

Article

Research on the Principle of a New Flexible Screw Conveyor and Its Power Consumption

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Abstract: A new screw conveyor with flexible discrete spiral blades is proposed to solve the problem of particle material gathering between the screw and the tube wall in the traditional screw conveyor. With a theoretical analysis, the power consumption model of the screw conveyor with flexible discrete spiral blades is built. Then, its practicability is verified by simulation and experimental testing. The simulation results show that the increase of the spiral angle will raise the transportation speed of the particles. The diameter of the flexible blades raises with the increase of the power consumption of the screw conveyor. The experimental testing verified the analysis and simulation results.

Keywords: screw conveyor; flexible blades; simulation; power consumption; test

1. Introduction

Screw conveyors are widely used in modern production and in the logistics of transporting granular materials [1]. When traditional rigid screw conveyors convey sticky bulk materials, the phenomenon of material gathering at the inner wall happens. This will reduce the transmission efficiency of the screw conveyer.

A flexible tube screw conveyor is proposed in this study to expand the self-loading range. The chief shaft and outer tube are made of rubber, and the screw blade is made of continuous-rigidity plastic. The conveyor to swing widely in a broaden range for the flexibility [2]. A method is proposed to reduce the wear and tear of the screw conveyor. In addition, the power consumption variation of the conveyor transmission affected by the structure parameters of the screw is analyzed [3]. The filling factor of the screw conveyor is a key point for the transmission efficiency. It can be determined by using a ribbon-type screw at different screw speeds [4]. A feeding device based on equal diameter and dual-spiral is designed for animals feeding. The structure parameters and rotary speed are optimized with the simulation software EDEM. Then, the theoretical results are verified by an experimental test [5].

In this paper, a flexible, discrete spiral blades screw conveyor is proposed. The power consumption parameters when using a flexible helical blade structure were studied by theoretical analysis and simulation experiments.

2. Analysis of the Mechanical Properties of a Single Flexible Blade

2.1. The Radial Analysis of a Single Blade

Since the fiber length is slightly longer than the inner diameter of the tube wall, the wall of the nylon fiber is shown in Figure 1. A nylon fiber can be idealized as an elongated cylindrical rod. The force passing through the center of the rod cross section, perpendicular to the rod's axis, is the radial force.

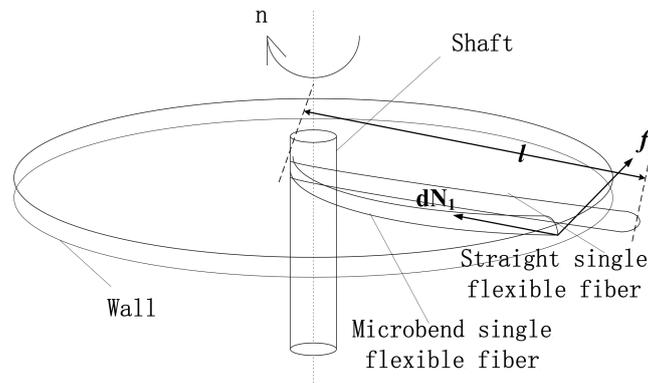


Figure 1. A single flexible blade radial force diagram.

According to Figure 1, the single fiber bundle length is l , dN_1 is a single fiber bend preloaded force, f_2 is the radial wall of the axial preload force of friction. The fiber bundle is slightly longer than the diameter of the wall.

A single fiber bend force dN_1 is:

$$dN_1 = \frac{\pi^3 E d_s^4}{256 l^2} \quad (1)$$

where E is the elastic modulus of the material, d_s is the diameter of the single nylon fiber, l is the distance between the working point and the supporting point.

2.2. The Axial Analysis of a Single Blade

The flexible blades are the elements of the screw conveyor. As a mechanical element, they must possess adequate strength and rigidity. When the end of the nylon fiber axis is fixed on the shaft, the other end is free, so this structure can be considered as a flexible cantilever beam of nylon fibers. The nylon fibers are thin cylinders, and the cross section of each fiber is circular. The force analysis is shown in the Figure 2.

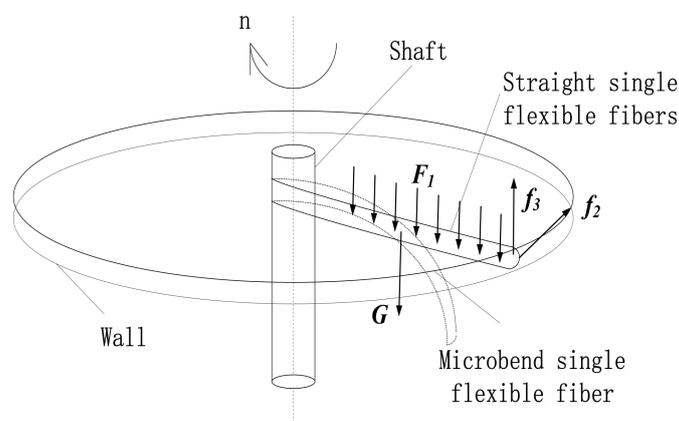


Figure 2. Single flexible helical blade axial force diagram.

In the Figure 2, F_1 is caused by the weight of the material of the uniformly distributed load. Since there is no granule material, the study of the screw conveyor is an idealization. f_3 is the radial wall friction preload in the axial direction.

When the fiber bundle gets bent, resistance to bending internal forces will be produced as well. Depending on the shape of the material, the internal forces resisting deformation are different. The formula of the maximum bending stress of the fiber bundles is:

$$\sigma_{\max} = \frac{\mu_1 d N_1 l}{0.2 d_s^3} \tag{2}$$

The friction along the axial preload is f_3 , so its maximum deflection W_{\max} is:

$$W_{\max} = \frac{64 f_3 l^3}{3 \pi E d_s^4} \tag{3}$$

2.3. The Structural Parameters Analysis of the Flexible Blade

The material of the flexible blade is wear-resistant fiber. The flexible screw diameter is slightly longer than the spiral pipe's diameter. According to the principle of material mechanics [6–8], the flexible blade is bent and contacts the inner wall of the tube. With the fibers rotation, there is no material-gathering phenomenon occurring. The structural parameters of the flexible blade are shown in Figure 3.

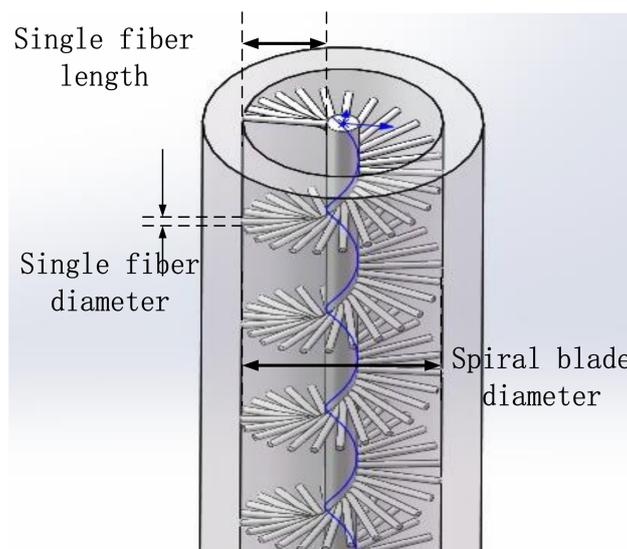


Figure 3. Flexible blade characteristics.

Based on Formula (1):

$$l = \frac{\pi d_s^2}{4} \sqrt{\frac{E \pi}{d N_1}} \tag{4}$$

d_s is from 0.5 mm to 2.5 mm. E is 3.2×10^9 N/m². $d N_1 = 100$ N, $1.5625 \text{ mm} \leq l \leq 39 \text{ mm}$, Stress must satisfy the condition that, less than the allowable stress $[\sigma]$, the material or institutions allowable stress is the national standard.

$$\sigma_{\max} \leq [\sigma] \tag{5}$$

Based on Formula (2), l is:

$$l \leq \frac{0.2d_s^3[\sigma]}{\mu_1 d N_1}$$

$[\sigma]$ of nylon 66 is 12 MPa, $d N_1 = 100$ N, the friction factor between plastic and plastic μ_k is 0.4, the calculation is

$$1.5 \text{ mm} \leq l \leq 187.5 \text{ mm}$$

The design should meet the stiffness conditions as follow:

$$\omega_{\max} = \frac{64f_3l^3}{3\pi E d_s^4} \leq [\omega] \tag{6}$$

The formula is:

$$l \leq \frac{1}{8} \sqrt[3]{\frac{3\pi E d_s^4 [\omega]}{f_3}} \tag{7}$$

With d_s from 0.5 mm to 2.5 mm, and $f_3 = 30$ N, the calculation is:

$$6.5 \text{ mm} \leq l \leq 38.75 \text{ mm}$$

2.4. The Flexible Blade Discrete Coefficient

As can be seen from Figure 4, the flexible spiral blade adopts a spiral form similar to that of the traditional spiral blade. This structure can make the material rising along the surface. When the gap between two fibers is too big, the flexible blade cannot meet the requirements of the conveying material blade. If the gap is small, the power consumption will be increased.

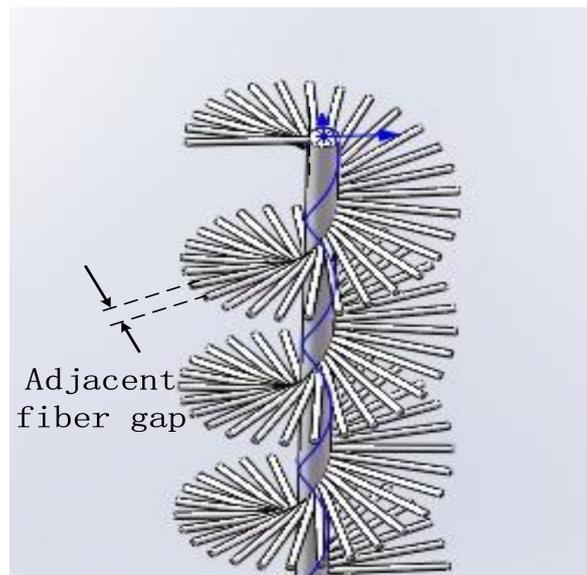


Figure 4. Flexible helix blade clearance diagram.

The discrete coefficient λ formula is:

$$\lambda = \frac{d_j}{d_i + d_j} \tag{8}$$

where d_i is the diameter of the nylon, and d_j is the average distance between two nylon fibers.

3. The Conveying Power Consumption Model

3.1. Single Particle Motion Analysis

We assume that the granular material is a continuous medium [9–12], and the particle size, shape and natures are the same. The material on the spiral vane motion analysis is shown in Figure 5.

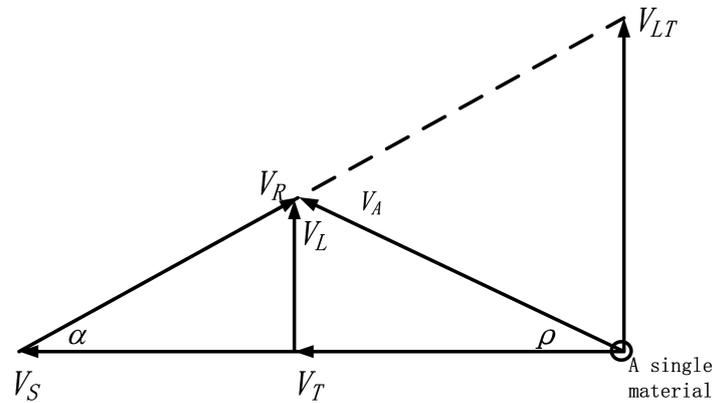


Figure 5. Diagram of the velocity of a single particle.

In Figure 5, V_s is the screw rotational speed, V_R is the relative speed of material along the spiral surface, V_A is the speed of the material, V_{LT} is the speed of the screw conveyor, V_T is the transport velocity.

The spiral angle of the blade is:

$$\alpha = \tan^{-1} \frac{P}{\pi D} \tag{9}$$

The tangential velocity V_S of the material is:

$$V_S = \omega R = \frac{2\pi n R}{60} = \frac{\pi n_z R}{30} \tag{10}$$

where R is the radius from the centerline of the screw axis to the wall, and n_z is the screw shaft speed. Therefore, the tangential velocity of the material increases with the acceleration of the rotation speed of the helical shaft and the increase of the helical radius. The relative speed of the material along the spiral surface V_R is:

$$V_R = \frac{V_S \sin \rho}{\sin(\alpha + \rho)} \tag{11}$$

The synthesis speed V_A is:

$$V_A = \frac{V_S \sin \alpha}{\sin(\alpha + \rho)} \tag{12}$$

Figure 5 shows the vertical speed of the materials that is:

$$V_L = \frac{\pi n_z R \sin \alpha \sin \rho}{30 \sin(\alpha + \rho)} \tag{13}$$

3.2. Power Consumption Calculation

The friction consumption of fibers is P_1 .

As shown in the Figure 6, the frictional force can be represented as:

$$df_1 = \tan \delta \rho_{(z)} h b g d l \cos \alpha \tag{14}$$

where $\rho_{(z)}$ is the density of the powder material, h is the thread height, b is the spiral groove width, dl is the length along the spiral element, and δ is the friction angle.

The corresponding torque infinitesimal dM_1 can be represented as:

$$dM_1 = \frac{1}{2}(D - d_z)\rho_{(z)}hbg \tan \delta \cos \alpha \lambda \frac{\pi D}{p} dz \tag{15}$$

where D is the diameter of the inner wall, and d_z is the screw shaft outer diameter.

By the formula $P = M\omega$, we have:

$$P_1 = M_1\omega = \omega \int_0^z \frac{(D - d_z)\rho_{(z)}hbg \tan \delta \cos \alpha \lambda \pi D}{2p} dz \tag{16}$$

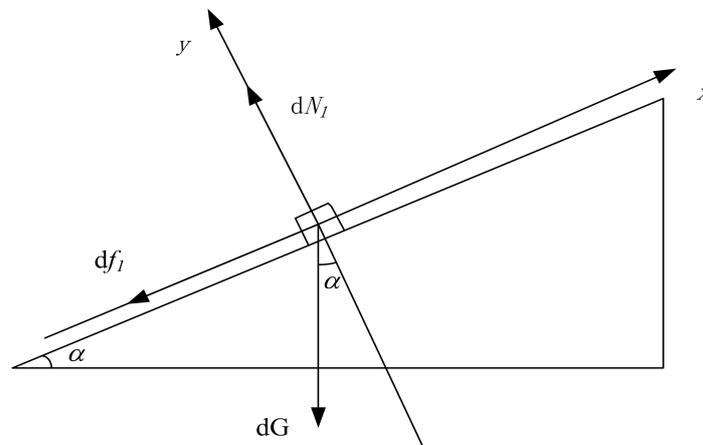


Figure 6. Diagram of the stress of the material along the spiral surface.

In Figure 7, the frictional force df_2 is:

$$df_2 = \tan \delta_1 \omega^2 \frac{D - d_z}{2} dm = \frac{\rho_{(z)}hb\omega^2(D - d_z)\pi D \tan \delta_1}{2p} dz \tag{17}$$

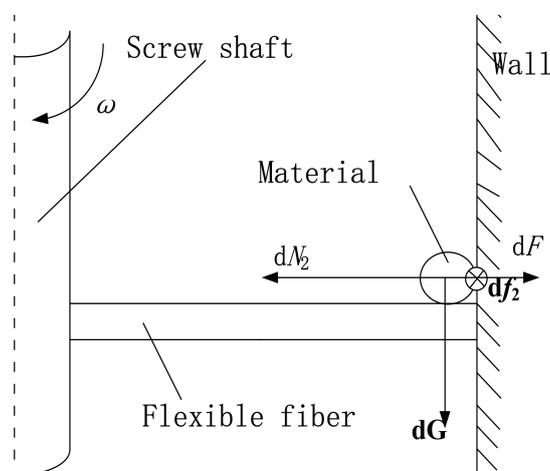


Figure 7. Vertical plane stress analysis.

The corresponding torque infinitesimal dM_2 can be represented as:

$$dM_2 = \frac{D - d_z}{2} df_2 = \frac{(D - d_z)^2 \rho(z) hb \omega^2 \pi D \tan \delta_1}{4p} dz$$

The consumption of the material due to the interaction with the spiral wall is P_2 .

By the formula $P = M\omega$, we have:

$$P_2 = M_2\omega = \frac{\omega(D - d_z)^2 hb \omega^2 \pi D \tan \delta_1}{4p} \int_0^z \rho(z) dz \tag{18}$$

Power is required to overcome the elastic deformation of the flexible helical fibers [13,14]. When the flexible screw rotates with the helical axis, the centrifugal force of single fiber will produce a force f_0 on tangent direction.

f_4 is the difference between dN_1 and f_0 . It is the elastic potential energy, as shown in Figure 8.

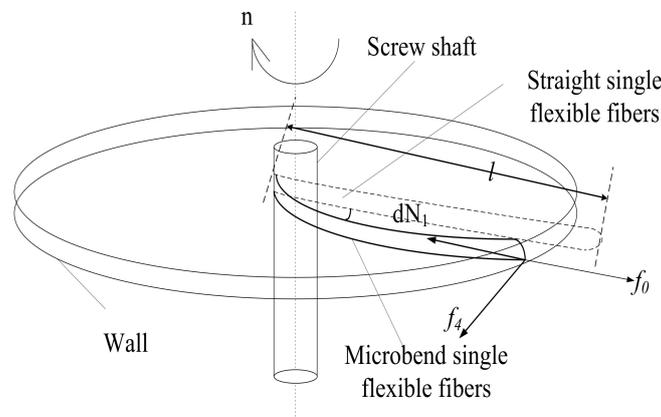


Figure 8. Stress analysis of the elastic deformation of the flexible spiral strand.

The centrifugal force f_0 and the friction force f_4 are:

$$f_0 = m\omega^2 l \tag{19}$$

$$f_4 = \mu m \omega^2 l + f_3 \tag{20}$$

where m is the quality of a single fiber, and ω is the rotating speed of the screw shaft.

We assumed the elastic potential energy of the fibers as the elastic potential energy of a spring:

$$E_p = \frac{1}{2} k \delta^2 \tag{21}$$

where δ is the deformation of the fiber bundle, and k is the spring stiffness which depends on the material itself:

$$\delta = \frac{f_4 l}{EA} \tag{22}$$

The total elastic energy of the nylon fiber is:

$$E_z = NE_p = \frac{1}{2} Nk \left[\frac{(\mu m \omega^2 l + \mu dN_1) l}{E \pi d_s^2} \right]^2 \tag{23}$$

We can obtain the total power consumption of elastic energy of the nylon fiber:

$$P_3 = \frac{E_Z}{t} = \frac{1}{2t} \text{Nk} \left[\frac{(\mu m \omega l^2 + \mu d N_1) l}{E \pi d_s^2} \right]^2 \tag{24}$$

where t is the working time.

To sum up, the total power consumption P is:

$$\begin{cases} P_1 = M_1 \omega = \omega \int_0^z \frac{(D-d_z) \rho(z) h b g \tan \delta \cos a \lambda \pi D}{2p} dz \\ P_2 = M_2 \omega = \frac{\omega (D-d_z)^2 h b \omega^2 \pi D \tan \delta_1}{4p} \int_0^z \rho(z) dz \\ P_3 = \frac{E_Z}{t} = \frac{1}{2t} \text{Nk} \left[\frac{(\mu m \omega l^2 + \mu d N_1) l}{E \pi d_s^2} \right]^2 \end{cases}$$

$$P = P_1 + P_2 + P_3 \tag{25}$$

4. Discrete Element Simulation

The Discrete Element Method (EDEM) software is used to simulate the process of a flexible screw conveyor transporting granular materials [15–18]. In the software, the flexible screw, tube wall, and granular material are built [19]. The material’s parameters [20–23] are shown in Table 1.

Table 1. Material properties.

Material	Poisson’s Ratio	Modulus of Elasticity (pa)	Density (kg/m ³)
Starch	0.25	2×10^7	1500
Nylon 66	0.28	3.2×10^9	1130
PVC	0.35	3×10^6	1400

The starch granules contact properties are shown in the Table 2, and the contact models in simulation are shown in Table 3.

Table 2. Starch granules’ contact properties.

Interaction	Coefficient of Restitution	Static Friction Coefficient	Rolling Friction Coefficient
Particle to particle	0.1	0.7	0.01
Particles to nylon	0.3	0.5	0.01
Particles to PVC tube	0.3	0.5	0.01

Table 3. Physical interaction model.

Interaction	Model
Particle to particle	Mertz–Mindin with bonding built-in
Particles to nylon	Mertz–Mindin (no slip) built-in
Particles to PVC tube	Mertz–Mindin (no slip) built-in

4.1. The Spiral Angle

Considering the limits of the manufacturing capacity, the spiral angles of the flexible screw conveyor is 20°, and the diameter of the spiral is 70 mm, which is the capability of the screw. Therefore, the maximum distance of each fiber is 1 mm, and the diameter of the spiral is 70 mm. The spiral shaft is 150 mm long, and the rotational speed is 400 rpm. The particle number is 10,000. We set three spiral angles of 10°, 20°, and 30° to simulate the process of the flexible screw working. Figure 9 shows the simulation results.

The low-speed material particles are colored in blue, and the high-speed particles are colored in red. It can be seen from Figure 9a that for most of the particles, the speed is from 100 mm/s to 480 mm/s. In Figure 9b, the speed of most particles is from 400 mm/s to 860 mm/s. In Figure 9c, the speed of most particles speed is from 800 mm/s to 1200 mm/s. The results show that the speed of the particles can be increased by the speed of the screw conveyer under certain other conditions. By collating the simulation data, the speed of the three experiments at the same transportation distance is shown in Figure 10.

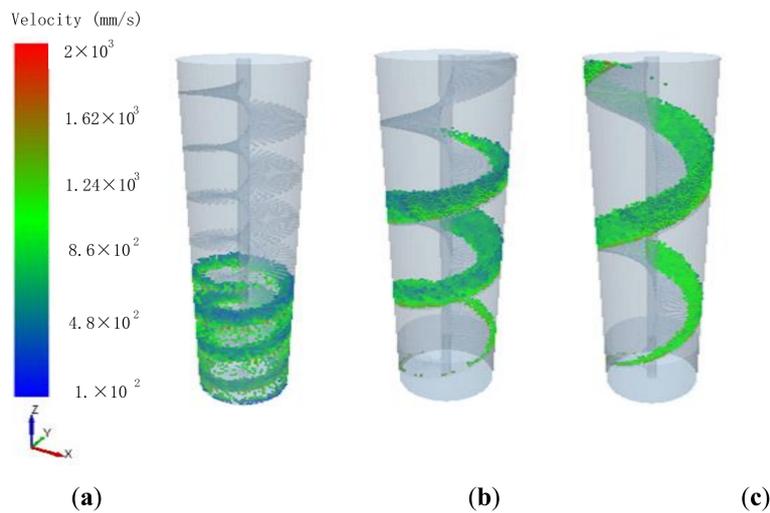


Figure 9. Different angles simulation results. (a) spiral angle 10°; (b) spiral angle 20°; (c) spiral angle 30°.

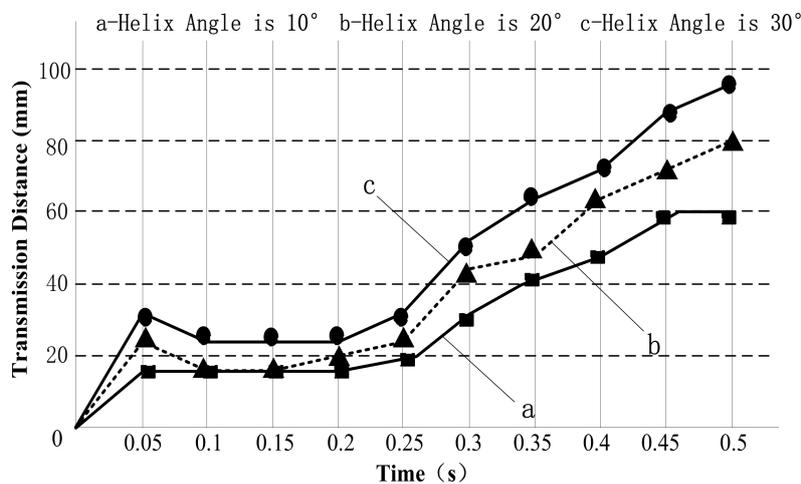


Figure 10. Transmission distance with different angles.

From Figure 10, it can be seen that increases of the spiral angle will improve the transportation efficiency of the granular material.

4.2. The Different Rotary Speed

The rotary speeds of the motor are 200 rpm, 600 rpm, and 800 rpm. We can see from Figure 11a that the rotary speeds of most particles are from 100 rpm to 2000 rpm. The particles rotate with the rotation of the helical axis, but the upward transport of the particles is not obvious. We can see from Figure 11b that the speed of most particles is between 100 rpm to 5000 rpm. The particles rotate with

the rotation of the helical axis, and the upward transport of the particles is obvious. The speed of the particles are from 1000 rpm to 8000 rpm in Figure 11c.

The data collected are shown in Figure 12. This shows that, under certain conditions, the transport of the particles increases with the increase of the speed of the screw conveyor.

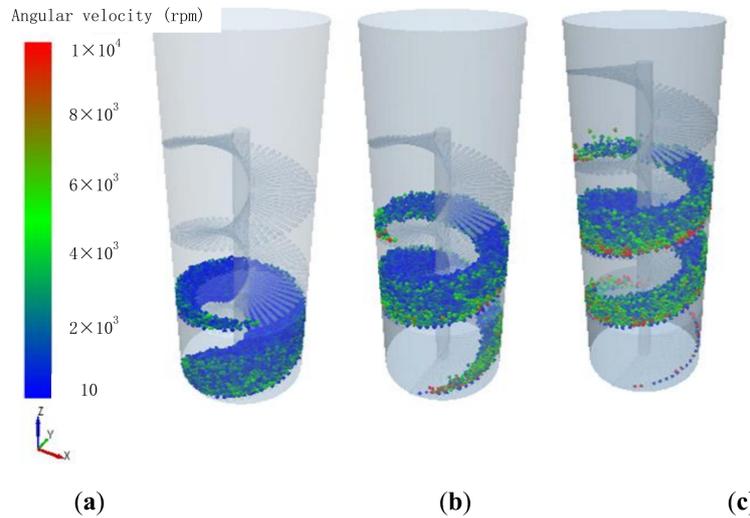


Figure 11. Different rotary speeds simulation. (a) Rotary speed 200 rpm; (b) rotary speed 600 rpm; (c) rotary speed 800 rpm.

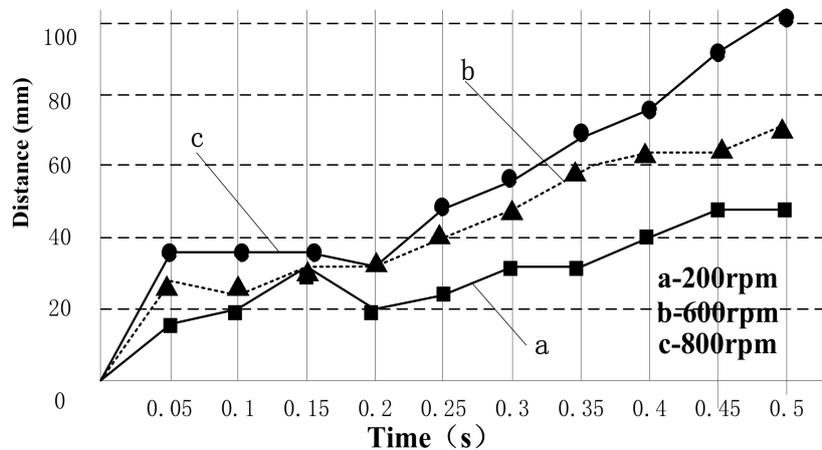


Figure 12. Particles speed with different rotary speeds.

5. Test and Results

5.1. Experiments

The experiments performed regard the sensor, rotary motor, tube and screw, data collection device, as can be seen from Figure 13a,b. The rotary speed range is from 100 rpm to 1000 rpm. Figure 14 shows the flexible blade screw conveyor, which is composed of tube, flexible blade, and axis. The conveyor is 2 m long, the diameter is 60 mm, and the screw angle is 20°. The transportation object is sand with homogeneous particle size.

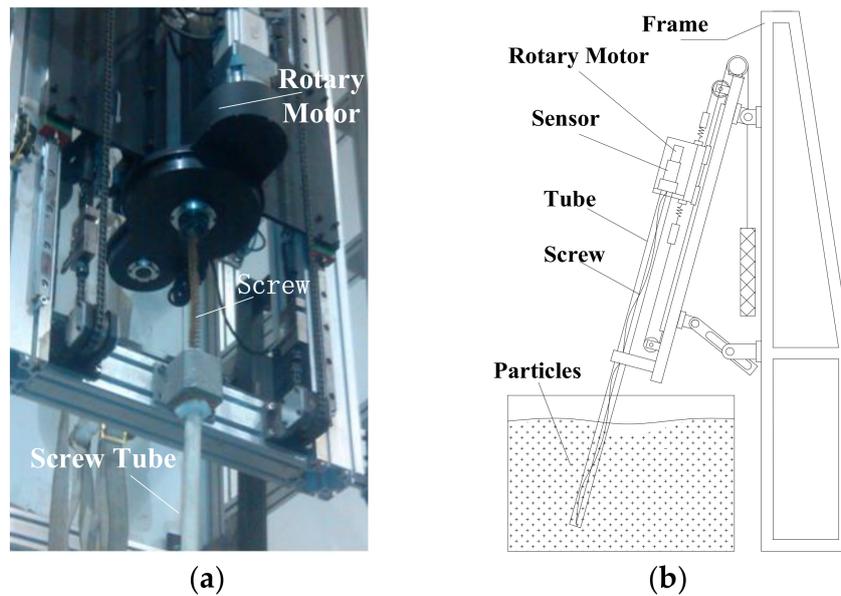


Figure 13. Test bed and parts. (a) Test bed. (b) Parts of test bed.

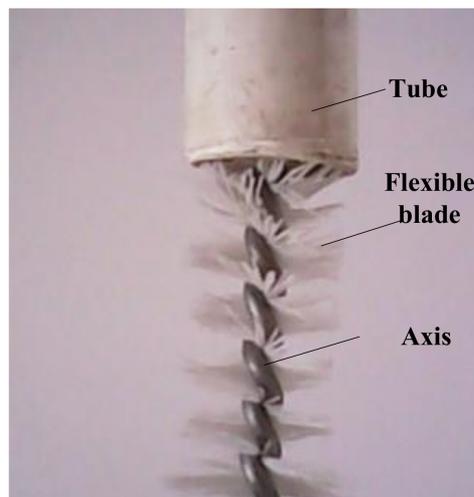


Figure 14. Flexible blade screw.

5.2. Results

In order to eliminate the adverse effects of No-load of the rotary motor, rotary torque curves without load were obtained from 100 rpm to 300 rpm. Figure 15 is a torque curve without load under 300 rpm. The other two torque curves are the same as in Figure 15. As we can see, the curve are similar to a horizontal straight line, and the value is 0.40×10^4 Nm.

As shown in the Figure 16, the three curves indicate the torque consumption under load. The data obtained with the Matlab software, are shown in Figure 17. The three lines represent test data, simulation data, and numerical solution when the rotary speed is 300 rpm. The numerical solution by the model is a limited data. Therefore, it is a horizontal line in Figure 17. In contrast, the test and simulation curves are obtained at the same time. It can be seen that the two curves raise with time, but the maximum values are lower than the numerical solution.

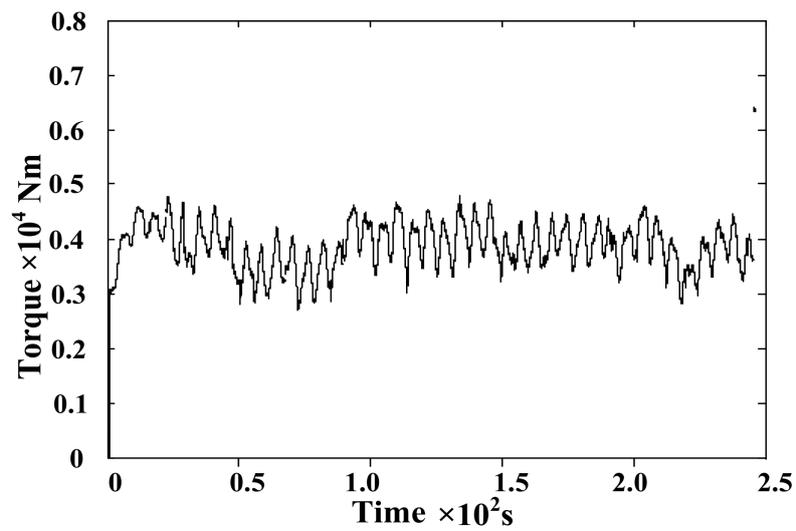


Figure 15. Torque without load.

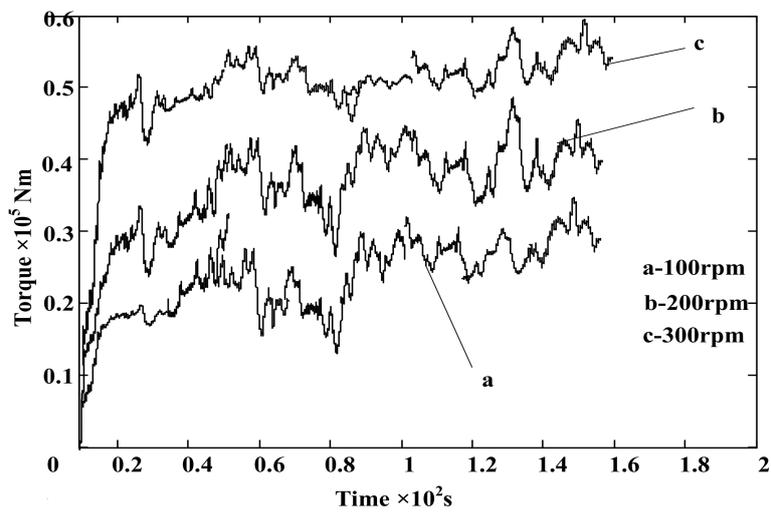


Figure 16. Torque of three rotary speeds.

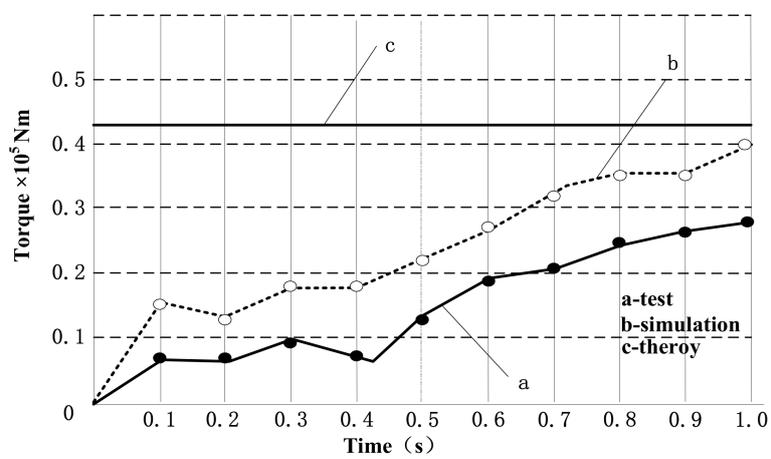


Figure 17. Contrast diagram.

6. Conclusions

The conclusions of this paper can be summarized as follows:

- (1) A flexible screw blade which is made of flexible fiber bundles is proposed as the spiral conveying shaft of screw conveyor for powder conveying. The ability to transmit particles whose diameter is bigger than that of the flexible fibers is verified by experiments.
- (2) According to the theory of particle mechanics and material mechanics, the power consumption and conveying quantity model of flexible screw blades for conveying bulk materials are established. The main parameters affecting the conveying amount and power consumption are: helical diameter, spiral rising angle, blade dispersion coefficient, and so on.
- (3) The mechanism of flexible spiral blade conveyor is verified by the particle material mechanics software EDEM. From the results of the simulation, we show that the conveying capacity of the particles decreases with the acceleration of the clearance of the flexible helical blades and increases with the speed, diameter, and angle of the screw conveyor; the power consumption of the particle material increases with the speed of the screw conveyor and the diameter of the spiral.
- (4) The theoretical and simulation results are verified by experiments. By comparing the power (torque) curves at the same speed, the growth trend of the experimental curves is consistent with the results of the theoretical analysis and simulation curves.

Author Contributions: Y.T. and J.G.; Methodology, M.C.; Software, P.Y.; experiment, Y.S. and T.D.; Data Analysis, F.Y. and J.T.; Validation, K.Z.; Writing-Original Draft Preparation, Q.C.; Editing paper format.

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Conflicts of Interest: The authors declare no conflict of interest.

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