Supercritical Antisolvent Processing of Nitrocellulose: Downscaling to Nanosize, Reducing Friction Sensitivity and Introducing Burning Rate Catalyst

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Nomenclature

Α	Pre-exponential factor
ABPR	Automated back pressure regulator
В	Burn rate coefficient
CNTs	Carbon nanotubes
Ea	Apparent activation energy
EtOH	Ethanol
f	Feeding rate of NC-solution/suspension
F	Feeding rate of CO ₂
MBPR	Manual back pressure regulator
MeOH	Methanol
micron-NC	Nitrocellulose microfibers (raw nitrocellulose)
п	Pressure exponent
nano-NC	Nitrocellulose nanoparticles
NC	Nitrocellulose
NC(sc)	Nitrocellulose particles obtained by SAS process
NC/CNT(sc)	Nitrocellulose composite with CNTs obtained by SAS process
$NC/Fe_2O_3(sc)$	Nitrocellulose with nano-Fe2O3 obtained by SAS process
NC/CNT/Fe ₂ O ₃ (sc)	Nitrocellulose with CNTs and nano-Fe ₂ O ₃ obtained by SAS process
Р	Pressure
Pc	Critical pressure of CO ₂
RDX	1,3,5-trinitro-1,3,5-triazinane
SAS	Supercritical Anti-Solvent process
sc-CO ₂	Supercritical carbon dioxide
SEM	Scanning electron microscopy
Tc	Critical temperature of CO ₂
TEM	Transmission electron microscopy
U	Burning rate

Section S1. Experimental Methods

Electron microscopy. Target-oriented approach was utilized for the optimization of the analytic measurements [1]. Before measurements the samples were mounted on a 25 mm aluminum specimen stub and fixed by conductive adhesive. Metal coating with a thin film (10 nm) of platinum/palladium alloy (80/20) was performed using magnetron sputtering method as described earlier [2]. The observations were carried out using Hitachi SU8000 field-emission scanning electron microscope (FE-SEM). Images were acquired in secondary electron mode at 2 kV accelerating voltage. Morphology of the samples was studied taking into account possible influence of metal coating on the surface [2].

Samples morphology was studied also using Hitachi transmission electron microscope (TEM). Before measurements the samples were mounted on a 3 mm copper grid and fixed in a grid holder. Images were acquired in bright-field TEM mode at 100 kV accelerating voltage.

Atomic force microscopy. Morphology of the samples was revealed by scanning probe microscopy (NTEGRA Prima microscope, NT-MDT) with \leq 10 nm and ~1nm cantilevers. Powdered samples were pressed in small pellets and its surface was monitored in semi-contact or contact scanning modes.

Specific surface area. The BET surface area was determined using FlowSorb III 2305 (Micromeritics) instrument by measuring the adsorption of a gas mixture (30%N₂/70%He) on the surface of powder. *Elemental analysis* was revealed by Perkin Elmer 2400 Series analyzer.

Thermal analysis. Thermogravimetric (TGA) runs were performed with Netzsch STA 449 F3 thermal analyzer. Samples ca. 1 mg weight have been poured in alumina pans, covered with pierced lids, and linearly heated at 5 K min⁻¹ rate in argon flow. Differential scanning calorimetry (DSC) was registered in separate experiments in Netzsch DSC 204 HP apparatus. Nearly 0.5 mg of samples were placed in aluminum crucibles, covered with pierced lids, and linearly heated with the same rate of 5 K min⁻¹ in nitrogen flow.

Friction sensitivity was determined in full set of experiments according to STANAG 4487 [3].

Section S2. Starting Materials

Scanning electron and probe microscopy have been used to disclose the morphology of the involved powders. Figures S1a, b represent the view of as-received nitrocellulose fibers showing a smooth surface with some cracks. Carbon nanotubes appeared as the elongated tortuous objects. In line with the manufacturer specification [4] the inner diameter of CNTs is ca.10 nm, the outer diameter is near 20 nm, and the length is no less than 2 μ m (Figures S1c, b). Iron oxide is formed mainly by nanoparticles as evidenced from both types of microscopy (Figure S1e, f). The specific surface area for nano-Fe₂O₃ after degassing the powder at 120 °C is 12.8 ± 0.3 m² g⁻¹, higher thermosetting (300 °C) reveals the larger value of 14.3 ± 0.3 m² g⁻¹. High purity carbon dioxide (Russian standard TU 2114-006-05015259-2014) and acetone (Russian standard TU 2633-012-29483781-2009) were used for synthesis.



Figure S1. Microstructure of (a, b) untreated micron-sized NC fibers, (c, d) carbon nanotubes, (e, f) nano-sized iron oxide.

Section S3. Details of the SAS process

Table S1 summarizes the performed experiments with identification of the following governing parameters: the nozzle diameter *D*, autoclave pressure *P*, the ratio between solution (suspension) and CO₂ feeding rates (f/F), the volume of solvent *V*, the NC mass m(NC) and its concentration in solution (suspension), w(NC), the additive type present, and the characteristics of the final product – its morphology and yield (*N* stands for number of runs).

expt #	<i>D</i> , μm	P, bar	<i>f/F</i> , cm³/g	V, ml	<i>m</i> (NC), g	<i>w</i> (NC), wt.%	CNT	Fe ₂ O ₃	Product appearance	Yield, %	Ν
1	150	100	1/50	20	0.159	1	-	-	uniform powder	81	1
2	150	110	1/50	20	0.158	1	-	-	gel-like recovered product	39	2
3	150	90	1/50	20	0.158	1	-	-	gel-like recovered product	11	1
4	150	120	1/50	20	0.158	1	-	-	gel-like recovered product	13	1
6	150	100	2/50	40	0.316	1	-	-	gel-like recovered product	27	1
7	150	100	1/50	31	0.488	2	-	-	gel-like recovered product	59	1
8	150	100	1/50	20	0.488	3	-	-	gel-like recovered product	39	1
9	200	100	2/50	30	0.288	1	-	-	gel-like recovered product	43	1
10	100	100	4/50	30	0.288	1	-	-	gel-like recovered product	45	1
11	760	90	1/50	40	0.675	2	-	-	"herring-bone" structures and uniform powder on filter	83	1
12	760	90	2/50	61	1.084	2	-	-	"herring-bone" structures and uniform powder on filter	85	1
13	760	90	4/50	61	1.087	2	-	-	"herring-bone" structures and uniform powder on filter	82	1
14	760	100	4/50	61	1.067	2	-	-	"herring-bone" structures and uniform powder on filter	83	1
15	760	120	1/50	61	1.024	2	-	-	uniform powder	88	1
16	760	120	4/50	61	1.012	2	-	-	uniform powder	88	1
17	760	100	2/50	126	1.004	1	-	-	"herring-bone" structures and uniform powder on filter	92	1
18	760	100	2/50	41	1.023	3	-	_	uniform powder	87	1

Table S1. SAS process parameters for NC modification

19	150	120	2/50	30	0.5	2	-	-	gel-like recovered product	-	1
20	760	100	1/50	63	1	2	-	-	uniform powder	88	2
21	760	100	1/50	61	1.08	2	+	-	uniform powder	88	2
22	760	100	1/50	40	0.634	2	+	+	uniform powder	87	1
23	760	100	2/50	61	1	2	-	-	uniform powder	86	1
24	760	150	1/50	40	0.668	2	-	-	uniform powder	96	1
25	760	120	2/50	60	1	2	-	-	uniform powder	91	20
26	760	120	2/50	61	1.06	2	-	+	uniform powder	91	2
27	760	100	2/50	61	1.024	2	+	-	uniform powder	87	3
28	760	100	2/50	61	1.019	2	+	+	uniform powder	93	2
29	760	100	2/50	61	1.011	2	-	+	uniform powder	89	2
30	760	120	2/50	61	1.097	2	-	-	uniform powder	86	1

Nickel and copper salicylates were intended to be introduced same as the iron oxide since they are known as catalysts for NC-based propellants [5]. But both salts appeared to be soluble in acetone-CO₂ binary system, thus not suitable for the selected process.

Section S4. Morphology of Nano-NC

Particle size distribution for nano-NC powder has been obtained by counting particles in AFM images. Typical AFM image is presented in Figure S2 and details of the numerical particle-size distribution can be found in Table S2.



Figure S2. AFM image of nitrocellulose powder produced via SAS process.

Table S2. Parameters of the particle-size distribution of nano-NC powder

Number of particles	216
Average diameters	
<d>, μm</d>	194
D43, μm	276
Cummulative distribution	
D10, μm	80
D50, μm	180
D90, μm	290
Log-normal approximation	
Xc, μm	195
σ	0.46

Section S5. Determination of catalyst content in fabricated composites

Considering the non-100% recovery of the product for NC composites with additive (see Table S1), the exact additive content in material can differ from that in original suspension, i.e., 1 wt.% of CNTs and 5 wt.% of nano-Fe₂O₃ above the 100% of NC. To check if this content remains the same in the final product, we perform the gentle annealing of the composites to receive the iron oxide residue. Figure S3 illustrates the heating program, the key issue is to use the low heating rates and sample masses during NC-core decomposition to prevent ignition of the sample and low recovery of the residue (e.g., 0.5 wt.% after 10 K/min heating to 300°C in preliminary tests). Sample loads were near 10 mg, low enough to eliminate self-heating, and appropriate to give a sufficient accuracy of weighting the residue.

We start with mechanical mixture of NC/CNT/Fe₂O₃ where there should be no loss of material during preparation. Brown residue after tests is 5.5 ± 0.2 wt.% of the initial mass, close to target $5/(100 + 1 + 5) \cdot 100 = 4.7\%$ considering the sampling inhomogeneity, weighting errors, and especially the not-complete annealing of the carbonaceous residues. For composites prepared with SAS process, the catalyst content was $5.3 \pm 0.5\%$ for NC/Fe₂O₃(sc) and $5.0 \pm 0.3\%$ for NC/CNT/Fe₂O₃(sc).



Figure S3. Temperature and mass profiles during annealing of NC-based composites with Fe₂O₃ addition.

Section S6. Thermokinetic analysis

Figure S4 shows the results of formal kinetic analysis of DSC curves obtained at 0.5-5 K/min for micron-(a) and nano-(b) NC. Non-linear regression estimates of the kinetic parameters and information criteria showing that single-step kinetic models outperform the two-step models are presented in figures.



Figure S4. Results of formal kinetic analysis for micron- (a) and nano-(b) sized nitrocellulose. Computations performed in THINKS thermokinetic software [6].

The obtained kinetic parameters were compared with the extensive data from review by Brill and Gongwer [7]. Figure S5 shows that our results fall to the kinetic compensation line that is supposed to include the autocatalytic reaction parameters.



Figure S5. Data from review [7] and the results of the current study.

Section S7. Combustion tests

Figure S6 shows the images of pressed nitrocellulose samples before and after experiment, as well as a frame from video during combustion. For nano-sized NC the amount of residue is notably higher that for micro-sized sample.



Figure S6. Combustion of untreated (a-c) and processed (d-f) nitrocellulose: (a, d) view of pellet before test, (b, e) still image of the burning surface, (c, f) residue after experiment. Length of white bar is 1 mm.

Analogously, the views of the samples before, during, and after combustion are presented in Figure S7. The additive type apparently influences the appearance of the combustion surface, the view and amount of the combustion residue.



Figure S7. Combustion nitrocellulose with additives of nano-iron oxide (a-c), carbon nanotubes (d-f) and both Fe_2O_3 and CNTs (g-i) : (a, d, g) view of pellet before test, (b, e, h) still image of the burning surface, (c, f, i) residue after experiment. Length of white bar is 1 mm.

Samples have been pressed at 300 MPa in cylinders with 6 mm diameter. Charges of two pellets (~0.5 g) were coated on the lateral surface and put in Crawford bomb. Combustion at 2 MPa of nitrogen was monitored by pressure rise and video-registration (at 1200 fps). Filming of the burning surface (2000 fps) was performed on uncoated 5 mm pellets in open air.

#	Sample	Density, g cm- ³	Porosity, %	Burnin	g rate, mm s-1at	P [MPa]	Parameters in $U = B \cdot P^{\wedge} v$		
	builipie			2	8	12	В	υ	R^2
1	NC	1.41 ± 0.01	15	4.0 ± 0.1	10.9 ± 0.5	13.8 ± 0.5	2.24 ± 0.08	0.75 ± 0.02	0.998
2	NC(sc)	1.40 ± 0.05	15	5.0 ± 0.1	10.2 ± 0.5	13.1 ± 0.5	3.17 ± 0.11	0.57 ± 0.02	0.998
3	NC/CNT(sc)	1.42 ± 0.02	15	5.0 ± 0.3	10.6 ± 0.5	13.2 ± 0.5	3.2 ± 0.2	0.57 ± 0.03	0.996
4	NC/Fe ₂ O ₃ (sc)	1.44 ± 0.05	13	4.5 ± 0.8	13.1 ± 0.5	13.1 ± 0.5	a	<u>a</u>	_a
5	NC/CNT/Fe ₂ O ₃ (sc)	1.44 ± 0.05	13	4.8 ± 0.3	12.8 ± 0.6	15.8 ± 0.6	2.8 ± 0.2	0.71 ± 0.03	0.995
6 ^b	NC/CNT/Fe ₂ O ₃	1.43 ± 0.01	14	5.3 ± 0.3	11.8 ± 0.6	14.6 ± 0.6	3.4 ± 0.2	0.60 ± 0.03	0.999

 Table S3. Results of combustion experiments

^a Values cannot be fitted by a single power dependency.

^b Composition #6 was prepared by dry mixing of the as-received NC, iron oxide and CNTs. All attempts to mix in liquid with ultrasonic vibrations or mechanical agitation result in films that even when cut in small pieces reveal the serious cracking in pressed pellets.



Figure S8. Combustion velocity against pressure for all involved compositions.

Video 1 is available at <u>https://youtu.be/UwP2gr4oHuo</u> Video 2 is available at <u>https://youtu.be/rs3KKf5Uk6w</u> Video 3 is available at <u>https://youtu.be/UE8-GHeiIWM</u> Video 4 is available at <u>https://youtu.be/VcvbKoOyNv8</u> Video 5 is available at <u>https://youtu.be/MmoUUPHsFOo</u> Video 6 is available at <u>https://youtu.be/xeesBCVG_MU</u>

Section S8. References

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