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Rubber Dam Isolation and High-Volume Suction Reduce Ultrafine Dental Aerosol Particles: An Experiment in a Simulated Patient

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Featured Application: This work contains relevant data for advanced simulation analysis such as computational fluid dynamics (CFD) that help to understand and mitigate dental aerosol particles towards a safe clinical environment.

Abstract: The ongoing Coronavirus Disease 2019 (COVID-19) pandemic has triggered the paralysis of dental services ascribed to the potential spread of severe acute respiratory syndrome (SARS)-CoV-2. Aerosol-generating procedures (AGPs) are common in dentistry, which in turn increase the risk of infection of the dental personnel due to the salivary presence of SARS-CoV-2 in COVID-19 patients. The use of rubber dam isolation (RDI) and high-volume evacuators (HVE) during AGPs is recommended to control dental aerosols, but the evidence about their effectiveness is scarce. This first study aimed to compare, in a simulated patient, the effectiveness of the following strategies: standard suction (SS), RDI and RDI + HVE. Using the laser diffraction technique, the effect of each condition on the volume distribution, average size and concentration of coarse (PM₁₀), fine (PM_{2.5}) and ultrafine (PM_{0.1}) particles were evaluated. During the teeth drilling, the highest volume fraction of dental aerosol particles with SS was below 1 μ m of aerodynamic diameter. Additionally, the RDI + HVE significantly reduced both the ultrafine dental aerosol particles and the concentration of total particulate matter. AGPs represent a potential risk for airborne infections in dentistry. Taken together, these preliminary results suggest that isolation and high-volume suction are effective to reduce ultrafine dental aerosol particles.

Keywords: aerosol-generating procedures; airborne particulate matter; dental simulator; high-speed handpiece; ultrafine

1. Introduction

The ongoing Coronavirus Disease 2019 (COVID-19) pandemic has triggered several forms of collateral damage but one obvious effect is the paralysis of dental services caused by the potential spread of severe acute respiratory syndrome (SARS)-CoV-2 [1]. In dentistry, approaches such as preventive, restorative and surgical use water-cooled rotary devices (i.e., high-speed handpieces) to perform interventions that are considered aerosol-generating procedures (AGPs) [2–4]. Taking into account

that the SARS-CoV-2 viral load is high at saliva, nose and oropharyngeal secretions in COVID-19 patients [5,6], other patients and dental personnel are considered at high risk for cross-infection spreading [7]. Recommendations have been released oriented to reopen dental practice and mitigate the risk of AGPs [3,4,8,9] that include the use of rubber dam isolation (RDI) and high-volume evacuators (HVE) for dental procedures [3,7,10–12]. However, there is a lack of evidence that supports the effectiveness of RDI and HVE, either alone or combined, to control dental aerosols during dental restorative procedures [4,13–15].

Dental aerosols contain potentially hazardous particulate matter of submicron size. Restorative dental procedures such as tooth grinding produce particulate matter (PM) that exhibit a high proportion of particles with an aerodynamic diameter smaller than 10 μm (PM₁₀) [16,17]. Aerosolized particles, based on the size below each name, are defined as coarse (PM₁₀) and fine (PM_{2.5}) particles [18]. After reaching the lower respiratory airways, the PM_{2.5} are associated with systemic inflammation and increased respiratory mortality risk [19-21]. A significant correlation was found between new COVID-19 cases and the average amount of outdoor coarse particles in cities from China and Italy [22,23]. Viral RNA was detected in samples taken after coughing in influenza positives from particles with an aerodynamic diameter smaller than one micron (PM₁), which correspond to a fraction of the PM_{2.5}, [24]. In a similar fashion, the SARS-CoV-2 RNA was also detected in PM_{2.5} from aerosol-coated areas of two hospitals from Wuhan [25]. Ultrafine particles $(PM_{0.1})$, another fraction of $PM_{2.5}$, also known as nanoparticles, are also associated with health risks, including also systemic inflammation and cancer [26]. However, there is a lack of published evidence regarding the control of fine and ultrafine particles using mitigation strategies in dentistry. Inasmuch as PM includes fine and ultrafine particles that are associated with AGPs in dental settings, it is relevant to understand its behaviour and determine the potential risk of airborne infections during dental practice [7,16,27]. In this first study, the authors test the effectiveness of two mitigation strategies, the RDI and the HVE, and their effectiveness on coarse (PM₁₀), fine (PM_{2.5}) and ultrafine (PM_{0.1}) dental aerosol particles distribution during a full-crown preparation of anterior teeth (teeth grinding), under controlled conditions in a simulated patient.

2. Materials and Methods

2.1. Dental Simulated Patient

A dental operating room (DOR), at the School of Dentistry of the Universidad del Valle, was used to perform all the experiments. This DOR consisted in a closed space without windows, equipped with a centralized air-conditioning system and with the following dimensions: 2.4 m high, 3 m width and 3 m large. A dental unit chair with both standard suction (SS) and HVE systems was adapted with a NISSIM Type 1 Dental simulator (NISSIN Dental Products Inc., Kyoto, Japan) (Figure A1) with magnetic attachable full dentate maxillary and mandibular models (NISSIN Dental Products Inc., Kyoto, Japan) to simulate a patient. The mannequin's mouth was fitted internally with latex to simulate the volume of a human oral cavity and the width of the mouth's opening was established and standardized using bilateral dental bite blockers at the second molar level. The average environmental conditions of the DOR were 22 °C and relative humidity of 65% during experiments.

2.2. Particulate Matter Detection and Quantitation

To detect and quantitate the dental fine ($PM_{2.5}$), the ultrafine ($PM_{0.1}$), as well as the coarse (PM_{10}), particles produced during the previously described dental procedure, a laser diffraction technique was implemented, using a specialized device for aerosol testing in a wet environment. The laser device Insitec S (Malvern Panalytical Ltd., Malvern, UK) was in a fixed position, which allowed the detection of dental particles at 11 cm from the mannequin's upper central incisors (Figure 1a,b). The measurement rate of the particle sizes was 5 per second and the detection size range of the device was 0.1 μ m to 1000 μ m. The RTSizer 7.4 (Malvern Panalytical Ltd., Malvern, UK) was used to analyse the signals

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generated from the detection of coarse, fine and ultrafine particles during vestibular and palatal preparation of the tooth for a full crown restoration. The retrieved variables aimed to describe the particle-size distribution of interest (between 0.1 μ m and 10 μ m) which included the volume fraction by range of particle sizes. In addition, the 10th, 50th and 90th percentiles of the particle diameter that corresponds to the cumulative undersize distribution by volume for the total particulate matter were calculated (Dv₁₀, Dv₅₀ and Dv₉₀, respectively) (ISO Standard N° 13320:2020). Also, the concentration in mg/m³ for the total particles was measured. In addition, the average size of the dental aerosolized particles below 10 μ m, the Sauter mean diameter (d_{3,2}), was determined.

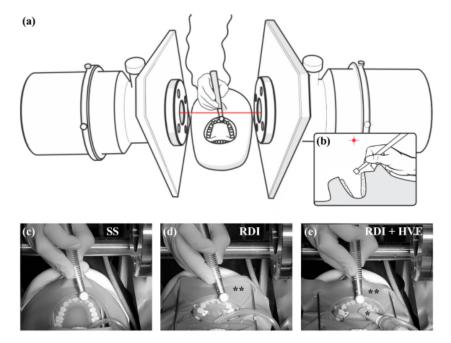


Figure 1. Experimental design using simulated patient and laser diffraction for particle quantitation. (a) Description of the spatial relationship between the mannequin's mouth and laser ray, demonstrating the location of the laser beam of the measurement device (Insitec S; Malvern Panalytical Ltd., Malvern, UK). (b) Scheme sagittal view showing the location of the laser beam (red dot with red cross) from the anterior teeth, at a linear distance of 11 cm. (c–e) Screenshots from the recorder experiments showing the three conditions: (c) standard suction (SS) with a saliva ejector; (d) rubber dam isolation plus standard suction (RDI); (e) rubber dam isolation plus high-volume suction (RDI + HVE) using both the standard suction (saliva ejector) and the high-volume evacuator (straight tip). *: High-volume evacuator's tip; **: Rubber dam.

2.3. Dental Isolation and Suction Techniques

In this first study, the experiments were set up for three different groups (Figure 1c–e). The first group was set up as standard suction (SS), using only a standard saliva ejector (Figure 1c). The second group was set up using rubber dam isolation plus standard suction (RDI) (Figure 1d). The third group included the previously described RDI plus a high-volume evacuator finished in a rigid plastic tip of 12 cm long and 0.8 cm of diameter (RDI + HVE) (Figure 1e). For the second and the third groups, the rubber dam isolation was performed using a standardized technique with the perforation guide provided by the manufacturer (Sanctuary Dental Dam Systems©, Perak, Malaysia) and a metallic frame young's arch. In order to obtain a standardized tension of the rubber dam during the whole experiments, the anterior maxillary and mandibular teeth were isolated up to the first bicuspids, secured with rubber dam clamps (RDCM1 for upper bicuspids and RDCM2 for lower bicuspids; Hu-Friedy Mfg. Co., Chicago, IL, USA), and maintaining the standard saliva ejector over the rubber dam. The HVE system was manually stabilized by the dental assistant (M.d.M.D.-P.) at 15 mm from the

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palatal side of the tooth of interest (Figure A2). Each experiment was video recorded in high-resolution from a static diagonal front position at 90 cm from the mouth of the mannequin.

2.4. Dental Restorative Procedures

To simulate grinding dental procedures, a standardized protocol of anterior teeth full-crown preparation was performed by an experienced prosthodontist clinician (D.G.). The sequence for full-crown preparation started with the vestibular side, followed by interproximal sides (mesial first, then distal), palatal side, and finished with the incisal part, for a complete anterior tooth preparation that lasted 6 min (standardized total time for full crown preparation in each experiment). An EXTRAtorque 605C high-speed handpiece (with press button, Borden 2-hole connection, triple spray and rotation between 280,000–380,000 rpm) (KaVo Dental, Charlotte, NC, USA) with current water coolant to prepare acrylic teeth were used (NISSIN Dental Products Inc., Kyoto, Japan). The protocol was performed with a diamond coated (medium size grain between 64–126 μ m) tapered chamfer dental burr with round end (reference 852, 016) for universal teeth grinding procedures (Hager and Meisinger GmbH, Neuss, Germany). The dental burr was replaced for a new one for the different settings and upper central incisors were replaced for each experiment.

2.5. Statistical Analysis

The experiments for each condition were performed in triplicate. Results are shown as mean \pm standard error of the mean (SEM). For the statistical analysis, a comparison of the quantitative variables between each RDI condition and the SS set up, and between sides (vestibular versus palatal), was performed using the Mann–Whitney test for non-normally distributed data. A logarithmic scale (log10) between 0.1 μm and 10 μm was implemented to plot the curve of particle-size distribution (based on the volume fraction) for each condition. The software GraphPad Prism version 8.4.3 for Windows (GraphPad Software, San Diego, CA, USA, www.graphpad.com) was used to perform the statistical analysis and to plot the graphs. A significance level of 0.05 was established for differences among the described variables.

3. Results

3.1. Ultrafine Dental Aerosol Particles Are Generated during Full-Crown Teeth Preparation

To determine the behaviour of AGP in each simulated condition (SS, standard suction; RDI, rubber dam isolation; RDI + HVE, rubber dam isolation plus high-volume evacuator), a volume frequency distribution in the range 0.1–10 μ m was generated for both vestibular and palatal sides (Figure 2a,b, respectively). Using only standard suction, the curve showed a displacement to the left, in the range below 1 μ m in size, in both vestibular and palatal sides (Figure 2a,b). In contrast, in the RDI group, the curve was displaced to the middle and to the right, in the range between 1–10 μ m, for both sides. For the RDI + HVE group, the location of HVE in the palatal side was consistent with less particle generation whereas in the vestibular side the curve exhibited two peaks: below 1 μ m and over 7 μ m (Figure 2a,b). During full-crown preparation, in the SS group, no PM_{2.5} was detected in the vestibular side or in the palatal side, and no significant difference was found in the vestibular side between PM_{0.1} and PM₁₀ (Table 1). In contrast, there was a significant difference between PM_{0.1} and PM₁₀ in the palatal side for the SS group (p < 0.05). Only one of three experiments detected a small percentage of fine particles (PM_{2.5}) in both vestibular and palatal sides of the RDI group (Figure 2a,b, Table 1). No significant difference was found in the volume fraction for PM_{0.1}, PM_{2.5} and PM₁₀ between vestibular and palatal sides (p > 0.05).

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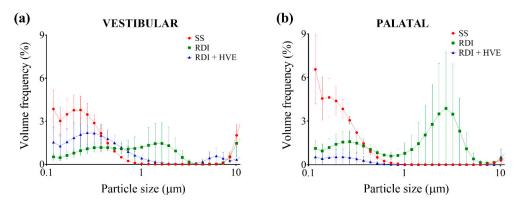


Figure 2. Curve distribution of volume fraction of the dental aerosolized particles under 10 μm. (a) The vestibular side shows an increased volume fraction for particles below 0.1 μm for the SS group, when compared to the RDI and RDI + HVE groups. (b) In the palatal side, the volume fraction distribution follows a similar pattern seen in (a), except for the RDI + HVE group. Results are shown as mean \pm standard error of the mean (SEM); n = 3. Abbreviations: SS, standard suction; RDI, rubber dam isolation; HVE, high-volume evacuator. X axis (Particle size) is Log₁₀ scaled.

Table 1. Volume fraction of ultrafine $(PM_{0.1})$, fine $(PM_{2.5})$, and coarse (PM_{10}) dental aerosol particles.

Side	Particulate Matter Size	Volume Fraction (%) by Group		
		SS	RDI	RDI + HVE
Vestibular	PM _{0.1} PM _{2.5} PM ₁₀	3.85 ± 1.33 0.00 ± 0.00 2.02 ± 0.77	$[0.52 \pm 0.25]$ * 0.93 ± 0.93 1.45 ± 0.92	1.54 ± 1.06 0.03 ± 0.01 $[0.33 \pm 0.04] *$
Palatal	PM _{0.1} PM _{2.5} PM ₁₀	6.56 ± 2.37 0.00 ± 0.00 0.29 ± 0.29	$[1.11 \pm 0.56]$ * 3.49 ± 3.49 0.37 ± 0.25	$[0.53 \pm 0.53] *$ 0.00 ± 0.00 0.53 ± 0.53

Comparison between groups shows a significant production of ultrafine particles during full-crown anterior teeth preparation. RDI and RDI + HVE strategies reduce these ultrafine particles in both vestibular side and palatal side. No difference was found for any parameter between vestibular side and palatal side. Results are shown as Mean \pm SEM; n = 3. The brackets and the asterisk (*) mean statistical difference when compared RDI and RDI + HVE to the SS group (p < 0.05). Abbreviations: PM, particulate matter; SS, standard suction; RDI, rubber dam isolation; HVE, high-volume evacuator.

3.2. Rubber Dam Isolation and High-Volume Suction Reduce the Volume Fraction of Ultrafine Dental Aerosol Particles

To determine the effectiveness of mitigation strategies to reduce dental aerosol particles, a comparison among SS, RDI and RDI + HVE groups was performed. In comparison to the SS group, a significant reduction of the ultrafine particles ($PM_{0.1}$) was found when the RDI was implemented (p < 0.05) but not for the use of RDI + HVE in the vestibular side (Figure 2a, Table 1). In the same side, a significant reduction of the coarse particles (PM_{10}) was achieved with the use of both rubber dam isolation and high-volume suction (p < 0.05) when compared to the SS group (Figure 2a, Table 1). On the other hand, in the palatal side, the ultrafine particles ($PM_{0.1}$) were significantly reduced with the use of RDI alone or combined with HVE (RDI and RDI + HVE groups) (p < 0.05) (Figure 2b, Table 1).

3.3. Rubber Dam Isolation and High-Volume Suction Reduce the Concentration of Dental Aerosol Particles

To determine the percentile distribution of dental aerosolized particles generated during the full-crown anterior teeth preparation, Dv_{10} , Dv_{50} and Dv_{90} were calculated. After comparison, Dv_{10} , Dv_{50} and Dv_{90} of the SS group were significantly lower (p < 0.05) than the RDI group in both vestibular side and palatal side (Figure 3a,b). Dv_{10} and Dv_{90} of the RDI group was significantly higher than the RDI + HVE group in the palatal side (p < 0.05) (Figure 3b). In addition, Dv_{50} and Dv_{90} of the SS group were significantly lower than RDI + HVE group in the vestibular side (p < 0.05) but no differences were found in the palatal side (Figure 3a,b).

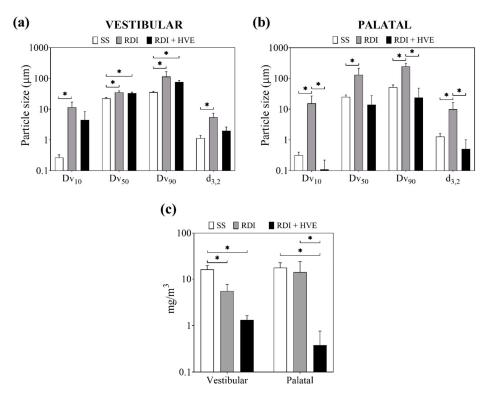


Figure 3. Rubber dam isolation and high-volume suction reduce dental aerosol particles. The distribution by volume (Dv) parameters for percentiles 10, 50 and 90 are shown for the vestibular side in plot (a) and the palatal side in plot (b). For these three percentiles, there is an increase in the average size of the particles based on the volume percent when the RDI is implemented. A significant increase in the $d_{3,2}$ (the average size of particles below 10 µm) is observed with the use of the RDI, but no effect is detected in the RDI + HVE group, when compared with the SS group. (c) The RDI and the RDI + HVE strategies reduce the concentration of aerosol-generating procedures (AGPs) in the vestibular side when compared with the SS group. In contrast, the RDI + HVE reduce this parameter when compared with both the SS group and the RDI group, in the palatal side. Results are shown as mean \pm SEM; n = 3; *: p < 0.05. Abbreviations: SS, standard suction; RDI, rubber dam isolation; HVE, high-volume evacuator. The Y axis of (a), (b) and (c) is Log₁₀ scaled.

To determine the effect of the mitigation strategies on the average size of the particles below 10 μ m for each condition, the Sauter mean diameter (d_{3,2}) was determined. For the SS group, the d_{3,2} was significantly lower than the RDI group in both vestibular side and palatal side (p < 0.05) whereas the d_{3,2} of the RDI group was significantly higher than the RDI + HVE group in the palatal side (Figure 3a,b). For the Dv parameters, no difference was found between vestibular side and palatal side in each group.

Both mitigation strategies, RDI and RDI + HVE, significantly reduced the concentration of aerosol particles in the vestibular side, when compared with the SS group (p < 0.05) (Figure 3c). In the palatal side, however, only the RDI + HVE showed effectiveness at reducing dental aerosol particles, compared to the SS and the RDI groups (p < 0.05) (Figure 3c). No difference was found between vestibular side and palatal side for any group.

4. Discussion

Our study demonstrates that the location of the tip of the high-volume evacuator, facing the aerosol-generating procedure side, and combined with rubber dam isolation, significantly reduce the volume fraction of the ultrafine particles ($PM_{0.1}$ or nanoparticles). In addition, the total concentration of aerosol particles produced during the drilling of resin-made teeth under controlled conditions was also significantly reduced in both vestibular and palatal sides using RDI + HVE. The ultrafine particles

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here detected corresponded to the highest proportion among aerosol dental particles in the hazardous range (aerodynamic diameter below $10~\mu m$) [21,26,28] when standard suction is implemented. Also, the use of rubber dam isolation combined with standard suction (RDI group) increased the average size of the dental aerosol particles, when compared with standard suction alone (SS). Moreover, the rubber dam isolation combined with high-volume suction effectively reduced the volume fraction of ultrafine particles in both vestibular side and palatal side. However, a significant reduction of total dental aerosol particles was only obtained in the palatal side using RDI + HVE when compared with SS and RDI conditions. This result suggests that the location of the high-volume evacuator based on the drilling side should be considered in aerosol mitigation strategies.

Simulation training is an effective method to test under safe conditions the response and the performance of health care personnel during AGPs in highly infectious disease context [29]. This dental simulator unit is a fast-response strategy to study AGPs in a dental office under controlled and patient-free conditions. Although this experimental setting is accurate for the study, it cannot replace real crown preparations, plus the use of artificial teeth for gridding might be different to that with natural teeth. Other clear limitation is the equipment use which require to be fixed, secure, and close to the mouth for proper measurement. In this context, the laser beam is not flexible due to the limited spatial range for aerosol quantitation. Therefore, this result should be used for comparisons with experiments carried out under similar controlled conditions, considering limitations such as the lack of microbial biofilms that bind to natural teeth, caries, oral and periodontal mucosa, quantity and quality of saliva and blood presence (which may affect the particle size of the dental aerosol particles) and other physiological confounding factors that may affect the behaviour of AGPs such as breathing and previous oral hygiene or previous rinse use within a real patient [30–32].

This study demonstrated that AGPs after teeth drilling are polydisperse by using a laser diffraction technique, with the highest proportion of ultrafine particles ($PM_{0.1}$) in the hazardous particle size range (PM_{10}). Interestingly, the particle fraction between $PM_{0.3-0.5}$ correlated with tooth drilling procedures in a real dental operating room, with no contribution of the particulate matter over 1 μ m [17]. This is consistent with our findings, in which aerosol particles were poorly or not detected over 1 μ m during artificial teeth drilling using standard suction in both vestibular and palatal sides. Nevertheless, the relative humidity was reported 40% [17], in contrast with our settings (average relative humidity: 65%). With a higher relative humidity (70%), another study reported similar findings regarding the increase of ultrafine particles during teeth drilling and grinding [33].

From the biomaterial point of view, we suggest that artificial teeth are a useful tool to reproduce dental tissues. Similarly, an experimental study that drilled and grinded natural teeth detected the highest proportion of dental aerosol particles in the PM_1 fraction, with no significant effect of the vacuum system on the ultrafine particles concentration [16]. The opposite effect was found in our study using high-volume suction, with a significant reduction of the volume fraction of the ultrafine particles in the palatal side (the same side where the tip of the volume evacuator was located). In contrast, this significant reduction in the RDI + HVE group was not observed in the vestibular side (Table 1). This can be explained by the fact that the tip of the high-volume evacuator was not able to suction properly these ultrafine particles, in part because of its location (palatal side) and due to the physical barrier of the tooth.

Currently RDI is highly recommended, even during restorative procedures to reduce infection risk [3,4]. When measured at one and two meters from the patient's mouth, the number of colony-forming units (CFUs) is reduced in two trials during restorative procedures with high-speed handpiece and RDI in children [34,35]. In contrast, when CFUs were measured in several points of the clinician's head, these were significantly increased when using rubber dam isolation versus control during restorative procedures in adults [14]. Aerosol particle sizes were not reported in these studies. In our study, the Dv_{10} , Dv_{50} , Dv_{90} and the $d_{3,2}$ of RDI group were significantly increased when compared with no rubber dam isolation (SS group) in both vestibular side and palatal side. This result may be explained by the fact that the study that took CFU measurements closer to the mouth of the patient [14] found an

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increase in this parameter, since larger particles may reach closer surfaces (e.g., clinician's head) but failed to reach longer distances (i.e., one to two meters from the patient's mouth).

Because of the lack of previous published studies on the methods implemented here, we were not able to perform a sample size calculation. However, the first results reported here are the basis for the experimental design, including statistical analysis and sample size calculation, of further and larger studies. Therefore, a triplicate experiment per condition was implemented in order to determine the feasibility of the experimental settings when analysing dental aerosol particles using laser diffraction. Taken together, our preliminary results support the effectiveness of the rubber dam isolation combined with high-volume suction to reduce the dental aerosol particles, although not always significantly and not for all particle sizes. Interestingly, the use of rubber dam isolation (with no HVE) reduces the ultrafine particles but increase the $Dv_{10-50-90}$ and the $d_{3,2}$ of total aerosol particles, which may increase their precipitation rate but also the surface of contamination in areas close to the patient's mouth. Further studies regarding the potential of infection of dental aerosol particles in the submicron range (under PM_{10}) are necessary. RDI is not possible for some procedures like dental surgery or dental hygiene. The results here reported represent a promising tool not only for the control of dental aerosol but also to understand the behaviour of airborne nanoparticles and mitigation strategies [36].

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Conflicts of Interest: The authors declare no conflict of interest.

Appendix A

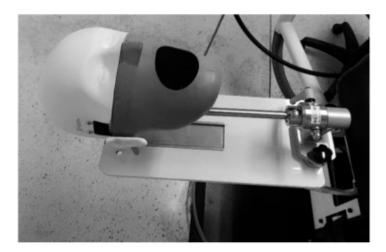


Figure A1. NISSIM Type 1 Dental simulator (NISSIN Dental Products Inc., Kyoto, Japan) attached to a dental unit chair with both standard suction and high-volume suction systems [these elements are not shown in the figure].

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Figure A2. The experimental setting with the clinician in the left side of the image, the measurement device, Insitec S (Malvern Panalytical Ltd., Malvern, UK) in the middle, the dental assistant holding the high-volume evacuator in the right and the real-time analytical computer equipment in the background.

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