



Article Heat Transfer Impacts on Maxwell Nanofluid Flow over a Vertical Moving Surface with MHD Using Stochastic Numerical Technique via Artificial Neural Networks

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Abstract: The technique of Levenberg–Marquardt back propagation with neural networks (TLMB-NN) was used in this research article to investigate the heat transfer of Maxwell base fluid flow of nanomaterials (HTM-BFN) with MHD over vertical moving surfaces. In this study, the effects of thermal energy, concentration, and Brownian motion are also employed. Moreover, the impacts of a heat-absorbing fluid with viscous dissipation and radiation have been explored. To simplify the governing equations from a stiff to a simple system of non-linear ODEs, we exploited the efficacy of suitable similarity transformation mechanism. Through applicability of state-of-the-art Adams numerical technique, a set of data for suggested (TLMB-NN) is generated for several situations (scenarios) by changing parameters, such as the Thermophoresis factor N_t , Hartmann number M_t , Eckert number E_c , concentration Grashoff parameter G_c , Prandtl number P_r , Lewis number Le, thermal Grashof number G_T , and Brownian motion factor N_h . The estimate solution of different instances has validated using the (TLMB-NN) training, testing, and validation method, and the recommended model was compared for excellence. Following that, regression analysis, mean square error, and histogram explorations are used to validate the suggested (TLMB-NN). The proposed technique is distinguished based on the proximity of the proposed and reference findings, with an accuracy level ranging from 10^{-9} to 10^{-10} .

Keywords: Maxwell fluid; MHD; boundary layer flow; Brownian motion; thermal radiation; permeable medium; Levenberg–Marquard technique; neural network

1. Introduction

Artificial Neural Networks (ANNs) are a groundbreaking new AI (artificial intelligence) technique. ANNs can grow in a variety of modes, depending on the data that flows through the network throughout the learning process, whether internally or externally.



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). To increase the performance of a Multilayer Perceptron (MLP) network, an artificial neural network uses the Back Propagation (BP) method to undertake simultaneous training. It is the most widely used, effective, and simple-to-learn paradigm for complex multilayered networks. Paul Werbos, who created the back propagation method in 1974, was the first to do so, while Rumelhart and Parker were the first to revive it (see ref. [1]). The Levenberg-Marquardt methodology/algorithm (LMA) is an innovative convergent reliability technique for artificial neural networks (ANNs) that provides a numerical solution to a wide range of fluid flow issues. Several researchers have recently used this method to examine mass and heat-transmission features, along with non-Newtonian fluid flow systems. Raja, M.A.Z et al. [2] suggest neural networks approach with backpropagation to analysis the 3D hall current of Cattaneo–Christov heat flux model relating biconvection nanofluidic flow with Darcy-Forchheimer law influence. Shoaib et al. [3] investigated the generation of entropy under the impact of MHD and thermal radiation using the proficiency of neural networks. Khan et al. [4] used a Backpropagated neural network optimized with Levenberg-Marquardt scheme (BNN-LMS) to investigate heat transport between two permeable parallel plates of steady Nano fluids applying Thermophoresis and Brownian impacts. To explain the third-order nonlinear scheme of Emden-Fowler paradigm, Sabir et al. [5] examined computational intelligence methodology employing Levenberg-Marquardt backpropagation neural networks. Using TLMB-NN based computational intelligence, Uddin et al. [6] showed how to combine magnetic and radiation effects to comprehend the investigation of Maxwell Nano liquid thin film stream across a stretchy and spinning disc.

As the efficiency of appliances and thermal schemes is associated to heat-transfer amounts, engineers and researchers have engaged on the issue of poor thermal conductivity and the subsequent weak heat-transmission factors proposed by convectional fluids, for example, water, glycol, ethylene oil, etc. Choi [7,8] exposed and demonstrated that the upmost-needed greater conducting liquid for improving the cooling scheme in maximum engineering and industrial appliances can be accomplished by combining nanometer-sized particles, for example, caused by carbides, carbon nanotubes, metals and oxides, etc., with conventional heat-transportation fluids. Various investigators have drawn to the fascinating and expressive evaluation of Nano fluids due to the auspicious purposes for example solid-state lighting, nuclear reactors, electronic appliances, safer surgery, and cancer therapy that might enhance heat-transfer competence for an improved cooling method Nayak et al. [9]. Nano fluid characteristics like as viscosity and thermal conductivity have a significant impact on heat-transmission rates, according to Sheikholeslami et al. [10]. As a result, the utilization of ultra-fine solid particles in fluids has affected significantly the improvement of heat-transmission execution. According to Nima et al. [11], such a variety develops in a more conductive heat-transfer liquid, which has uses in electronics, transportation sectors, pharmaceutical sectors, biomedicine, atomic reactors, and power manufacture, etc. According to Eastman et al. [12], the heat-absorption capacity of Nano fluids is significantly higher than that of conventional fluids, with thermal conductivity rising equal to 40% dependent on the size, shape, and thermal properties of solid nanomaterials. Various thermophysical characteristics of Nano fluids have been investigated by many researchers in relation to these important applications, as seen in references [13,14] and their referred references. Concerning the flows in porous medium, the literature review displays that countless explorations of curiosity have been done. In fluid-saturated porous media the convective flow has been mainly inspired by its significant role in many natural and industrial problems in recent studies of interest. The heat-transfer study of incorporating the effects of porosity is significant. Keeping in view the porosity effects, Maleki et al. [15] reported the analysis of nanoliquid over a porous radiative plate. In porous medium for the problem of steady flow over a rotating disk, Mohimanian and Rashidi [16], used the HAM, involving two auxiliary parameters for the analytic estimated solution.

A lot of consideration has been given in recent years for the study of boundary layer flow of magneto hydrodynamics (MHD) and heat transfer owing to its uses in engineering and manufacturing. Pavlov et al. [17] investigated MHD boundary layer flow of an electrically conducting fluid in the existence of a constant transverse magnetic field, and Chakrabarti and Gupta et al. [18] expanded the study to include heat transmission and hydro magnetic flow. Several researchers have approved the exploration of the MHD influence on Nano fluids. Shagaiya Daniel et al. [19] studied that optical grafting, metal casting, crystal growth, metallurgical process, tunable optical fiber filters, the polymer industry, liquid metal cooling blankets for fusion reactors, and including the stretching of plastic sheets are just a few of the many uses of MHD. In a magnetic area, MHD is concerned with the movement of an electrically behaving fluid, which has the potential to regulate the system's flow and heat transmission.

The magnetic field, when applied to nanofluids, magnetizes the flow, creating magnetohydrodynamic flow. The MHD flow under the influence of thermal radiation has always been an interesting area for the researcher. The MHD flow studied the involvement between the electrically conductive fluid and magnetic field. Thermal radiation affects the concentration of molecules and enhances the temperature by increasing energy and molecular movement.

The primitive studies showing anomalous improvements in nanofluid thermal properties over those of the base fluid, specifically the heat-transfer coefficient, have been largely discredited. Thermophysical properties of nanofluid are not designated via classical theories due to their conventional suspensions. Measurements of the thermophysical properties of nanofluids impart only integral information about their transport processes and, as a rule, do not clarify the mechanisms of these processes. The mechanisms of transport processes were studied using the molecular dynamics method. Furthermore, the densities of the nanoparticles material play an important role in the improvement of the thermal conductivities of the nanoparticles. Moreover, the heat-transfer coefficient of the nanoparticles is of great importance due to concentration of the particles involved the fluid. It can accelerate the heat-transfer system in the nanofluids as compared to base fluid [20–22].

The esteem of the Maxwell fluid, which is appropriate to the rate of those kinds of fluids, is owing to its simplicity and ability to anticipate stress relaxation, as well as its tremendous behaviour in engineering and trade activity, particularly in the polymer areas. The research of [23–25] provides appropriate information about Maxwell fluid. Various researchers have been interested in the flow issues with a stable or continually moving flat plate since the past century, because it has numerous technical applications in disciplines such as aerodynamics, naval architecture, and so on. Applying boundary layer theory, Sakiadis [26] investigated the flow through a continually moving flat plate. Merkin [27] explored free stream flow across a vertical flat surface, including the impacts of buoyancy forces. Wilks [28] explained above a fixed flat upright surface the constant free stream flows in the semi-infinite field. Ghalambaz et al. [29] analyzed the mixed convection boundary layer flow and heat transfer over a vertical plate embedded in a porous medium filled with a suspension of nano-encapsulated phase change materials. Similarly, S.A.M. Mehryan et al. [30] explained the natural convection flow of a suspension containing nano-encapsulated phase change particles in an eccentric annulus. Because of buoyancy forces, the flow develops, and a continuous heat flux is delivered to the stationary upright plate. Bachok et al. [31] explained the heat-transmission research of a comparable free stream flow owing to a sliding flat permeable plate. By using boundary layer estimation, Sadeghy et al. [32] analyzed the Maxwell fluid flow across a moving flat plate. Damseh [33] reported the flow of viscoelastic fluid across an infinitely porous perpendicular flat plate with first-order chemical effects. Nadeem et al. [34] explained the MHD Maxwell Nano fluid flow across a flat plate in motion. With boundary coating estimations, Zhao et al. [35] addressed the unsteady naturally convected Maxwell fluid flow through a perpendicular uniform surface. Utilizing boundary layer theory, Bhatti et al. [36] investigated MHD Nano fluid flow through a porous stretched cylinder, as well as the impacts of heat radiation and chemical reactivity. With boundary coating flow assumptions, Bachok et al. [37] explained the Nano fluid flow owing to a uniform moving surface. Employing boundary layer theory, we show the flow of magneto hydrodynamics Maxwell Nano fluid across an upright moving uniform permeable plate with impacts of heat and concentration buoyancy. With radiation and viscous dissipation results, heat-absorbing fluids have deliberated.

Because finding an accurate solution to a problem analytically might be challenging, the investigator uses a combination of numerical and semi-numerical approaches to solve the problem. The Method of Spectral Relaxation [38], HPM [39], Keller Box Method [40], Galerkin finite element method [41], and many others are examples of approaches. All of the mentioned literature on Nano fluid flow for many fluidic systems was formed exploiting and utilizing various numerical and semi-numerical methodologies; however, AI-based numerical computing paradigms are critical to using HTM-BFN model, i.e., to investigate the heat transmission of Maxwell base fluid flow of nanomaterials with MHD above perpendicular moving surfaces. Evolutionary estimation approaches are used in stochastic numerical calculating solvers connected to neural networks to get the solutions/outcomes of differential equations for linear and non-linear, exhibiting different measurements of various circumstances. The engagement of these approaches comprises COVID-19 Models [42,43], mosquito dispersal model [44], atomic physics [45], magneto hydrodynamics [46,47], Emden Fowler system [48,49], thermodynamics [50], nonlinear corneal shape model [51], nanotechnology [52], and flow model of non-linear unipolar electro hydrodynamic pump [53]. All of these inspiring features boost investigators to use a reliable and perfect AI algorithm-based numerical computational model for numerical exploration of the Magneto-hydrodynamic Nano-fluid mathematical paradigm by using numerical and graphical analyses to examine the influence of all variations or physical gauges on velocity, concentration, and temperature profiles. MATLAB and Mathematica tools are used to simulate numerical behavior.

The following are the prominent aspects of the proposed design-computing methodology:

- A new AI-based intelligent computing methodology via Levenberg–Marquardt back propagation with neural networks (TLMB-NN) is used to viably explore the solution dynamics for the heat transfer of Maxwell base fluid flow of nanomaterials (HTM-BFN) with MHD;
- By providing the required equivalent modification, the mathematical modeling of the novel design HTM-BFN in expressions of PDEs has transformed to similar non-linear ODEs;
- Based on Hartmann number, Grashof numbers, concentration Grashoff factor, Lewis number, Brownian motion factor, Thermophoresis factor, Eckert number, Prandtl number, and other characteristics, the Adam's solver is exploited to build a dataset for the designed TLMB-NN as an alternative to the dynamic of HTM-BFN;
- Modeling HTM-BFN for various scenarios by employing the TLMB-NN testing, validation, and training samples based procedures, and evaluation with orientation results rationalizes its perfection; and
- The applicability of the suggested TLMB-NN to successfully represent the HTM-BFN model has supported by convergence graphs of calculated MSE, fitness, histograms, and regression metrics.

The subsequent research has been classified as follows: the interpretation and consequences of the HTM-BFN model problem are described in Section 2; Section 3 presents the solution approach as well as the impacts of the recommended TLMB-NN on numerous HTM-BFN alternatives; and Section 4 concludes with concluding observations and probable future study.

2. Mathematical Interpretation and Flow Assessment

Owing to a vertically moving flat permeable surface, we investigated the laminar, two-dimensional boundary coating flow of magneto hydrodynamics Maxwell nanofluid. The *x*-axis is parallel to the vertically moving flat plate, while the *y*-axis is orthogonal to it. Concentration and thermal buoyancy are other key factors. As consequences with thermal radiation and viscous dissipation, the fluid has been assumed to be heat absorbing.

The fluid has given an unrestricted stream velocity $\overline{U}_e(\overline{x})$, and the velocity $\overline{U}_w(\overline{x})$, to the normally moving surface is given. The pattern of flow is presented via Figure 1. The dimensional boundary layer equations are given as [54].

$$\frac{\partial \overline{u}}{\partial \overline{x}} + \frac{\partial \overline{v}}{\partial \overline{y}} = 0, \tag{1}$$

$$\overline{u}\frac{\partial\overline{u}}{\partial\overline{x}} + \overline{v}\frac{\partial\overline{u}}{\partial\overline{y}} + \lambda(\overline{u}^{2}\frac{\partial^{2}\overline{u}}{\partial\overline{x}^{2}} + \overline{v}^{2}\frac{\partial^{2}\overline{u}}{\partial\overline{y}^{2}} + 2\overline{u}\overline{v}\frac{\partial^{2}\overline{u}}{\partial\overline{x}\partial\overline{y}} = -\frac{1}{\rho}\frac{\partial p}{\partial\overline{x}} + v\left(\frac{\partial^{2}\overline{u}}{\partial\overline{u}^{2}}\right) - \frac{\overline{u}B_{0}^{2}\sigma}{\rho} + g_{0}\beta_{T}(\overline{T} - \overline{T}_{\infty}) + g_{0}\beta_{c}(\overline{C} - \overline{C}_{\infty}),$$
(2)

$$\begin{pmatrix} \overline{u} \frac{\partial \overline{T}}{\partial \overline{x}} + \overline{v} \frac{\partial \overline{T}}{\partial \overline{y}} \end{pmatrix} = \alpha \left(\frac{\partial \overline{T}}{\partial \overline{y}} \right)^2 + \frac{\mu_B}{(\rho C_P)_f} \left(\frac{\partial \overline{u}}{\partial \overline{y}} \right)^2 + \frac{16a^*}{3k^*} \frac{\overline{T_{\infty}^3}}{(\rho C_P)_f} \\ \times \frac{\partial^2 \overline{T}}{\partial \overline{y}^2} + \tau \left(D_B \frac{\partial \overline{T}}{\partial \overline{y}} \frac{\partial \overline{C}}{\partial \overline{y}} + \left(\frac{\partial \overline{T}}{\partial \overline{y}} \right)^2 \right) - \frac{Q_0}{(\rho C_P)_f} (\overline{T} - \overline{T}_{\infty}),$$

$$(3)$$

$$\overline{u}\frac{\partial\overline{C}}{\partial\overline{x}} + \overline{v}\frac{\partial\overline{C}}{\partial\overline{y}} = \left(\frac{\partial^2\overline{T}}{\partial\overline{y}^2}\right)\frac{D_T}{\overline{T}_{\infty}} + \frac{\partial^2\overline{C}}{\partial\overline{y}^2}D_B.$$
(4)

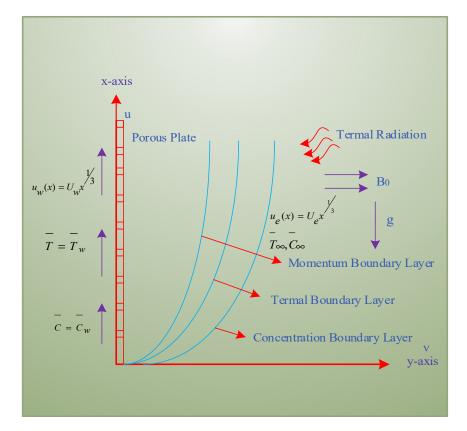


Figure 1. Flow geometry for HTM-BFN model with MHD.

In terms of boundary conditions,

$$\overline{u} = \overline{U}_w(\overline{x}), \quad \overline{v} = \overline{V}_w(\overline{x}), \quad \overline{T} = \overline{T}_w, \quad \overline{C} = \overline{C}_w, \quad at \ \overline{y} = 0
\overline{u} \to \overline{U}_e(\overline{x}), \quad \overline{T} \to \overline{T}_{\infty}, \quad \overline{C} \to \overline{C}_{\infty}, \quad at \ \overline{y} \to \infty,$$
(5)

where the wall dimensional velocity is $\overline{U}_w(\overline{x})$, and $\overline{V}_w(\overline{x})$ is dimensional mass flux velocity where for injection $\overline{V}_w(\overline{x}) > 0$, and for suction $\overline{V}_w(\overline{x}) < 0$. The wall dimensional temperature and concentration are $\overline{T}_w, \overline{C}_w$. The temperature, concentration and dimensional free stream velocity are $\overline{T}_\infty, \overline{C}_\infty, \overline{U}_e(\overline{x})$ respectively. Equation (2) gives outside the boundary layer:

$$-\frac{1}{\rho}\frac{d\overline{p}}{d\overline{x}} = \lambda \overline{U}_e^2 \frac{d^2 \overline{U}_e}{d\overline{x}^2} + \overline{U}\frac{d\overline{U}_e}{d\overline{x}} + \frac{\sigma B_0^2}{\rho}\overline{U}_e,\tag{6}$$

Following are the variables in the boundary layer with no dimensions are:

$$x = \frac{\overline{x}}{L}, \quad y = R_e^{\frac{1}{2}} \left(\frac{\overline{y}}{L} \right), \quad u = \frac{\overline{u}}{U_0}, \quad v = R_e^{\frac{1}{2}} \left(\frac{\overline{v}}{U_0} \right),$$

$$u_e(x) = \frac{\overline{U}_e(\overline{x})}{U_0}, \quad u_w(x) = \frac{\overline{U}_w(\overline{x})}{U_0}, \quad v_w(x) = R_e^{\frac{1}{2}} \frac{\overline{V}_w(\overline{x})}{U_0},$$

$$\theta = \frac{\overline{T} - \overline{T}_{\infty}}{\overline{T_w - T_{\infty}}}, \quad \phi = \frac{\overline{C} - \overline{C}_{\infty}}{\overline{C_w - C_{\infty}}}, \quad p = \frac{\overline{p} - p_{\infty}}{\rho_f U_0^2},$$
(7)

where the characteristic velocity is U_0 . We get the following system of equations by merging Equations (6) and (7):

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{8}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} + \frac{\lambda U_0}{L} \left(u^2 \frac{\partial^2 u}{\partial x^2} + v^2 \frac{\partial^2 u}{\partial y^2} + 2uv \frac{\partial^2 u}{\partial y \partial x} \right) - \left(\frac{\lambda U_0}{L} \right) u_e^2 \frac{d^2 u_e}{dx^2} - u_e \frac{du_e}{dx} = + \frac{\partial^2 u}{\partial y^2} + \left(\frac{\sigma B_0^2 L}{\rho U_0} \right) (u_e - u) + (\overline{T}_w - \overline{T}_\infty) \frac{g_0 \beta_T L}{U_0^2} \theta + (\overline{C}_w - \overline{C}_\infty) \frac{g_0 \beta_c L}{U_0^2} \phi,$$
(9)

$$u\frac{\partial\theta}{\partial x} + v\frac{\partial\theta}{\partial y} = \frac{1}{P_r}\frac{\partial^2\theta}{\partial y^2} + \frac{U_0^2}{C_p(\overline{T_w} - \overline{T_\infty})} \left(\frac{\partial u}{\partial y}\right)^2 + \frac{4R}{3P_r}\frac{\partial^2\theta}{\partial y^2} + \frac{\partial\phi}{\partial y}\frac{\partial\theta}{\partial y}N_b + N_t \left(\frac{\partial\theta}{\partial y}\right)^2 - \frac{Q_0L}{(\rho C_p)_f}\theta,$$
(10)

$$u\frac{\partial\phi}{\partial x} + v\frac{\partial\phi}{\partial y} = \frac{1}{P_r} \left(\frac{1}{L_e} \frac{\partial^2\phi}{\partial y^2} + \frac{N_T}{N_b L_e} \frac{\partial^2\theta}{\partial y^2} \right). \tag{11}$$

The dimensionless boundary conditions have obtained by applying Equation (7) in Equation (5):

$$u = u_w(x), \quad v = v_w(x), \quad \theta = 1, \quad \phi = 1, \quad at \ y = 0$$

$$u \to u_e(x), \quad \theta \to 0, \quad \phi \to 0, \qquad as \ y \to \infty.$$
 (12)

We suppose that $u_w(x)$, and $u_e(x)$, have the subsequent structure $u_w(x) = U_w x^{\frac{1}{3}}$, and $u_e(x) = U_e x^{\frac{1}{3}}$, where the dimensionless constants are U_w , U_e . The similarity transformations are introduced here as:

$$\begin{split} \psi &= U_e^{\frac{1}{2}} x^{\frac{2}{3}} f(\eta), \ \eta = U_e^{\frac{1}{2}} x^{-\frac{1}{3}} y, \ \theta = g(\eta), \\ \phi &= h(\eta), \ u = \frac{\partial \psi}{\partial y}, \ v = -\frac{\partial \psi}{\partial y}, \end{split}$$
(13)

Thus, we get $v_w(x) = -\frac{2}{3}U_e^{\frac{1}{2}}x^{-\frac{1}{3}}s$, where dimensionless transpiration parameter is *s*, and the suction and injection cases are given by s > 0, s < 0, correspondingly. Equations (8)–(12) yield the form, after manipulating the similarity transformations given in Equation (13),

$$3(f'^{2}-1) - 6ff'' + 2\beta(\eta f'^{2}f'' + 1 - f'^{3} + 2f''' f^{2}) -9((M(1-f')f''' + G_{T}g + G_{c}h) = 0,$$
(14)

$$\frac{1}{P_r}\left(1+\frac{4R}{3}\right)g'' + E_c f''^2 + h'g'N_b + g'^2N_t + \frac{2}{3}fg' - Hg = 0,$$
(15)

$$h'' + g'' \frac{N_t}{N_b} + \frac{2}{3} L_e P_r f h' = 0.$$
(16)

Their relative boundary conditions are given as:

$$\begin{cases} f(\eta) = s, \ h(\eta) = 1, \ g(\eta) = 1, \ f'(\eta) = \gamma, \ at \ \eta = 0 \\ f'(\eta) = 1, \ g(\eta) = h(\eta) = 0, \ as \ \eta \to \infty, \end{cases}$$

$$(17)$$

where for moving flat plate $\gamma = \frac{U_w}{U_e}$, is non-dimensional factor. If free stream and moving flat surface are parallel, then $\gamma > 0$, but, if not parallel, then $\gamma < 0$, and for plate at rest $\gamma = 0$. The dimensionless parameters are specified as under:

$$M = \frac{LB_{0}^{2}\sigma}{U_{0}U_{e}x^{-\frac{2}{3}}\rho}, \quad \beta = \frac{\lambda U_{0}U_{e}x^{-\frac{2}{3}}}{L}, \quad G_{c} = \frac{\beta_{c}Lg_{0}(\overline{C}_{w}-\overline{C}_{\infty})}{U_{0}^{2}U_{e}^{2}x^{-\frac{2}{3}}}, \\ G_{T} = \frac{\beta_{T}Lg_{0}(\overline{T}_{w}-\overline{T}_{\infty})}{U_{0}^{2}U_{e}^{2}x^{-\frac{2}{3}}}, \quad L_{e} = \frac{\alpha}{D_{B}}, \quad P_{r} = \frac{v}{\alpha}, \quad N_{t} = \frac{\tau(\overline{T}_{w}-\overline{T}_{\infty})D_{T}}{v\overline{T}_{\infty}}, \\ N_{b} = \frac{\tau(\overline{C}_{w}-\overline{C}_{\infty})D_{B}}{v}, \quad E_{c} = \frac{U_{0}^{2}U_{e}^{2}}{C_{p}-\frac{2}{3}(\overline{T}_{w}-\overline{T}_{\infty})}, \\ H = \frac{Q_{0}L}{U_{0}U_{e}x^{-\frac{2}{3}}(\rho C_{p})_{e}}, \quad R = \frac{4\sigma^{*}\overline{T}_{\infty}^{3}}{kfk^{*}}$$
(18)

where *M* is the Hartmann number, β denote the Deborah number, G_c and G_T represent the concentration and thermal Grashoff parameters, *Le* denote the Lewis number, P_r show the Prandtl number, N_t and N_b represent the Thermophoresis and Brownian motion parameters, Eckert number is indicated by E_c , *H* display the heat-absorption factor, and *R* signify the Radiation parameter. The Nusselt number N_{ux} , is specify as:

$$N_{ux} = \frac{xq_w}{k(T_w - T_\infty)}$$

where

And

$$q_w = -k\left(1 + \frac{16\sigma^* T_\infty^3}{3k^* kf}\right) \left(\frac{\partial T}{\partial y}\right)_{y=0},$$

$$\operatorname{Re}_{x}^{-\frac{1}{2}}Nu_{x} = -\left(1 + \frac{4R}{3}\right)g'(0).$$

the Sherwood quantity is expressed as:

$$Sh_x = \frac{xh_m}{D_B(C_w - C_\infty)},$$

where, $h_m = -D_B \left(\frac{\partial C}{\partial y}\right)_{y=0'}$ and $\operatorname{Re}_x^{-\frac{1}{2}} Sh_x = -h'(0)$.

In above q_w , h_m are the mathematical representations, which describe the heat slope of wall and mass of wall incline, correspondingly.

3. Solution Methodology

In the shape of a neural network structure, Figure 2 displays the suggested TLMB-NN model. The suggested TLMB-NN is accomplished by operating 'nf tool', i.e., in Mat lab's neural network (NN) toolbox, setting a procedure for fitting NN tools, whereas the Levenberg–Marquardt with backpropagation is concluded, finding out the weight of neural networks. In Figure 3a, the suggested TLMB-NN model and the mathematical model along with concern geometry have displayed and in Figure 3b the overall elaboration of flow demonstration has presented, while the necessary details of the size and structure of the networks is tabulated in Table 1.

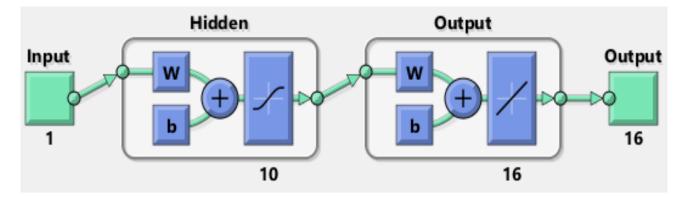
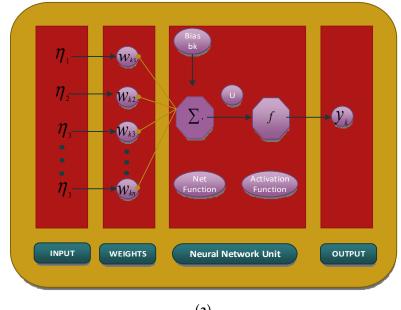
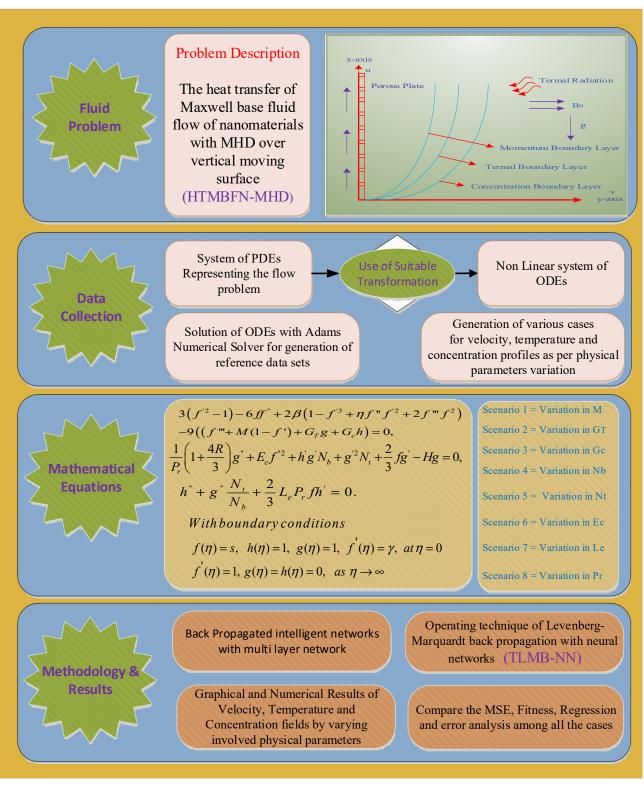


Figure 2. Design of Neural Network for HTM-BFN model.

For fixed values of $\beta_D = 0.5$, R = 0.6, and H = 0.3 are exercised for the variation of distinct parameters M, G_T , G_c , N_t , N_b , E_c , L_e , and P_r respectively, with four cases of HTM-BFN model, individually. With replacements for all alternatives, as stated in Table 1, the suggested TLMB-NN is operated to solve differential Equations (14)–(16) of the flow paradigm for eight scenarios, exploiting the Adams numerical solver method [55–57]; that is in Mathematica software the command 'Nonlinear differential system (ND Solver)' is exercised with time interval 0.01 to generate dataset of TLMB-NN for inputs between 0 and 2 as deliberate below in Tables 1 and 2. With a set of 10 hidden neurons, for training 80% data values, 10% individually for validation and testing the solutions for f', g and h for 201 input points are informally scattered.



(a) Figure 3. Cont.



(b)

Figure 3. (a) Configuration of a particular neuron paradigm and (b) overall working flow chart.

Index	Description
Layer structure	One input, one output, and one hidden layer
Hidden neuron	10–20
Validation	10-fold cross validation
Input grid	201 points
Output grid	16×201 points
Training samples	80%
Validation samples	10%
Testing samples	10%
Leaning methodology	Levenberg–Marquardt
Label target data	Created with Adams numerical method

Table 1. Size and structural details of the networks.

 Table 2. Scenarios interpretation beside with cases for HTM-BFN model with MHD.

Scenarios	Cases -	Physical Quantities of Concern							
Scenarios		M	G_T	Gc	N _b	N_t	Ec	Le	P_r
	C1	0.1	0.2	0.2	0.1	0.1	0.3	0.3	6.5
1	C2	0.3	0.2	0.2	0.1	0.1	0.3	0.3	6.5
1	C3	0.5	0.2	0.2	0.1	0.1	0.3	0.3	6.5
	C4	0.7	0.2	0.2	0.1	0.1	0.3	0.3	6.5
	C1	0.3	0.1	0.2	0.1	0.1	0.3	0.3	6.5
2	C2	0.3	0.2	0.2	0.1	0.1	0.3	0.3	6.5
2	C3	0.3	0.3	0.2	0.1	0.1	0.3	0.3	6.5
	C4	0.3	0.4	0.2	0.1	0.1	0.3	0.3	6.5
	C1	0.3	0.2	0.1	0.1	0.1	0.3	0.3	6.5
2	C2	0.3	0.2	0.2	0.1	0.1	0.3	0.3	6.5
3	C3	0.3	0.2	0.3	0.1	0.1	0.3	0.3	6.5
	C4	0.3	0.2	0.4	0.1	0.1	0.3	0.3	6.5
	C1	0.3	0.2	0.2	0.2	0.1	0.3	0.3	6.5
4	C2	0.3	0.2	0.2	0.4	0.1	0.3	0.3	6.5
4	C3	0.3	0.2	0.2	0.6	0.1	0.3	0.3	6.5
	C4	0.3	0.2	0.2	0.8	0.1	0.3	0.3	6.5
	C1	0.3	0.2	0.2	0.1	0.3	0.3	0.3	6.5
-	C2	0.3	0.2	0.2	0.1	0.5	0.3	0.3	6.5
5	C3	0.3	0.2	0.2	0.1	0.7	0.3	0.3	6.5
	C4	0.3	0.2	0.2	0.1	0.9	0.3	0.3	6.5
6	C1	0.3	0.2	0.2	0.1	0.1	0.1	0.3	6.5
	C2	0.3	0.2	0.2	0.1	0.1	0.3	0.3	6.5
	C3	0.3	0.2	0.2	0.1	0.1	0.5	0.3	6.5
	C4	0.3	0.2	0.2	0.1	0.1	0.7	0.3	6.5

Scenarios	Cases -	Physical Quantities of Concern							
		M	G_T	G _c	N _b	N_t	E _c	L _e	P_r
	C1	0.3	0.2	0.2	0.1	0.1	0.3	0.1	6.5
-	C2	0.3	0.2	0.2	0.1	0.1	0.3	0.3	6.5
7	C3	0.3	0.2	0.2	0.1	0.1	0.3	0.5	6.5
	C4	0.3	0.2	0.2	0.1	0.1	0.3	0.7	6.5
	C1	0.3	0.2	0.2	0.1	0.1	0.3	0.3	5.5
8	C2	0.3	0.2	0.2	0.1	0.1	0.3	0.3	6
	C3	0.3	0.2	0.2	0.1	0.1	0.3	0.3	6.5
	C4	0.3	0.2	0.2	0.1	0.1	0.3	0.3	7

Table 2. Cont.

4. Results and Discussion

The TLMB-NN outcomes for the HTM-BFN model have been shown in Figures 4–9 for different circumstances (scenarios) (1 to 8). Figures 4–6 show the outcomes of eight scenarios in terms of performance and transition phases: M, G_T , G_c , N_t , N_b , E_c , L_e , and P_r . The fitting plots and error histograms in Figures 7–9 were stated in terms of solution with error for four distinct situations, however, the regression estimations exhibited for four unique HTM-BFN model with MHD, collections in Figures 10–12. In addition, for every HTM-BFN model scenario, Table 3 lists the convergence achieve parameter in terms of mean square error (MSE), execution, performed period, performance duration, back propagation, and temporal complexity gauges for scenarios 1 to 8.

In Figure 4a,c,e, Figure 5a,c,e and Figure 6a,c,e for test processes, the convergence of MSE, validation, and training progressions for eight scenarios of the HTM-BFN model with MHD are considered. MSE nearby 9.7×10^{-10} , 8.16×10^{-10} , 1.41×10^{-9} , 4.24×10^{-9} , 4.91×10^{-7} , 6.51×10^{-9} , 1.03×10^{-9} , and 2×10^{-9} , with epochs 274, 245, 433, 574, 402, 486, 371, and 282, correspondingly, provided the finest network performance. The lower the MSE number, the more precise and effective the performance of the given approach may be. The estimates of step size Mu and Levenberg–Marquardt gradient are compactly (10^{-8} , 10^{-8} , 10^{-8} , 10^{-6} , 10^{-6} , 10^{-9} , and 10^{-8}) and (9.98×10^{-8} , 9.97×10^{-8} , 9.98×10^{-8} , 9.98×10^{-8} , 5.43×10^{-6} , 1.01×10^{-6} , 2.54×10^{-6} , and 9.97×10^{-8}) are presented in Figure 4b,d,f, Figure 5b,d,f and Figure 6b,d,f. The aforesaid outputs and graphical validations identify the authenticity that TLMB-NN is efficient, precise, and convergent for each case of HTM-BFN paradigm.

Figures 7–9 demonstrate the effectiveness of the HTM-BFN model by comparing the generated outcomes of eight different scenarios for inputs ranging from 0 to 2 with a step range of 0.01 to reference numerical Adams method outcomes and related outcomes, as well as the error dynamics plot. The highest error for test, train, and validation gauges achieved through suggested TLMB-NN for eight scenarios of the design paradigm is less than 9×10^{-10} , 8×10^{-10} , 1×10^{-9} , 4×10^{-9} , 4×10^{-7} , 7×10^{-9} , 2×10^{-9} , and 2×10^{-9} , while the error dynamics and outcomes of HTM-BFN model for eight detached scenarios is also inspected for every input point aside from error histograms are shown in Figures 7–9, correspondingly. The average value of error bin about comparison zero line has error nearby for eight distinct situations of the HTM-BFN model -1.4×10^{-6} , 3.06×10^{-6} , 5.98×10^{-6} , -6.3×10^{-6} , 2.6×10^{-4} , -1.6×10^{-5} , -1.2×10^{-6} , and 4.07×10^{-6} . Correlation analyses have frequently used to summarize the analysis inside regression analyses. Figure 10 through Figure 13 show the impacts of the HTM-BFN model's eight related alternatives. The correlation R-values are continuously near to unity, implying that the optimal value for training, testing, and validation for precise modeling is close to unity, which explains how effectively TLMB-NN resolves the HTM-BFN model.

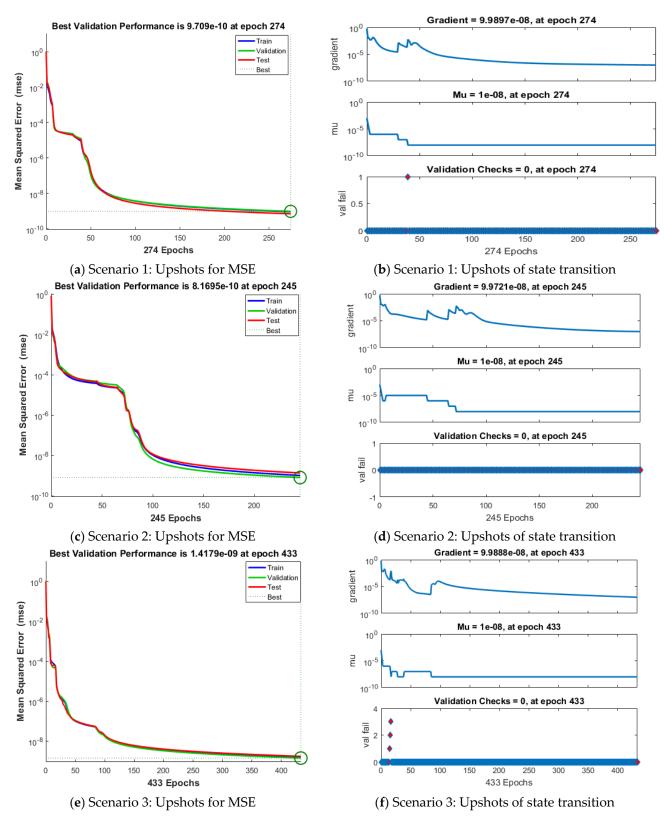


Figure 4. Solution of performance and state transition of proposed TLMB-NN for solving HTM-BFN model with MHD for scenarios 1–3.

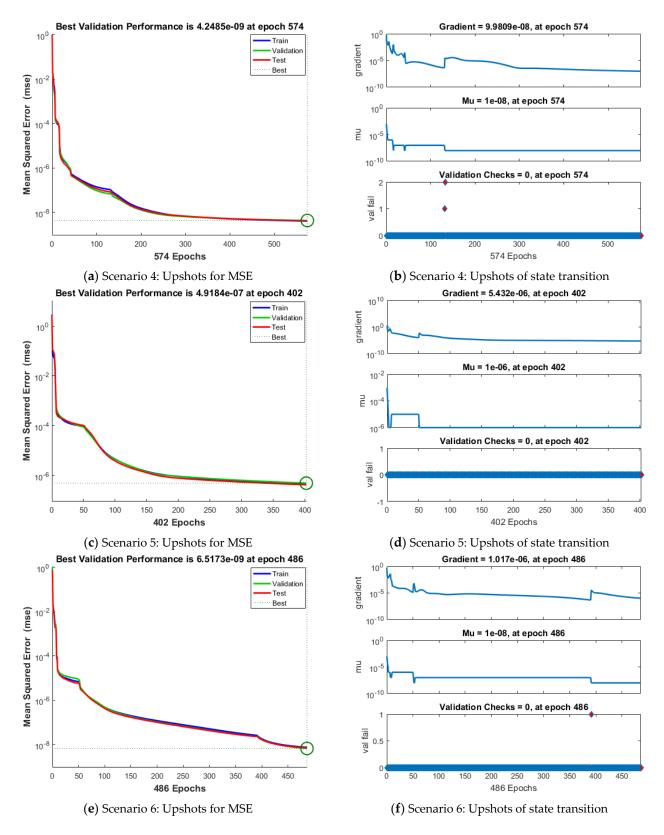


Figure 5. Solution of performance and state transition of proposed TLMB-NN for solving HTM-BFN model with MHD for scenarios 4–6.

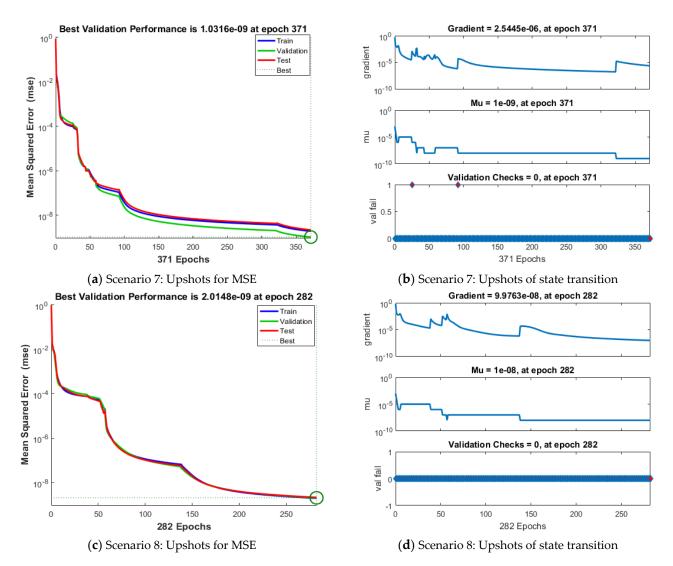
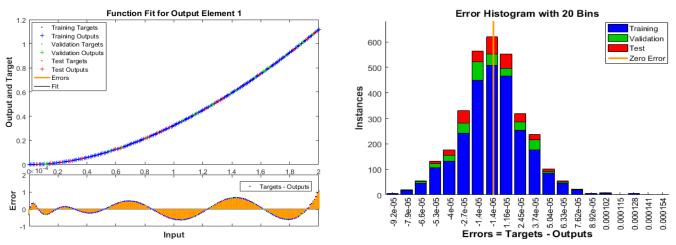
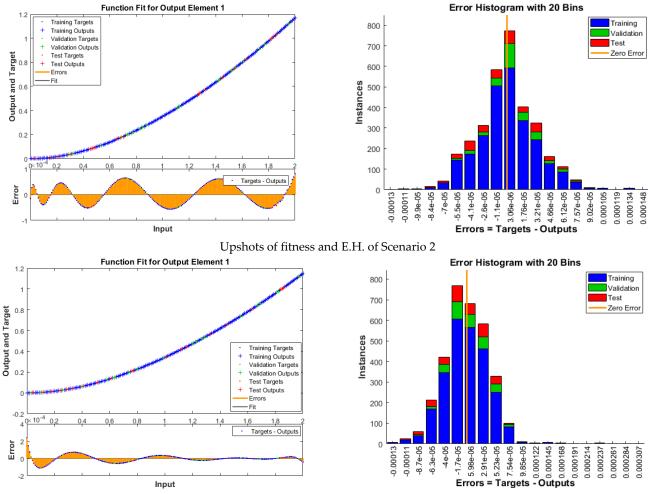


Figure 6. Solution of performance and state transition of proposed TLMB-NN for solving HTM-BFN model with MHD for scenarios 7 and 8.



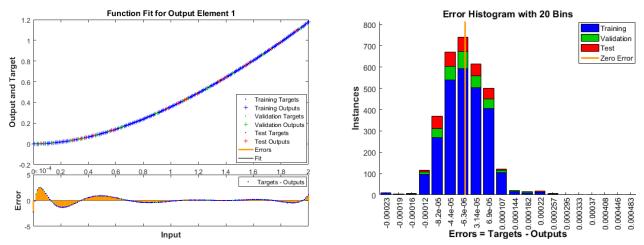
Upshots of fitness and E.H. of Scenario 1

Figure 7. Cont.



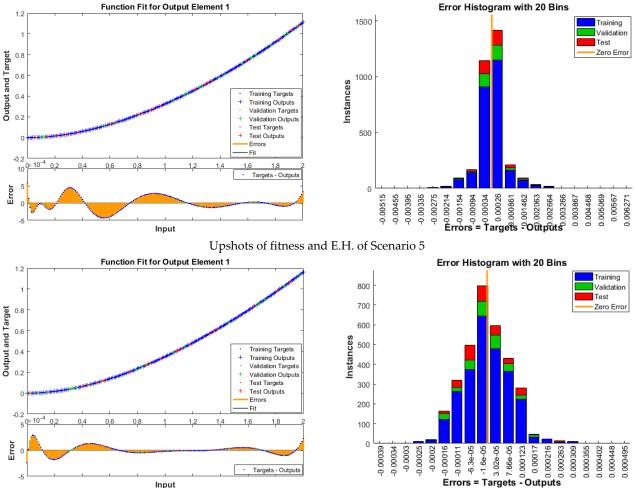
Upshots of fitness and E.H. of Scenario 3

Figure 7. Solution of fitness and error histogram of proposed TLMB-NN for solving HTM-BFN model with MHD for scenarios 1–3.



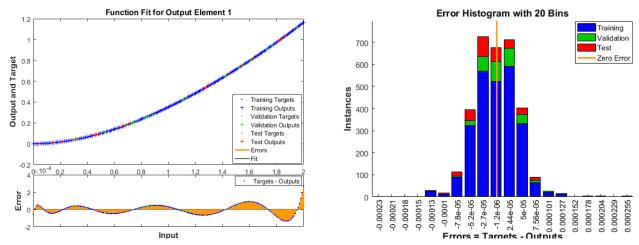
Upshots of fitness and E.H. of Scenario 4





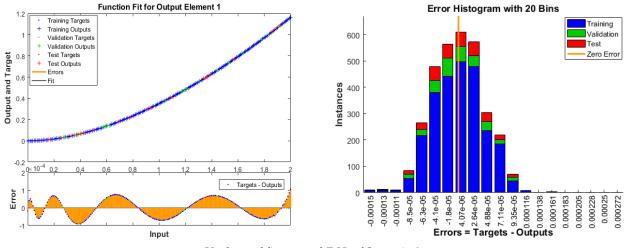
Upshots of fitness and E.H. of Scenario 6

Figure 8. Solution of fitness and error histogram of proposed TLMB-NN for solving HTM-BFN model with MHD for Scenarios 4–6.



Upshots of fitness and E.H. of Scenario 7





Upshots of fitness and E.H. of Scenario 8

Figure 9. Solution of fitness and error histogram of proposed TLMB-NN for solving HTM-BFN model with MHD for Scenarios 7 and 8.

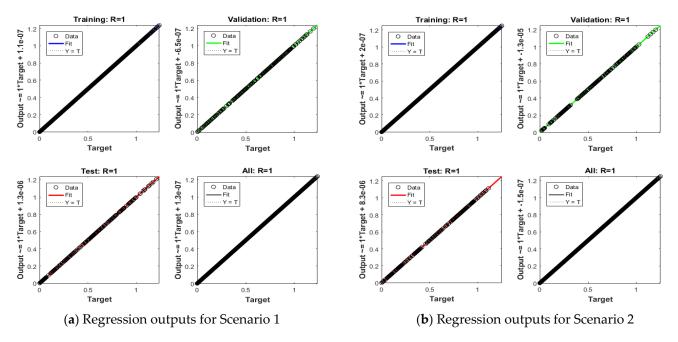


Figure 10. Regression performance of the proposed TLMB-NN for solving HTM-BFN model with MHD of Scenarios 1 and 2.

Furthermore, the associated numerical data in Table 3 demonstrate that MSE performance for the suggested TLMB-NN technique is approximately 10–10 for various HTM-BFN model situations (1 to 8). The numerical results in Table 3 demonstrate that, while solving the HTM-BFN model, TLMB-NN executions are sound.

The effects of TLMB-NN are shown in Figures 14–16, respectively, for velocity distribution $f'(\eta)$, temperature distribution $g(\eta)$, and concentration distribution $h(\eta)$ for all eight scenarios of the (HTM-BFN) paradigm. In Figure 14a,c,e, the influence of velocity profile $f'(\eta)$ on the variation of Hartmann number M, thermal Grashoff parameter G_T and concentration Grashoff parameter G_c for scenarios 1, 2, and 3 of the (HTM-BFN) model is measured; on the other hand, in Figure 14b,d,f, the related values of AE are plotted in order to attain the performance of the HTM-BFN model approach.

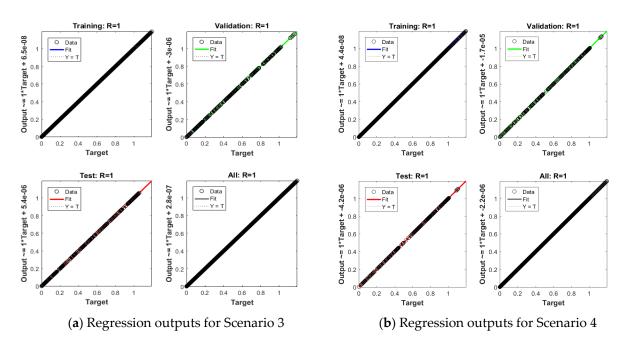


Figure 11. Regression performance of the proposed TLMB-NN for solving HTM-BFN model with MHD of Scenarios 3 and 4.

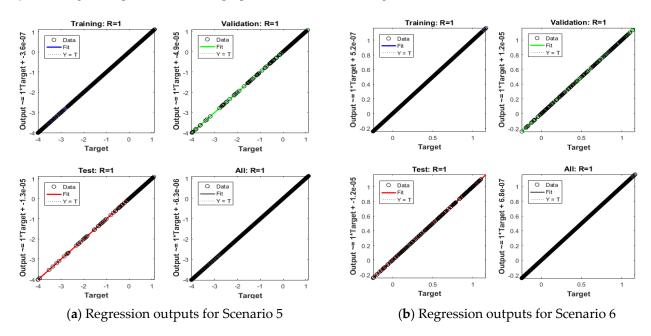


Figure 12. Regression performance of the proposed TLMB-NN for solving HTM-BFN model with MHD of Scenarios 5 and 6.

Figure 14a,c,e illustrates graphs of velocity versus various physical parameter values. As seen in Figure 14a–c, the velocity increases in magnitude by increasing the values of M, G_T and G_c . Figure 14a depicts the alteration in Hartmann number for velocity distribution. When the magnetic field's effect is increased, the flow accelerates, causing the velocity distribution to accelerate. The influence of thermal Grashof number G_T and concentration Grashoff parameter G_c on velocity distribution is explained in Figure 14c,e, and we detect that the velocity increases when G_T and G_c magnitudes escalate. There might be some overlapping between the reference and proposed solutions. As a conclusion, for scenarios (4, 5, and 6) of the HTM-BFN model, Figure 15a,c,e illustrate the results of different magnitudes for Brownian motion parameter N_b , Thermophoresis parameter N_t , and Eckert number E_c for temperature profile $g(\eta)$. In Figure 15b,d,f the appropriate values of AE are determined. As demonstrated in Figure 8a,c, both the parameters N_b and N_t have

the same influence on the temperature distribution, as temperature rises with improving values of these parameters. Furthermore, due to thermophoresis and Brownian motion, the temperature is increased by adding more heating when the nanoparticles and fluid reach a specific point. As a result, the thermal barrier layer thickens, increasing N_t and N_b values, and the temperature near the permeable sheet swiftly rises. As the Eckert number E_c has been raised, the temperature profile accelerates, as seen in Figure 8e. Moreover, the results reveal a consistent overlap between the recommended and reference outcomes. For scenarios 7 and 8, Figure 16a,c depicts the impact of the concentration profile $h(\eta)$ for various values of physical parameters, however, Figure 16b,d depicts the suitable value of AE. Figure 9a,c shows that raising the Lewis number L_e and the Prandtl number P_r lowers the concentration profile $h(\eta)$. This observation also demonstrates that the suggested and reference solutions are always overlapping.

Table 3. Outcomes of TLMB-NN for eight scenarios (HTM-BFN model) with MHD.

Scenarios		MSE Level		Execution	Gradient	Mu	Epoch	Time
Scenarios	Training	Validation	Testing	Execution	Glaulent	Iviu		
М	9.249×10^{-10}	$9.709 imes 10^{-10}$	$7.092 imes 10^{-10}$	$9.25 imes 10^{-10}$	$9.99 imes10^{-8}$	$1.00 imes10^{-8}$	274	12
G_T	$1.039 imes 10^{-9}$	8.169×10^{-10}	$1.380 imes 10^{-9}$	$1.04 imes 10^{-9}$	$9.97 imes10^{-8}$	$1.00 imes 10^{-8}$	245	12
G _c	$1.677 imes 10^{-9}$	$1.417 imes 10^{-9}$	$1.742 imes 10^{-9}$	$1.68 imes 10^{-9}$	$9.99 imes10^{-8}$	$1.00 imes 10^{-8}$	433	32
N _b	3.9720×10^{-7}	$4.248 imes 10^{-9}$	$4.092 imes 10^{-9}$	$3.97 imes 10^{-9}$	$9.98 imes 10^{-8}$	$1.00 imes 10^{-8}$	574	31
Nt	$4.607 imes10^{-7}$	$4.918 imes10^{-7}$	$4.232 imes 10^{-7}$	$4.61 imes 10^{-7}$	$5.43 imes 10^{-6}$	$1.00 imes 10^{-6}$	402	29
Ec	$7.368 imes10^{-9}$	$6.517 imes10^{-9}$	$6.931 imes10^{-9}$	$7.37 imes 10^{-9}$	$1.02 imes 10^{-6}$	$1.00 imes10^{-8}$	486	20
Le	$1.883 imes 10^{-9}$	$1.031 imes 10^{-9}$	$2.151 imes10^{-9}$	$1.88 imes 10^{-9}$	$2.54 imes10^{-9}$	$1.00 imes 10^{-10}$	371	27
P_r	$1.931 imes 10^{-9}$	$2.014 imes10^{-9}$	$2.113 imes 10^{-9}$	$1.93 imes 10^{-9}$	$9.98 imes10^{-8}$	$1.00 imes 10^{-8}$	282	12

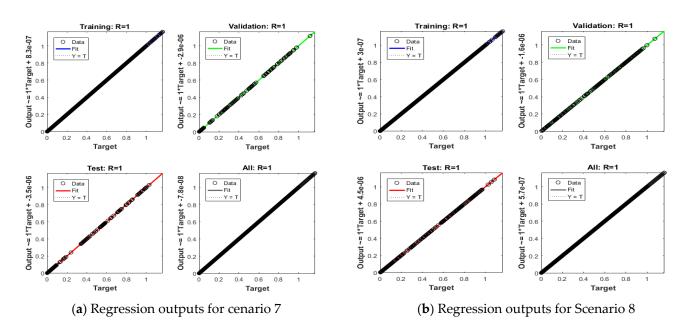


Figure 13. Regression performance of the proposed TLMB-NN for solving HTM-BFN model with MHD of Scenarios 7 and 8.

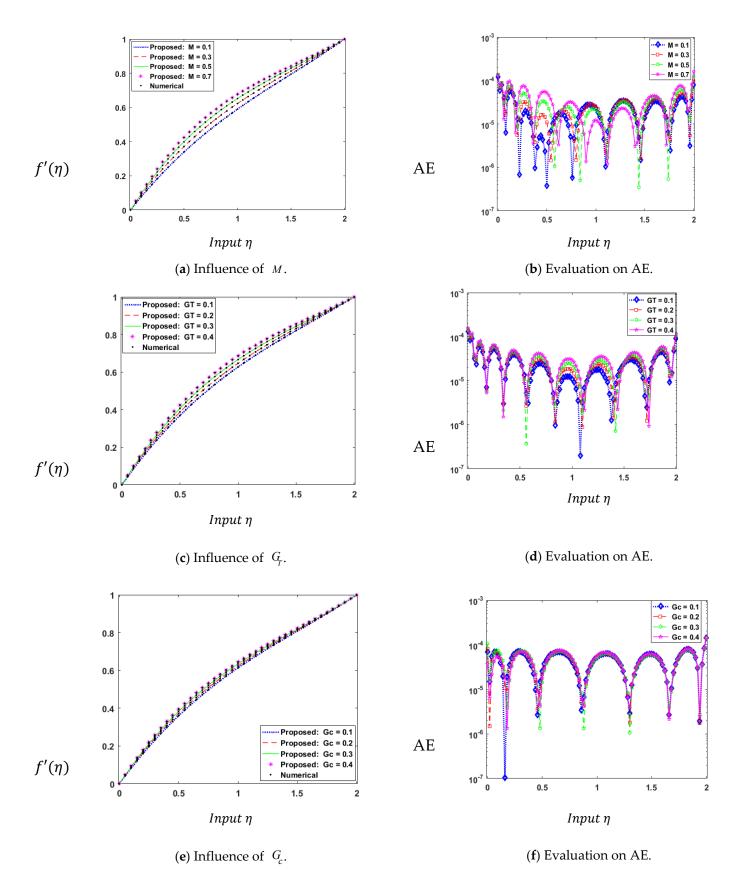


Figure 14. Evaluation of suggested TLMB-NN with outcomes of reference dataset for Scenarios 1–3 of HTM-BFN model with MHD.

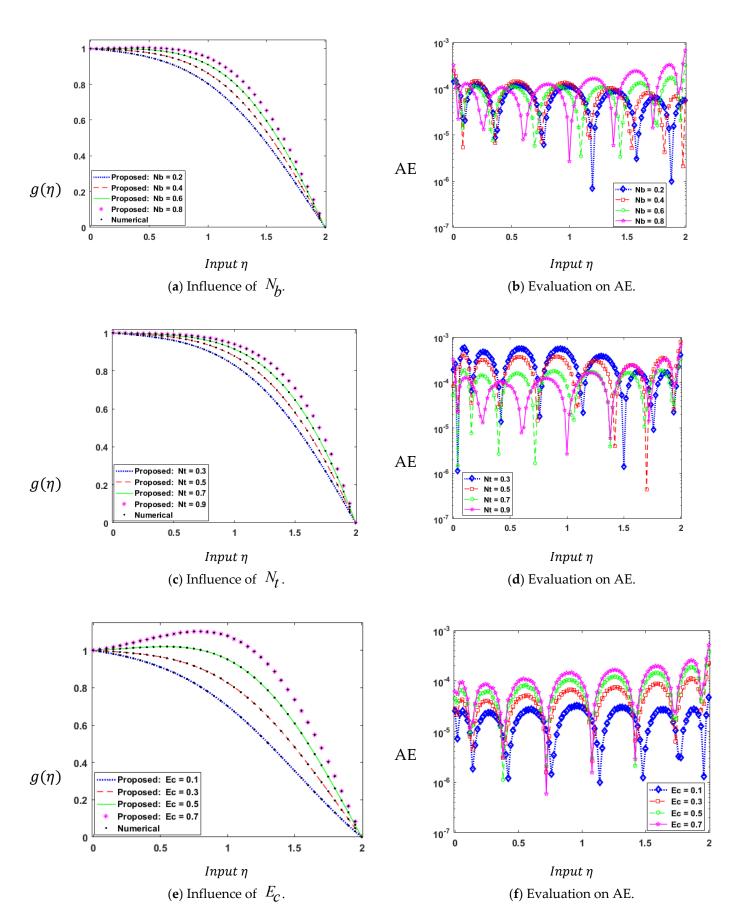


Figure 15. Evaluation of suggested TLMB-NN with outcomes of reference dataset for Scenarios 4–6 of HTM-BFN model with MHD.

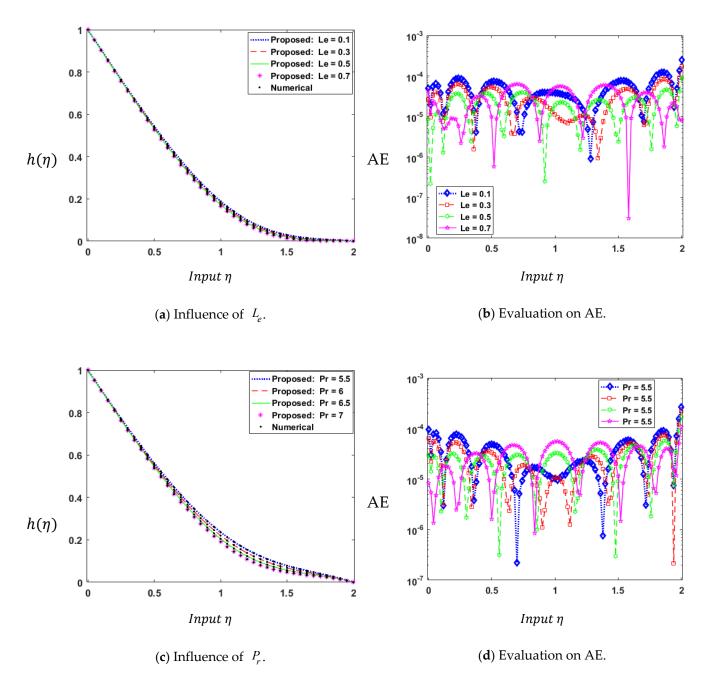


Figure 16. Evaluation of suggested TLMB-NN with outcomes of reference dataset for Scenarios 7 and 8 of HTM-BFN model with MHD.

For all eight scenarios, the findings of TLMB-NN paired with conventional Adam numerical solutions, so the absolute error was revealed to approach the precision measurements from suggestion solutions, and the results are exhibited in Figure 14b,d,f and Figure 15b,d,f for scenarios 1, 2, 3, 4, 5, and 6, together with subgroups 16 (b, d) for scenarios 7 and 8. For velocity profile, the AE achieve values for scenarios 1, 2, 3 are 10-6 to 10-4, 10-7 to 10-4, and 10-7 to 10-4, respectively, as shown in Figure 14b,d,f. While values for scenario 4, 5, and 6 in Figure 15b,d,f for temperature profile are approximately 10-7 to 10-4, 10-8 to 10-2, and 10-8 to 10-4. Likewise, the AE achieves values 10-7 to 10-4 and 10-7 to 10-4 for scenarios 7 and 8 for the concentration profile shown in the subgroup 16 (b,d). The TLMB-NN computing approach solves HTM-BFN model variations with sufficient, convergent, and vigorous productivity in all of these numerical and graphical examples.

In the boundary conditions for moving flat plate, $\gamma = \frac{U_w}{U_e}$, is the non-dimensional parameter. Here γ is positive when the free stream and moving flat surface are parallel then but, if not parallel, then γ is negative and for the plate at rest γ it will be zero. Similarly, *s* is the dimensionless transpiration parameter. For the suction and injection cases, *s* is specified by s > 0, s < 0, respectively.

5. Conclusions

The influence of Maxwell base fluid flow of heat transfer of nanomaterials with MHD above perpendicular moving surfaces has been investigated computationally in this research, using the HTM-BFN model with MHD. The solution of a mathematical model exhibiting HTM-BFN with change of specific circumstances (scenarios) has examined using the Levenberg–Marquardt neural networks approach with backpropagation procedure. The form of PDEs describing the transformation of a mathematical flow into a scheme of non-linear ODEs employing suitable similarity variables conversion system. The Adams numerical approach has operated to generate the dataset for the HTM-BFN model, including deviations of several physical measurements like Hartmann number, Grashof number, Prandtl number, Brownian motion, and thermophoresis parameters. The HTM-BFN reference dataset is created by modifying different variants, with 80%, 10%, and 10% of the dataset being used for TLMB-NN training, testing, and validation, respectively. The scheme's excellent performance is observed through the matching of suggested and reference results around 10^{-9} to 10^{-10} , along with graphical and numerical illustrations of error histogram plots of convergence, regression dynamics, and mean square errors.

In future, to solve fluid mechanics problems [58–61] and a collection of computer virus propagation models in the networks [62,63], and information security [64]; the TLMB-NN design and its latest improved types could be used effectively. Similarly, in forthcoming studies the authors intend to work on the mathematical modelling of the problems involving the boundary layer theory, according to the suggested correct shapes of velocity and temperature profiles [65,66]. Moreover, the proposed AI-based intelligent computing methodology using neural networks with deep learning is definitely helpful for learning the physical dynamics of conduction heat transfer more efficiently, reliably, and effectively.

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Nomenclature

x, y (m)	Cartesian coordinate system	G_T	Thermal Grashof number
$v ({\rm m}^2{\rm s}^{-1})$	Kinematic viscosity	G _C	Concentration Grashoff parameter
$q_w (wm^{-2})$	Surface heat flux	R	Radiation parameter
σ*	Stefann Boltzman constant	P_r	Prandtl number
D_B	Brownian diffusion coefficient	E_C	Eckert number
L_e	Lewis number	$E_C k^*$	Coefficient of Mean absorption
N_t	Thermophoresis factor	N_b	Brownian motion parameter
β	Deborah number	h_m (kgs ⁻¹ m ⁻²)	Surface mass flux
U_w, U_e	Dimensionless constants	U_0	Characteristic velocity
H	Heat absorption factor	Nu_x	Nusselt number
D_T	Thermophoretic diffusion coefficient	MSE	Mean square error
MHD	Magnetohydrodynamics	ANN	Artificial neural networks
ODEs	Ordinary differential equations	PDEs	Partial differential equations
HTM-	Heat transfer of Maxwell base	TLMB-	Technique of Levenberg-
BFN	fluid flow of nanomaterials	NN	Marquardt back propagation with neural networks

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