.72	1.45	54.87	33.43	27.21	39.36	81.04	2
204	0.42	32.33	2.64	5.6	1.41	53.11	33.21	35.47	31.32	52.59	2
205	6.82	26.33	2.79	5.91	1.37	51.75	34.69	34.29	31.01	95.3	2
206	180.82	28.03	2.38	5.54	1.3	49.07	33.93	30.15	35.92	35.11	2
207	131.01	26.33	2.79	5.91	1.37	51.75	34.69	34.29	31.01	58.84	2
208	0.01	28.37	2.05	5 15	1 23	46.34	33.07	32.09	34 84	17 44	2
209	0.79	28.17	12	6 59	1.20	51 75	34.93	27 57	37.5	19 32	2
210	766.63	26.5	2.3	5.39	1.38	52.05	32.65	29.37	37.98	74.62	2
210	34 74	24.83	2.66	5.97	1.37	51 79	34.35	34 25	31.4	31.81	2
212	17 58	28.63	2 39	5.2	1.07	54 49	34 73	28.89	36 37	11 52	2
212	3 32	28.37	1.05	5.15	1.11	46 34	33.07	32.09	34.84	67.05	2
210	14 81	28	2 14	5.13	1.20	51 53	33.07	31 51	35.42	33.43	2
214	152 99	28.63	2.14	5.10	1.37	54 49	34 73	28.89	36.37	65 34	2
210	0.03	28.17	1 33	6 38	1.11	55.8	34 99	24.95	40.05	63.29	2
210	0.05	20.17	0.99	5.89	1.40	50.62	34.31	35.33	30.35	94.6	2
217	6.16	29.6	1.46	6.68	1.54	53.12	33.10	20.29	46 51	21.81	2
210	4 35	29.6	1.40	6.68	1.41	53.12	33.19	20.29	46.51	76.4	2
21)	4.00	29.0	1.40	6 59	1.41	51 75	34.93	27.57	37.5	1/ 91	2
220	220.20	26.17	1.2	5.39	1.37	52.05	22.65	27.37	27.08	14.91 81.01	2
221	230.39	20.5	2.3	5.39	1.30	52.05	32.05	29.37	37.90	50.40	2
222	0.01	24.03	2.00	5.97	1.37	51.79	24.35	34.25	31.4 21.4	09.49 84 78	2
223	0.03	24.03	2.2	5.97	1.37	51.79	22.65	34.23	27.09	04.70	2
224	0.03	20.3	2.07	5.39	1.30	52.05	32.03	29.37	37.90	96.62	2
225	0.82	32.33	2.04	5.6	1.41	55.11	33.21	35.47	31.32	97.64	2
220	61.6	34.77	1.42	6.7Z	1.37	51.87	32.73	24.33	42.93	30.87	2
227	6.16	34.17	0.99	5.89	1.34	50.62	34.31	35.33	30.35	68.71	2
228	9.8	30.2	1.28	5.85	1.4	52.69	36.19	27.95	35.86	39.13	2
229	1.79	28.03	2.25	5.54	1.3	49.07	33.93	30.15	35.92	44.54	2
230	10.42	28.63	2.32	5.2	1.44	54.49	34.73	28.89	36.37	1.05	2
231	15.87	28.37	2.07	5.15	1.23	46.34	33.07	32.09	34.84	65.08	2
232	0.42	28	1.95	5.13	1.37	51.53	33.07	31.51	35.42	48.18	2
233	25.4	29.8	1.53	7.06	1.58	59.48	36.31	18.61	45.08	66.82	2
234	21.94	28	2.14	5.13	1.37	51.53	33.07	31.51	35.42	64.13	2
235	682.46	26.33	2.38	5.91	1.37	51.75	34.69	34.29	31.01	61.97	2
236	0.38	28	2.17	5.13	1.37	51.53	33.07	31.51	35.42	39.53	2

Table A1. Cont.

 Table A2. SMFO and other comparison algorithms 10-fold cross-validation results.

Algorithm	Index	Max	Min	Mean	Std	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10
SMFO	accs	0.958333	0.791667	0.894384	0.056461	0.956522	0.956522	0.958333	0.875	0.916667	0.869565	0.916667	0.869565	0.833333	0.791667
SMFO	sens	1	0.75	0.874073	0.099287	1	0.916667	0.941176	0.8	0.909091	0.909091	1	0.75	0.764706	0.75
SMFO	spes	1	0.833333	0.923187	0.06527	0.923077	1	1	0.928571	0.923077	0.8333333	0.857143	0.933333	1	0.8333333
SMFO	mccs	0.916667	0.585369	0.789217	0.111741	0.916057	0.916667	0.907485	0.741941	0.832168	0.742424	0.845154	0.707317	0.697589	0.585369
MFO	accs	0.958333	0.695652	0.850906	0.069384	0.695652	0.875	0.869565	0.826087	0.916667	0.826087	0.875	0.833333	0.958333	0.833333
MFO	sens	1	0.545455	0.805058	0.129786	0.545455	0.916667	0.8	0.833333	0.916667	0.75	0.75	0.846154	1	0.692308
MFO	spes	1	0.818182	0.900335	0.070731	0.833333	0.833333	0.923077	0.818182	0.916667	1	0.9375	0.818182	0.923077	1
MFO	mccs	0.919866	0.397276	0.706981	0.135508	0.397276	0.752618	0.734465	0.651515	0.833333	0.690849	0.713024	0.664336	0.919866	0.712525
BA	accs	1	0.375	0.7875	0.213497	0.791667	0.833333	1	0.913043	0.958333	0.956522	0.608696	0.916667	0.375	0.521739
BA	sens	1	0.375	0.775332	0.230311	0.769231	0.8	1	0.8	1	0.909091	0.7	1	0.4	0.375
BA	spes	1	0.333333	0.794077	0.228935	0.818182	0.888889	1	1	0.928571	1	0.538462	0.833333	0.333333	0.6
BA	mccs	1	-0.2582	0.572323	0.438456	0.585369	0.669342	1	0.832666	0.91878	0.916057	0.238462	0.845154	-0.2582	-0.0244
GSA	accs	0.958333	0.695652	0.855435	0.081639	0.826087	0.791667	0.958333	0.869565	0.958333	0.791667	0.695652	0.913043	0.875	0.875
GSA	sens	1	0.6	0.842946	0.118463	0.818182	0.866667	1	0.818182	0.888889	0.6	0.692308	0.916667	0.9	0.928571
GSA	spes	1	0.666667	0.852056	0.10488	0.833333	0.666667	0.909091	0.916667	1	0.928571	0.7	0.909091	0.857143	0.8
GSA	mccs	0.91878	0.389324	0.705087	0.16755	0.651515	0.547723	0.91878	0.74048	0.912871	0.573316	0.389324	0.825758	0.749159	0.741941

Algorithm	Index	Max	Min	Mean	Std	#1	#2	#3	#4	#5	#6	#7	#8	#9	#10
MVO	accs	0.958333	0.695652	0.842572	0.083615	0.826087	0.75	0.958333	0.869565	0.958333	0.791667	0.695652	0.826087	0.875	0.875
MVO	sens	1	0.6	0.83628	0.118855	0.818182	0.8	1	0.818182	0.888889	0.6	0.692308	0.916667	0.9	0.928571
MVO	spes	1	0.666667	0.833874	0.10955	0.833333	0.666667	0.909091	0.916667	1	0.928571	0.7	0.727273	0.857143	0.8
MVO	mccs	0.91878	0.389324	0.680314	0.171967	0.651515	0.466667	0.91878	0.74048	0.912871	0.573316	0.389324	0.659093	0.749159	0.741941
WOA	accs	1	0.75	0.860145	0.071755	0.75	1	0.913043	0.833333	0.875	0.826087	0.875	0.833333	0.782609	0.913043
WOA	sens	1	0.625	0.823689	0.128234	0.625	1	0.9	0.923077	1	0.769231	0.8	0.727273	0.692308	0.8
WOA	spes	1	0.727273	0.893593	0.100358	0.8125	1	0.923077	0.727273	0.75	0.9	1	0.923077	0.9	1
WOA	mccs	1	0.4375	0.723757	0.153443	0.4375	1	0.823077	0.669342	0.774597	0.664141	0.774597	0.669342	0.592308	0.832666
GOA	accs	0.958333	0.695652	0.855435	0.081639	0.826087	0.791667	0.958333	0.869565	0.958333	0.791667	0.695652	0.913043	0.875	0.875
GOA	sens	1	0.6	0.842946	0.118463	0.818182	0.866667	1	0.818182	0.888889	0.6	0.692308	0.916667	0.9	0.928571
GOA	spes	1	0.666667	0.852056	0.10488	0.833333	0.666667	0.909091	0.916667	1	0.928571	0.7	0.909091	0.857143	0.8
GOA	mccs	0.91878	0.389324	0.705087	0.16755	0.651515	0.547723	0.91878	0.74048	0.912871	0.573316	0.389324	0.825758	0.749159	0.741941
CLOFOA	accs	0.958333	0.666667	0.830797	0.080856	0.782609	0.826087	0.666667	0.875	0.913043	0.791667	0.869565	0.791667	0.958333	0.833333
CLOFOA	sens	1	0.714286	0.844316	0.099605	0.769231	0.75	0.8	0.846154	1	0.785714	0.888889	0.714286	1	0.888889
CLOFOA	spes	1	0.571429	0.8421	0.114379	0.8	1	0.571429	0.909091	0.866667	0.8	0.857143	0.9	0.916667	0.8
CLOFOA	mccs	0.919866	0.371429	0.672348	0.153658	0.564902	0.690849	0.371429	0.752618	0.832666	0.579538	0.734465	0.607808	0.919866	0.669342
HGWO	accs	0.958333	0.695652	0.855254	0.074398	0.869565	0.833333	0.916667	0.869565	0.958333	0.791667	0.695652	0.826087	0.916667	0.875
HGWO	sens	1	0.6	0.83283	0.139342	0.727273	0.933333	1	0.818182	0.888889	0.6	0.615385	0.916667	0.9	0.928571
HGWO	spes	1	0.666667	0.858593	0.113401	1	0.666667	0.818182	0.916667	1	0.928571	0.8	0.727273	0.928571	0.8
HGWO	mccs	0.912871	0.415385	0.711557	0.145478	0.76277	0.639064	0.842075	0.74048	0.912871	0.573316	0.415385	0.659093	0.828571	0.741941
IGWO	accs	0.958333	0.695652	0.842572	0.083615	0.826087	0.75	0.958333	0.869565	0.958333	0.791667	0.695652	0.826087	0.875	0.875
IGWO	sens	1	0.6	0.819497	0.134967	0.727273	0.8	1	0.818182	0.888889	0.6	0.615385	0.916667	0.9	0.928571
IGWO	spes	1	0.666667	0.852208	0.102594	0.916667	0.666667	0.909091	0.916667	1	0.928571	0.8	0.727273	0.857143	0.8
IGWO	mccs	0.91878	0.415385	0.683678	0.167058	0.659093	0.466667	0.91878	0.74048	0.912871	0.573316	0.415385	0.659093	0.749159	0.741941
OBLGWO	accs	0.916667	0.782609	0.847101	0.046862	0.916667	0.869565	0.782609	0.782609	0.791667	0.875	0.875	0.833333	0.869565	0.875
OBLGWO	sens	0.916667	0.666667	0.807326	0.078075	0.833333	0.875	0.666667	0.916667	0.764706	0.785714	0.818182	0.785714	0.727273	0.9
OBLGWO	spes	1	0.636364	0.889754	0.108325	1	0.866667	0.857143	0.636364	0.857143	1	0.923077	0.9	1	0.857143
OBLGWO	mccs	0.845154	0.536745	0.697367	0.102198	0.845154	0.723793	0.536745	0.580023	0.573316	0.777429	0.749159	0.676123	0.76277	0.749159

Table A2. Cont.

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