



Article

Experimental Study and Thermodynamic Analysis of Hydrogen Production through a Two-Step Chemical Regenerative Coal Gasification

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Abstract: Hydrogen, as a strategy clean fuel, is receiving more and more attention recently in China, in addition to the policy emphasis on H_2 . In this work, we conceive of a hydrogen production process based on a chemical regenerative coal gasification. Instead of using a lumped coal gasification as is traditional in the H_2 production process, herein we used a two-step gasification process that included coking and char-steam gasification. The sensible heat of syngas accounted for 15–20% of the total energy of coal and was recovered and converted into chemical energy of syngas through thermochemical reactions. Moreover, the air separation unit was eliminated due to the adoption of steam as oxidant. As a result, the efficiency of coal to H_2 was enhanced from 58.9% in traditional plant to 71.6% in the novel process. Further, the energy consumption decreased from 183.8 MJ/kg in the traditional plant to 151.2 MJ/kg in the novel process. The components of syngas, H_2 , and efficiency of gasification are herein investigated through experiments in fixed bed reactors. Thermodynamic performance is presented for both traditional and novel coal to hydrogen plants.

Keywords: hydrogen production; gasification; thermodynamic analysis; fixed bed reactor

1. Introduction

As a result of the new round of hydrogen energy economy flourish, hydrogen production from coal is receiving increased research focus. Hydrogen is vital to future energy systems. It is clean, carbon free, and an important material for chemical industries [1–3]. Moreover, H_2 can be used to generate power, drive cars, and synthesize chemicals such as methanol and ethanol, but unfortunately cannot be gained from natural gas reservoirs [4,5]. Therefore, there is great significance in retrieving efficient hydrogen production from other sources. Compared with other hydrogen production options for China, coal to H_2 has a strategic importance due to the country's large amount of coal reserves.

Coal to hydrogen technology is based on coal gasification, which originated early last century [6,7]. The process has been developed over the past 20 years in China in conjunction with several commercialized projects [8,9]. The basic process involves coal gasification, water gas shift (WGS), and gas separation. Coal gasification is the main unit that decides the whole plant efficiency. Currently, the majority of coal to hydrogen processes employ GE and Shell gasification, which uses oxygen as an oxidant. Further, the cold gas efficiencies are typically lower than 80% [10,11]. Nevertheless, the low cold gas efficiency and use of oxygen limits coals hydrogen efficiency to less than 60% [12,13]. In recent years, several alternative coal gasification technologies have been proposed, including Huaneng TPRI (Thermal Power Research Institute) and transport integrated gasification (TRIG). These new technologies have a higher cold gas efficiency and are able to improve coal to hydrogen efficiency [14,15]. However, most of these

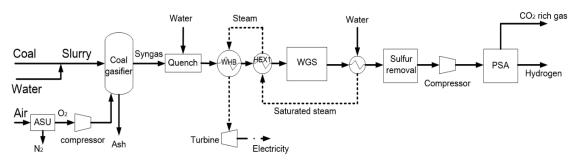
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technologies still need oxygen for gasification, a process which results in huge power consumption. Another coal to hydrogen process is based on supercritical water gasification [16–18]. This technology does not require pure oxygen and is expected to be highly efficient. Many previous experiments have been carried out to prove these findings [16–18]. For example, hydrogen mole fraction for this technology was reported to be higher than 70% [16–18]. Nevertheless, supercritical water coal gasification operates over 20 MPa and may result in a higher cost for the gasifier. There are some publications relative to the topic of hydrogen production through steam gasification of coal, char, and biomass [19–23]. Herein, thermodynamic and kinetic analysis are presented.

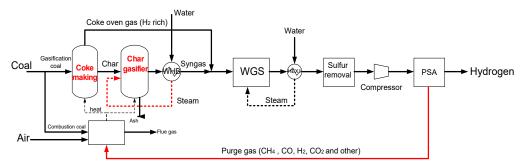
In our previous paper [24], a two-step chemical regenerative coal gasification was proposed and a much higher cold gas efficiency was reported. Moreover, in the two-step gasification, gas with high H_2 concentration was produced. In this paper, a coal to hydrogen process based on this gasification is presented. Experiments were carried out in fixed bed reactors and components of syngas, H_2 , are reported. Additionally, thermodynamic performance of the whole process is simulated.

2. Hydrogen Production Based on a Two-Step Chemical Regenerative Coal Gasification

In a traditional coal to hydrogen plant, GE or Shell gasification is typically employed. Figure 1a shows the most popular process based on GE gasification, wherein coal is mixed with water to produce slurry. The slurry reacts with oxygen from an air separation unit (ASU) to produce syngas containing CO and H_2 . Water is used to quench the syngas and then a waste heat boiler (WHB) is used to recover heat. Afterward, syngas is sent to a water gas shift (WGS) where sulfur removal and a pressure swing adsorption (PSA) unit are used to produce high purity H_2 . Limited by the low cold gas efficiency of gasification, it is typically lower than 80% [10,11]. Considering a huge power consumption for ASU, the efficiency of coal to hydrogen in such a traditional plant is lower than 60% (LHV based) [12,13].



(a) Traditional hydrogen production process from coal



(b) Hydrogen production based on a two-step chemical regenerative coal gasification

Figure 1. (a) Traditional hydrogen production process from coal. (b) Proposed hydrogen production process based on a two-step chemical regenerative coal gasification.

In this novel process, a two-step chemical regenerative coal gasification is proposed for H_2 production (Figure 1b). Coal gasification is divided into two steps: coke making and char gasification. The coke making process can drive volatile out of coal and can get char and high H_2 concentration

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gas, i.e., coke oven gas (COG). For char-steam gasification, steam is used to recover syngas sensible heat, providing part of the heat requirement of the char-steam reaction. Through such a chemical regenerative pathway, the sensible heat of the syngas can be converted into the chemical energy of the syngas, wherein cold gas efficiency of gasification is expected to be lifted. To produce H_2 , COG and syngas will be sent to the WGS unit, sulfur unit, and PSA unit. Moreover, the purge gas from the PSA unit mainly contains CH_4 , H_2 , CO, and CO_2 and can be recovered to combust together with coal, which provides heat for coke making and char-steam gasification. Furthermore, no oxygen is needed for coal gasification and consequently ASU is eliminated.

3. Experimental Setup and Results

The gasification unit is the key unit for the proposed hydrogen production process. Several experiments have been carried out for validation.

3.1. Experimental Setup

In this study, the experiment equipment mainly includes char making, steam generation, char-steam gasification, and a gas analyzer. First, coal is dried in a burner at 101 °C for 12 h after being crushed into powder under 2 mm. Then it is placed in a vacuum tube for char and coke oven gas (COG) production. The infrared-heated reaction tube has a maximum heating rate of 50 °C/s and can heat the coal to 1000 °C in 20 s. COG gas is collected by bags after processing water washing, cooling, and filter. The prepared char will be placed in a fixed bed reactor to react with steam that is generated in a steam generator. Gas from char-steam reactor is detected through an online gas analyzer (GA) and collected by bags. Aglient 490pro chromatogram is used to analyze the final components of all collected gases. The experiment setup is shown in Figure 2.

3.2. Typical Results of Char Making

Bituminous coal, the components of which are shown in Table 1, is used, wherein char is prepared at 900 $^{\circ}$ C at a heating rate 25 $^{\circ}$ C/s. The components and production of COG and char are presented in Tables 2 and 3. It can be seen that through the coke making process, COG gas with high H₂ concentration can be made.

Table 1. Components and lower heating value of coal sample.

С	Н	0	N	S	ASH	LHV, KJ/KG
74.3%	4.7%	10.7%	0.87%	0.33%	9.1%	26,835.8

Table 2. Components of coke oven gas (COG) production.

Component	COG
СО	21.9%
H_2	51.7%
O_2	1.7%
N_2	9.0%
CH_4	11.6%
H_2O	-
H_2S	0.1%
CO_2	3.5%
C_2H_4	0.5%
Volume Per kg Coal	563.85 L

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Component	Char
С	94.94%
Н	0.55%
О	0.39%
N	-
S	-
Ash	4.12%
Char Yield, kg Per kg Coal	59.33%

Table 3. Components of char.

3.3. Typical Results of Char-Steam Gasification

Next, 10 g char is placed in the reaction tube and 0.2 g/mL steam is sent to gasify the char at $1000-1100~^{\circ}$ C. The char conversion ratio is 54.0% at $1000~^{\circ}$ C after 1 h. Online gas components of products at different temperatures are shown in Figures 3–5 (each experiment at different temperatures is repeated three times; the average values of gas components are used in the figures). H_2 concentration is typically higher than 70% and the rest mainly includes CO and CO_2 . Besides carbon reaction with steam, it can be inferred from the gas fraction of carbon dioxide that the water gas shift reaction also occurred to further convert CO into H_2 and CO_2 .

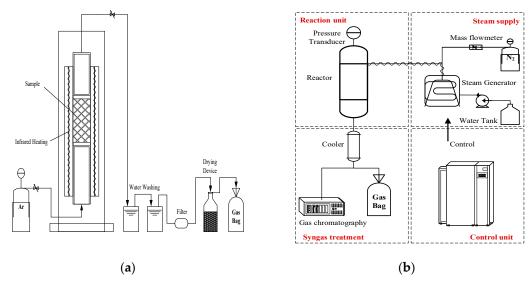


Figure 2. Experimental setup for (a) char making and (b) char-steam gasification [24].

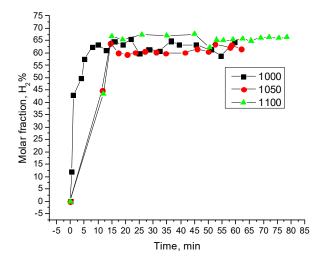


Figure 3. Online H₂ fraction from char-steam gasification at different tempeatures.

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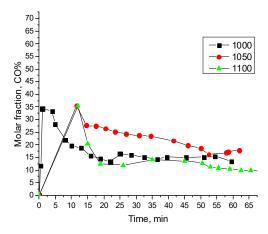


Figure 4. Online CO fraction from char-steam gasification at different tempeatures.

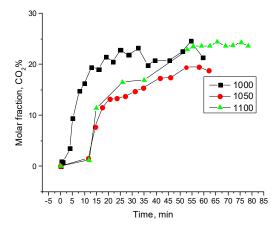


Figure 5. Online CO₂ fraction from char-steam gasification at different tempeatures.

4. Thermodynamic Performance Comparison and Discussion

Based on the above experimental results, thermodynamic performance of the whole process is presented in this section. ASPEN PLUS software V8.2 was used for process simulation and the PR-BM method was selected. Next, 1300 °C and 4 MPa was assumed for GE gasification; 1100 °C and 2.5 MPa was assumed for char-steam gasification. In the proposed process, part of the coal was sent to the combustion chamber to provide heat to coking and char-steam reaction. The temperature of combustion was 1150 °C and the temperature of flue gas was 120 °C. The PSA unit for both processes operated at 5 MPa and the purity of the H_2 product was 99.9%. Three indicators were used to evaluate thermodynamic performance, as shown in Equations (1)–(3). Cold gas efficiency represented the ratio of converting chemical energy of coal into syngas. The coal to hydrogen efficiency denoted the amount of chemical energy of coal converted into hydrogen product. Exergy efficiency stood for the ratio of the exergy of H_2 product to the exergy of feed coal.

Coal to hydrogen efficiency = Lower heating value of hydrogen product/Lower heating value of coal (2)

Experimental results of char making process were directly used for char-steam gasification simulation. Further, the simulated results of syngas components agreed well with the experiments presented in Figure 3. A thermodynamic analysis showed that coal to hydrogen efficiency based on chemical regenerative gasification was as high as 71.6% (LHV based), which was far higher than

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58.9% of traditional GE gasification-based plant. Moreover, the energy consumption for unit hydrogen production decreased from 183.8 MJ/kg in a traditional plant to 151.2 MJ/kg in this novel process. The efficiency upgrade was mainly caused by the improvement of cold gas efficiency during coal gasification, in addition to being brought by the reduction of power consumption for air separation (Table 4). By recovering the sensible heat of syngas to drive gasification reaction, sensible heat was converted into the chemical energy of syngas and thereby the cold gas efficiency of chemical regenerative gasification was lifted by 5.6%. Adopting steam instead of pure oxygen as an oxidant reduced the power consumption for air separation (Table 5). Thus, the coal input for the auxiliary power generation is reduced, which further helped improve the whole plant efficiency. To disclose the reason for system performance enhancement, exergy analysis is also presented in Table 6. The exergy efficiency of the novel coal to hydrogen plant was 78.5%, which was 13.9 percentage points higher than the traditional plant. It can be seen that the efficiency upgrade was mainly a result of the reduction in exergy destruction of coal gasification, air separation, auxiliary power generation, and heat recovery of syngas units. Eliminating the air separation unit reduced exergy destruction by 3.1 percentages and the coal gasification unit (including char making and char gasification) reduced exergy destruction by 4.3 percentages. Because there is no power consumption for air separation, the exergy destruction in auxiliary power generation unit also decreased by 2.3%. Furthermore, recovery of syngas sensible heat instead of quenching reduced exergy destruction by 2.8%.

Table 4. Thermodynamic performance of the hydrogen production plant.

Item	Hydrogen Production Based on Chemical Regenerative Gasification		Hydrogen Production Based on GE Gasification	
	Total System	Input		
Energy Input, kJ				
Coal input for gasification (including to gasifier and combustion unit)	25,842.9	96.3%	24,071.7	89.7%
Coal input for auxiliary power generation	992.9	3.7%	2764.1	10.3%
subtotal	26,835.8	100.0%	26,835.8	100.0%
	Gasification 1	Island		
Energy Input, kJ				
Coal input for gasification	25,842.9	-	24,071.7	-
LHV of purge gas recovered from PSA	4588.9	-	-	-
Subtotal	30,431.8		24,071.7	
Gas output from gasifier and COG, kJ	25,333.0		18,677.7	-
Cold gas efficiency of gasification		83.2%		77.6%
	WGS and PS	A Unit		
Energy Output, kJ				
Hydrogen	19,214.4		15,806.3	
LHV of purge gas	4588.9		-	
	Coal to H ₂ Eff	iciency		
Coal to H ₂ efficiency		71.6%		58.9%
Energy consumption for unit hydrogen production, MJ/kg		151.2		183.8

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Table 5. Power balance of the plant.

Item	Hydrogen Production Based on Chemical Regenerative Gasification	Hydrogen Production Based on GE Gasification	
Power Produced, kJ			
Power from auxiliary power generation	397.2	1105.6	
Power from heat recovered	-	358.4	
subtotal	397.2	1464.0	
Power Consumption in Each Unit,	kJ		
ASU	-	898.2	
Oxygen compression	-	434.8	
PSA	397.2	131.0	
Subtotal	397.2	1464.0	

Table 6. Exergy balance of the hydrogen production plant.

Item	Hydrogen Production Based on Chemical Regenerative Gasification		Hydrogen Production Based on GE Gasification			
Total System Input						
Exergy Input, kJ						
Coal input for gasification (including to gasifier and combustion unit)	26,876.6	96.3%	25,034.6	89.7%		
Coal input for auxiliary power generation	1032.6	3.7%	2874.6	10.3%		
subtotal	27,909.2	100.0%	27,909.2	100.0%		
	Exergy Destruc	tion				
Air separation and oxygen compression	-	-	865.2	3.1%		
Coal gasification (including char making and char gasification)	3070.0	11.0%	4270.1	15.3%		
Quench or heat recovery of syngas	753.5	2.7%	1535.0	5.5%		
WGS	669.8	2.4%	641.9	2.3%		
Shifted gas cooling	195.4	0.7%	725.6	2.6%		
PSA unit	697.7	2.5%	614.0	2.2%		
Auxiliary power generation	614.0	2.2%	1255.9	4.5%		
Subtotal	6000.5	21.5%	9879.9	35.4%		
	Exergy Outp	ut				
Exergy Output, kJ						
Hydrogen	21,908.7	78.5%	18,029.3	64.6%		
1	Exergy Efficiency of	Coal to H ₂				
Exergy efficiency of coal to H ₂		78.5%		64.6%		

5. Conclusions

In this study, a hydrogen production process based on a chemical regenerative coal gasification was conceived. A two-step gasification process that employed coking and char-steam gasification was adopted instead of a lumped coal gasification, as is commonly done in the traditional H_2 production process. Experimental results shows that by the adoption of two-step gasification, COG gas with high H_2 purity and syngas with H_2 over 70% were both produced. The efficiency of coal to H_2 can be enhanced from 58.9% in the traditional plant to 71.6% in the novel process. The lifting of coal to hydrogen efficiency were mainly accomplished using the cold gas efficiency improvement due to recovering and converting the sensible heat of syngas into the chemical energy of syngas through

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thermochemical reactions. Further, the reduction of auxiliary power consumption was caused by the elimination of the air separation unit.

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