

## Article

# Thin-Walled Commercially Pure Titanium Structures: Laser Powder Bed Fusion Process Parameter Optimization

Fatma Nur Depboylu <sup>1</sup>, Evren Yasa <sup>2,\*</sup>, Ozgur Poyraz <sup>3</sup> and Feza Korkusuz <sup>4</sup> 

<sup>1</sup> Department of Bioengineering, Institute of Science and Technology, Hacettepe University, Ankara 06800, Turkey

<sup>2</sup> Department of Mechanical Engineering, Eskişehir Osmangazi University, Eskişehir 26480, Turkey

<sup>3</sup> Department of Mechanical Engineering, Eskişehir Technical University, Eskişehir 26555, Turkey

<sup>4</sup> Faculty of Medicine, Department of Sports Medicine, Hacettepe University, Ankara 06100, Turkey

\* Correspondence: eyasa@ogu.edu.tr

**Abstract:** Laser powder bed fusion (L-PBF) process parameters can be changeable depending on the part geometry due to thermal conductivity differences. The number of studies on the process parameter development for commercial pure titanium (Cp-Ti) with the L-PBF process is also quite limited in the literature. The aim of this study is to present a comprehensive process development for the production of Cp-Ti bulk and thin structures with the L-PBF technology. In the first phase, the right process parameters, including scan speed, laser power, hatch distance, and layer thickness, were identified with prismatic specimens with thin walls so that the obtained parameters could be used for both bulky sections and thin features such as lattice structures. The process parameters were varied to change the volumetric energy density from 19 to 208 J/mm<sup>3</sup> among 80 different parameter sets. Parameter sets having a Volumetric Energy Density (VED) value between 32 J/mm<sup>3</sup> and 47 J/mm<sup>3</sup> gave almost fully dense Cp-Ti parts while the laser power was set to 200–250 W and the scan speed was used as 1000–1400 mm/s. Finally, Vickers hardness and tensile tests were applied to highly dense Cp-Ti parts. This study involving investigating the effect of process parameters on a wide range demonstrated that L-PBF is a favorable manufacturing technology for Cp-Ti parts with almost full density and good mechanical properties as well as good dimensional accuracy even on thin geometries. Moreover, the results show that combining parameters into a single one, i.e., VED, is not a proper way to optimize the process parameters since increasing laser power or decreasing the scan speed may alter the results, although VED is increased in both manners.

**Keywords:** Laser powder bed fusion (L-PBF); commercial pure titanium (Cp-Ti); process parameter optimization; volumetric energy density (VED); mechanical testing



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## 1. Introduction

The inherent principle of additive manufacturing (AM) is based on the creation of 3D parts from layers [1–3]. AM offers several advantages, such as almost unlimited design freedom, waste reduction, and reduced lead time from design to testing, which are compelling even for very demanding industries, including aerospace and biomedical [4,5]. Laser powder bed fusion (L-PBF) offers the highest technological maturity level as well as the widest industrial use for metallic materials among the AM techniques. Moreover, it is suitable for a very wide range of materials, including steels, aluminum alloys, copper alloys, nickel superalloys, and titanium alloys, as well as precious metals. Among these alloys, titanium alloys have an important place in various applications due to their strength-to-density ratios and corrosion/oxidation resistance provided by the passivation layer formed at their surface when exposed to air [6].

Commercially pure titanium is called Cp-Ti, with 99% Ti content. Cp-Ti shows lower mechanical strength in comparison to its alloys since it has a single phase ( $\alpha$ ) compared to

the  $\alpha + \beta$  phase encountered in Ti6Al4V [7]. Cp-Ti, however, has superior ductility with the greater elongation of Cp-Ti (15–24%) compared to Ti6Al4V (6–10%) [8]. Ti6Al4V is the most used titanium alloy studied extensively with L-PBF [9]. On the other hand, the number of studies on the process parameter development for Cp-Ti with the L-PBF process is quite limited in the literature (see Table 1).

**Table 1.** Previous L-PBF process parameter optimization studies for Cp-Ti and their density results.

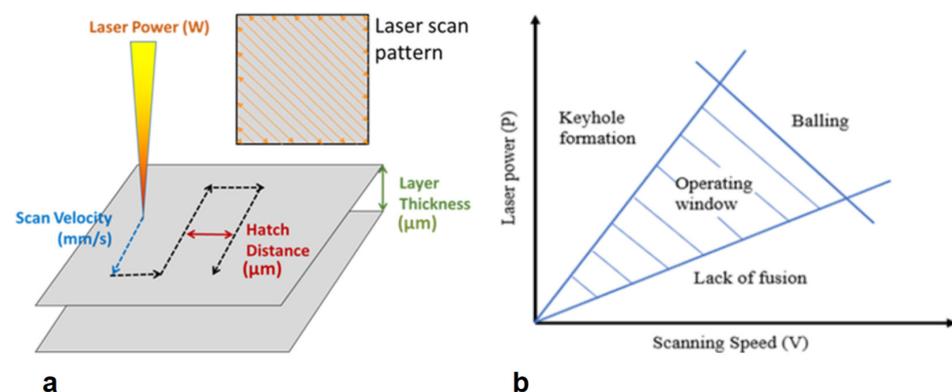
Ref.	Material	Laser Spot Size ( $\mu\text{m}$ )	Laser Power (W)	Layer Thick. ( $\mu\text{m}$ )	Scanning Speed (mm/s)	Hatch Distance ( $\mu\text{m}$ )	VED ( $\text{J}/\text{mm}^3$ )	Density
[10]	Cp-Ti (Grade 1)	64	122	30	400	120	85	Almost Full
[11]	Cp-Ti	-	50	25	333	80	75	98.7%
[12]	Cp-Ti (Grade 1)	50	50- 250	30	-	-	-	Over 99%
[8]	Cp-Ti (Grade 1)	-	100	30	385	120	72	Almost Full
[13]	Cp-Ti (Grade 1)	120	120- 440	30	1000	120	33–122	Almost Full
[14]	Cp-Ti (Grade 2)	80	165	100	138	100	120	99.5%
[15]	Cp-Ti (Grade 2)	70	90	50	100–400	-	90	99.5%
[16]	Cp-Ti	-	210	30	1000	120	58	99.5%
[17]	Cp-Ti (Grade 1)	60–70	250–340	50	700–800	100–120	52–97	98.2%

Hundreds of process parameters are defined in the L-PBF process, and moreover, the interactions of some parameters have a significant impact on part performance in terms of microstructural, dimensional, and mechanical properties. Among several parameters, laser power ( $P$ ), scan speed ( $v$ ), layer thickness ( $t$ ), and scan spacing, also known as hatch distance, ( $s$ ) are the most effective parameters (see Figure 1a) playing a significant role on the energy density [18]. By formulating these main parameters, penetrated energy level to the molten pool is calculated by Volumetric Energy Density (VED), Surface Energy Density (SED), and Linear Energy Density (LED), as shown in Equations (1)–(3), respectively. It is important to note that, although it is practical to combine all these critical parameters into one using volumetric energy density, the change in porosity, as well as other material properties, cannot be solely explained based on VED since the effect of individual parameters may be different at constant energy density values [19].

$$VED = \frac{P}{v \cdot t \cdot s}, \quad (1)$$

$$SED = \frac{P}{v \cdot t}, \quad (2)$$

$$LED = \frac{P}{v}, \quad (3)$$



**Figure 1.** (a) The most effective L-PBF process parameters. Reprinted with permission from Oliveira et al. [20]; [Mater. Des]; [Elsevier]; [2020]. (b) Specified porosity regions at laser power-scan speed graph. Reprinted with permission from Ahmed et al. [21]; [J. Manuf.Process]; [Elsevier]; [2022].

As Figure 1b shows, the process window for the LPBF process is generally found as a triangle leading to maximum density eliminating keyhole porosity and lack of fusion. Generally, the keyhole porosity occurs as a result of increasing the VED value, while a lack of fusion porosity can form due to inadequate VED. The keyhole porosity shows a smaller and more spherical geometry, while the lack of fusion is generally identified as irregular and bigger pores.

Although most process parameter studies mainly focus on cubic or prismatic geometries, it is usually not possible to make very thin features with the same parameters since dimensional accuracy is not taken as one of the objectives. However, Mohr et al. [22] reported that the process parameters depend on the part geometry because of thermal conductivity differences. Bulk geometries provide higher heat transfer from the top of the part to the base plate due to higher sectional area compared to thin structures. Thin walls increase the distance of the melt pool from the top to the base plate resulting in heat accumulation and residual stresses due to the higher aspect ratio of the melt pool. Low heat transfer of thin walls also affects the cooling rate and can finally lead to crack propagation or warping inside the part [23,24]. L-PBF process parameter optimization can assist in minimizing defect formation [25]. A few optimized process parameter studies from the literature focused on the effects of process parameters on the microstructure, mechanical properties, and manufacturability of thin-walled Cp-Ti structures. Zhang et al. [24] discussed the microstructure and tensile properties of fabricated thin-walled titanium structures via L-PBF. Ataei et al. [8] studied the microstructure, surface roughness, and hardness features of manufactured porous Cp-Ti structures via L-PBF. Montufar et al. [26] also investigated the microstructure and mechanical properties of L-PBF-produced lattice-structured Cp-Ti for tissue engineering. However, the tested process parameters on thin-walled Cp-Ti, including laser power, scanning speed, layer thickness, hatch distance, and VED, are not well defined comprehensively in the mentioned studies due to inadequate ranges of parameter sets.

The aim of this study is to identify process parameters, mainly laser power, scan speed, layer thickness, and hatch distance for bulk and thin wall manufacturing that are especially suitable for lattice structures integrated into bulk parts. Both sets of process parameters, which can also be combined into a single parameter as VED, require a high density to ensure good mechanical properties. Moreover, for thin wall manufacturing, high dimensional accuracy is also desired. Thus, this study seeks to find suitable sets of parameters based on their effect on density, and this task was carried out by generating process maps in terms of scan speed and laser power at different hatch distance and layer thickness values specifying which parameters lead to full density or different types of porosities such as keyhole or lack of fusion. The mechanical properties of highly dense samples produced with determined sets of parameters were evaluated with hardness tests and tensile tests.

## 2. Materials and Methods

### 2.1. Materials

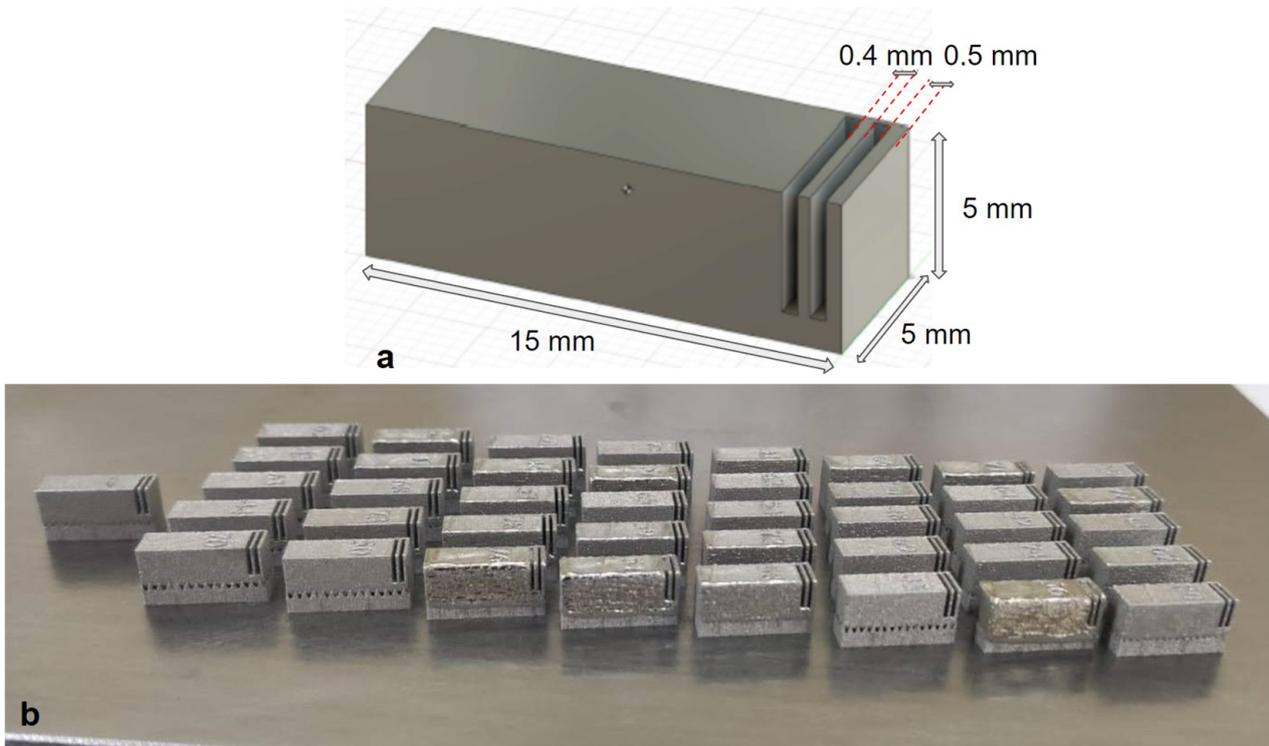
In this study, the L-PBF process parameter optimization was performed using EOSPRINT 2.8 software with gas-atomized spherical Cp-Ti Grade 2 (supplied by EOS) powder on EOS M290 L-PBF equipment. The average particle size ( $d_{50}$ ) is specified to be between 38 and 45  $\mu\text{m}$  [27].

### 2.2. Methods

#### Cp-Ti Process Parameter Optimization

A simple prismatic part was used with outer dimensions of  $5 \times 15 \times 5$  mm with two thin walls having thicknesses of 0,4 mm and 0,5 mm (see Figure 2a). The laser power (LP) was varied between 150 and 300 W (at 4 levels), whereas the scan speed (SS) was varied between 400 and 1200 mm/s (at 5 levels), while the hatch distance (HD) was set to either 90 or 110  $\mu\text{m}$  (2 levels) and the layer thickness (LT) was selected either 40 or 60  $\mu\text{m}$  (2 levels) (see Table 2). This led to 80 different parameter sets with different VED values varying

between 19 and 208 J/mm<sup>3</sup>. Moreover, one sample of each with 40 μm and 60 μm layer thickness was produced with standard parameters (laser power of 340 W, scan speed of 125 mm/s, and hatch distance of 120 μm) for comparison.



**Figure 2.** (a) Design of prismatic sample geometry with 0.4 mm and 0.5 mm thin walls; (b) Manufactured samples with 60 μm layer thickness.

**Table 2.** L-PBF AM process parameter sets and VED ranges of Cp-Ti samples.

Parameter Set	Laser Power (W)	Scan Speed (mm/s)	Hatch Distance (μm)	Layer Thick. (μm)	VED (J/mm <sup>3</sup> )	
Density 80 Sets	150	400	90	40	19–104	
		600				
		800				
		1000				
		1200				
	200	400	90	40	25–139	
		600				
		800				
		1000				
		1200				
	250	400	90	40	32–173	
		600				
800						
1000						
1200						
300	400	90	40	38–208		
	600					
	800					
	1000					
	1200					
Tensile Test	C1	250	1200	110	40	47
	C2	200	1000	110	40	45
	C3	200	1400	110	40	32

Up-skin and down-skin parameters were not utilized, and the stripe width was used as 7 mm by applying a stripe scanning pattern. Figure 2b shows 41 Cp-Ti samples produced at 60  $\mu\text{m}$  layer thickness in the first batch. After the best parameters from this preliminary test were determined based on the highest density and productivity, the parameters were tested in terms of mechanical properties (see Table 2). A total of 9 tensile test specimens with 100 mm length and 12 mm diameter were produced. Three different parameter sets were employed with three repetitions (see Figure 3a). All samples were sandblasted and heat treated at 780  $^{\circ}\text{C}$  for 2 h to relieve residual stresses while the specimens were attached to the base plate. Later, they were cut using wire electrical discharge machining (WEDM), and the tensile specimens were turned into the final geometry, as shown in Figure 3b.

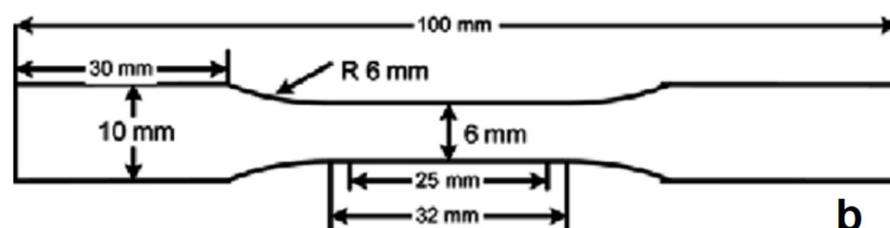
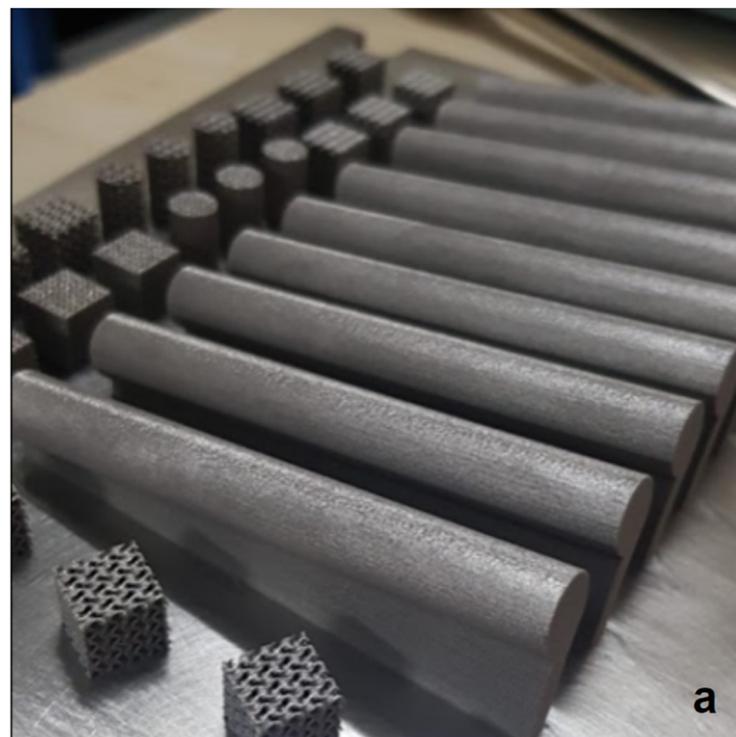
### 2.3. Material Characterization

#### 2.3.1. Density Measurements

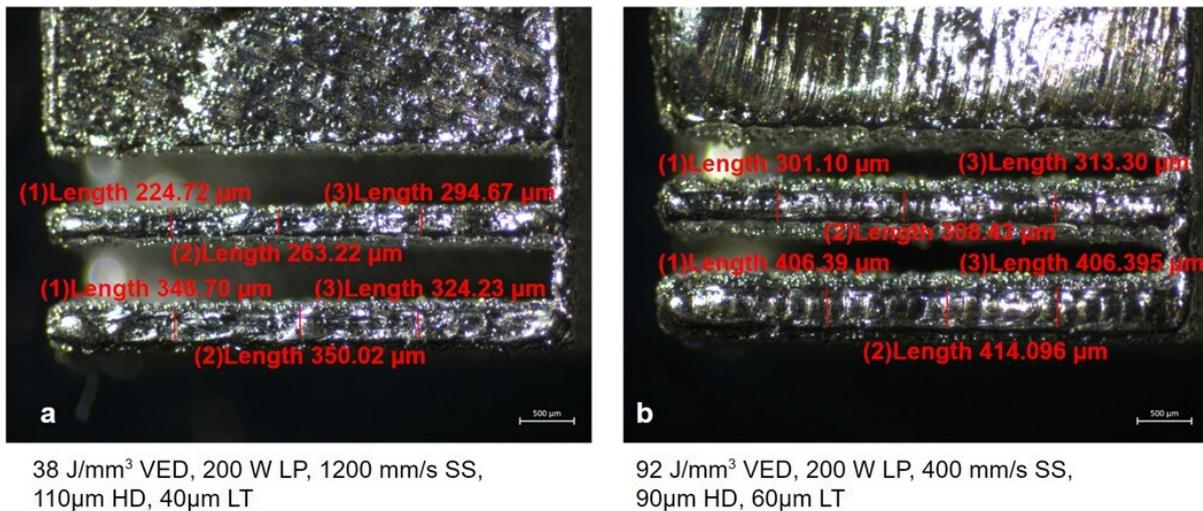
Metallography was applied to the cross-sections of prismatic samples along the build direction. For grinding, 1000 and 2500 grids were used, respectively, and then polishing with a diamond solution was performed. Density results were analyzed, and porosities were classified with an optical microscope (BX50, OLYMPUS).

#### 2.3.2. Dimensional Measurement of Thin Walls

Images from 0.4 mm and 0.5 mm thin walls were taken under a stereomicroscope (Stemi 508, ZEISS), and the thickness values were measured at 3 different locations. Figure 4 shows two examples made with different sets of process parameters.



**Figure 3.** (a) Nine as-built tensile test samples; (b) Dimensions of machined tensile test samples.



**Figure 4.** (a) Measurement of wall thicknesses at 40 µm layer thickness. (b) Measurement of wall thicknesses at 60 µm layer thickness.

### 2.3.3. Mechanical Tests

Vickers hardness (Duramin 4, Struers) was measured with 500 gf load at different locations on each sample (with approx. 100 µm interval) per ASTM E384. The samples were compared with a nominal hardness value (195 HV) of Cp-Ti grade 2 material data [27].

The tensile tests were performed on a Besmak BMT 200E tensile test device with 200 kN load capacity according to ASTM E8 standard. A mechanical extensometer (Epsilon 3542) was utilized for the elongation measurement. The tensile samples were tested with a 0,6 mm/min strain rate at room temperature. The fractured surfaces of the samples were investigated under a stereomicroscope (MZ16A, Leica).

## 3. Results and Discussion

### 3.1. Cp-Ti Density Characterization

Metallographic results of prismatic samples were classified, as shown in Figure 5, under 4 categories: fully dense, few number of small pores, keyhole porosity, and lack of fusion. Some examples of fully dense specimens are shown in Figure 5a,c,e, while an example of small pores is presented in Figure 5b. Lack of fusion porosity and keyhole are demonstrated in Figures 5d and 5f, respectively. The VED value for each sample shows that by only looking at this value, it is not possible to distinguish between different density levels. Very close VED values can lead to totally different density conditions, as depicted in Figure 5e,f. Almost the same VED (56–57 J/mm<sup>3</sup>) results in almost fully dense or keyhole porosity due to the combination of scan speed and laser power. This is better explained with the results shown in Figure 6, where VED and LED values for each parameter set are shown with 19–208 J/mm<sup>3</sup> and 0.125–0.75 J/mm ranges, respectively, and the resulting pore types are also symbolized in the process windows. Boundary lines separate almost fully dense parts from keyhole and lack of fusion porosities. Red parameter sets to the left of the boundary lines are keyhole porosities due to the high VED values. The blue sets above and around the boundary line have small pores, while the orange sets, which have low VED values, to the right of the line were formed as lack of fusion. Na et al. [10] also presented that the keyhole formation is seen as laser power increases from 120 W to 440 W, while lack of fusion generates as scan speed increases from 500 mm/s to 2000 mm/s. The outcomes showed similarity with Figure 6 outcomes.

The 5 parameter sets with very high VED values were canceled in 40 µm layer thickness batch as 139, 170, 173, and 208 J/mm<sup>3</sup>. The white rectangles in the graphs represent those sets that were not manufactured. High-dense green samples between the lines were determined as parameter sets to be worked on further in parameter optimization. Figure 6

shows that the number of fully dense samples increased as scan speed increased in all graphs regardless of layer thickness and hatch distance values. The almost fully dense samples were achieved practically for all laser power values except for 150 W. Small porosity formation can be observed at 800 and 1000 mm/s scan speed with all laser power values, while a lack of fusion pores generated at 1200 mm/s scan speed with 150 W for Figure 6b–d.

It was found that the number of almost full dense samples is lower at 60  $\mu\text{m}$  LT according to 40  $\mu\text{m}$  LT at the same LP, SS, and HD values (see Figure 6). It can be remarked that higher layer thickness causes a reduction in the density of cp-Ti parts.

Higher VED values were obtained at 90  $\mu\text{m}$  hatch distance because of heat accumulation [23,25] compared to 110  $\mu\text{m}$ . The increase in VED caused keyhole porosity formation at 90  $\mu\text{m}$  while small, porous, highly dense parts were achieved with 110  $\mu\text{m}$  hatch distance under the same LP (200 W), SS (800 mm/s), and LT (60  $\mu\text{m}$ ) values. Boundary lines between 1000 mm/s and 1200 mm/s SS and 200 W and 250 W LP mostly provide green samples, although VED values decreased as LT and HD increased at four graphics. The reason for this likely is that the laser power and scanning speed parameters influence density according to hatch distance and layer thickness. Na et al. [10] also achieved almost fully dense parts at 1000 mm/s scanning speed with 120 W to 440 W when LT is 30  $\mu\text{m}$  and HD is 120  $\mu\text{m}$ .

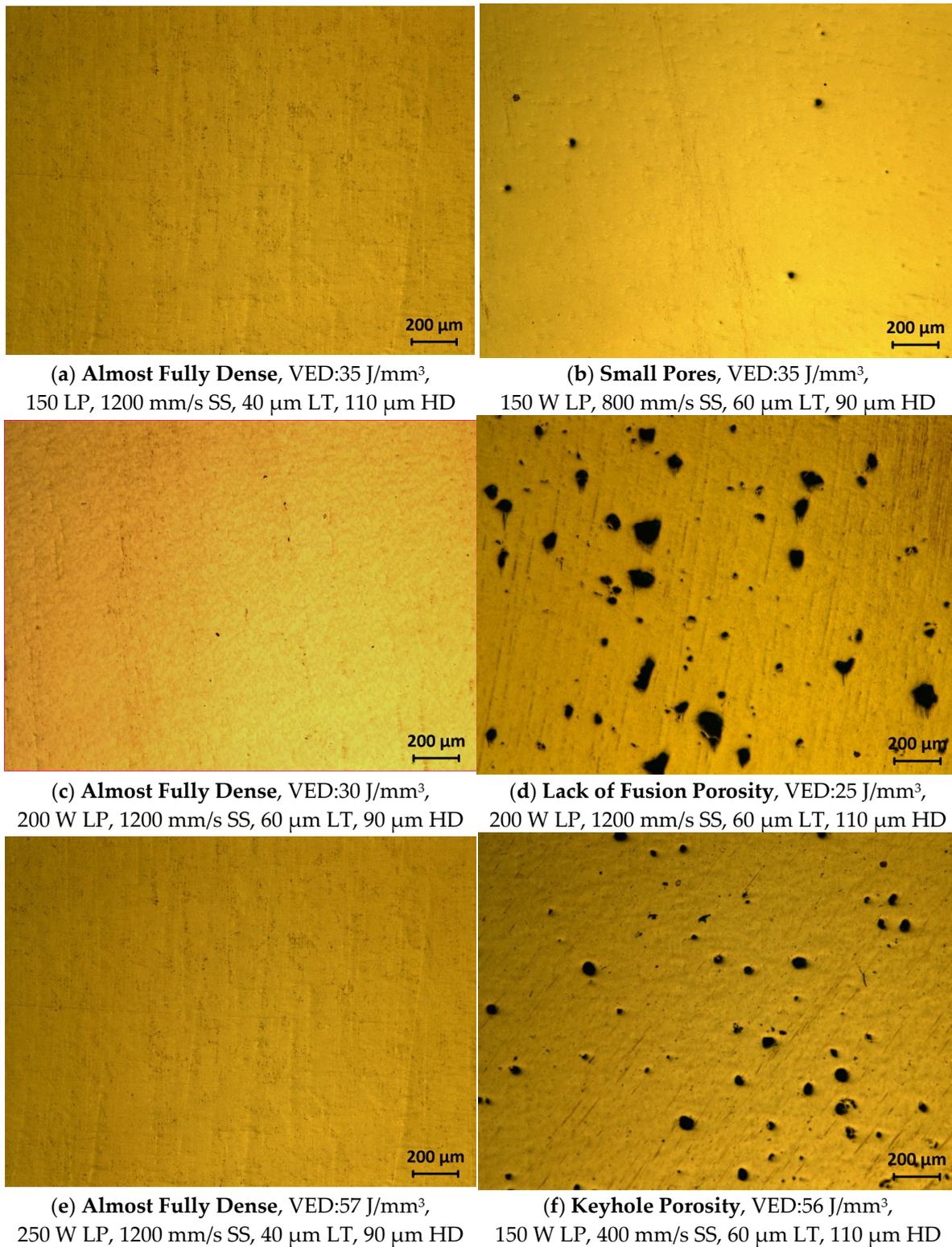
Almost full-density results can be obtained at certain ranges of laser power and scanning speed values, although VED values differ. This proves that the VED parameter is not the only criterion for the exposure process. Additionally, Figure 5 shows that both different types of porosity and almost full density can occur at the same or very close VED values. Another reason is that the physics of the complex melt pool cannot be explained since the interaction between the heat source and the powder is ignored in the VED formula [28].

Low layer thickness and high hatch distance are recommended with high scanning speed and moderate laser power values at the aforementioned outcomes as a result of the density characterization of Cp-Ti prismatic samples. Tensile test parameter sets were prepared according to the VED range of green samples in the graph within the scope of the study. In addition, reaching almost full density with 33 J/mm<sup>3</sup> [13] and 58 J/mm<sup>3</sup> [15] VED values shows that this study is also correlated with the literature.

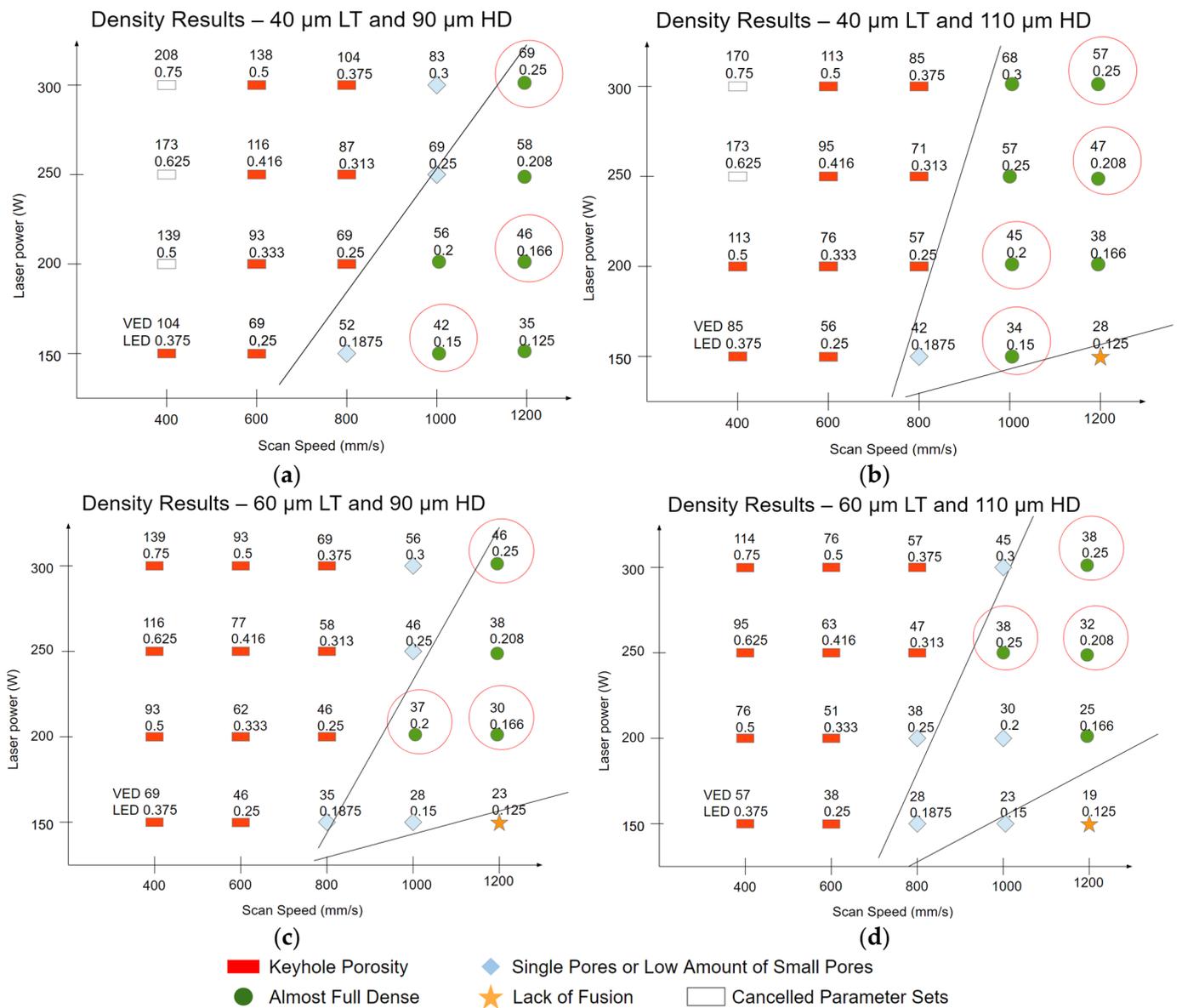
### 3.2. Dimensional Accuracy of Thin Walls

A dimensional error graph was created for the 0.4 mm (blue columns) and 0.5 mm (orange columns) wall thicknesses for each parameter set specified in Figure 7. Samples from parameter set number 1 to S40 (standard 40  $\mu\text{m}$  parameter set) were produced with 40  $\mu\text{m}$  layer thickness, while samples from 41 to S80 (standard 60  $\mu\text{m}$  parameter set) included 60  $\mu\text{m}$  layer thickness. Gaps in the graph are due to the parameter sets that were canceled due to high VED values.

The results show that the average dimensional error at a 60  $\mu\text{m}$  layer thickness was approximately 30% less than the average of the samples produced with a 40  $\mu\text{m}$  layer thickness. The effect of layer thickness on wall thickness can be explained with melt pool dimensions and laser track discontinuity [29]. Zhang et al. [29] stated that the melt pool sizes of lower layer thickness were larger than those with higher layer thickness under the same laser power and scanning speed since larger layer thickness requires more energy. It can be expressed that 60  $\mu\text{m}$  layer thickness needs higher laser energy for powder fusion according to 40  $\mu\text{m}$  in this study. Zhang et al. [29] indicated that the track discontinuity of the thicker layer is clearly higher than the thinner layer due to insufficient VED in addition to the melt pool size factor. Thin-walled structures can also generate heat accumulation which can cause crack propagation at high energy density. The heat is transferred from the top of the layer to the bottom faster as the layer thickness decreases; in other words, heat conductivity increases.

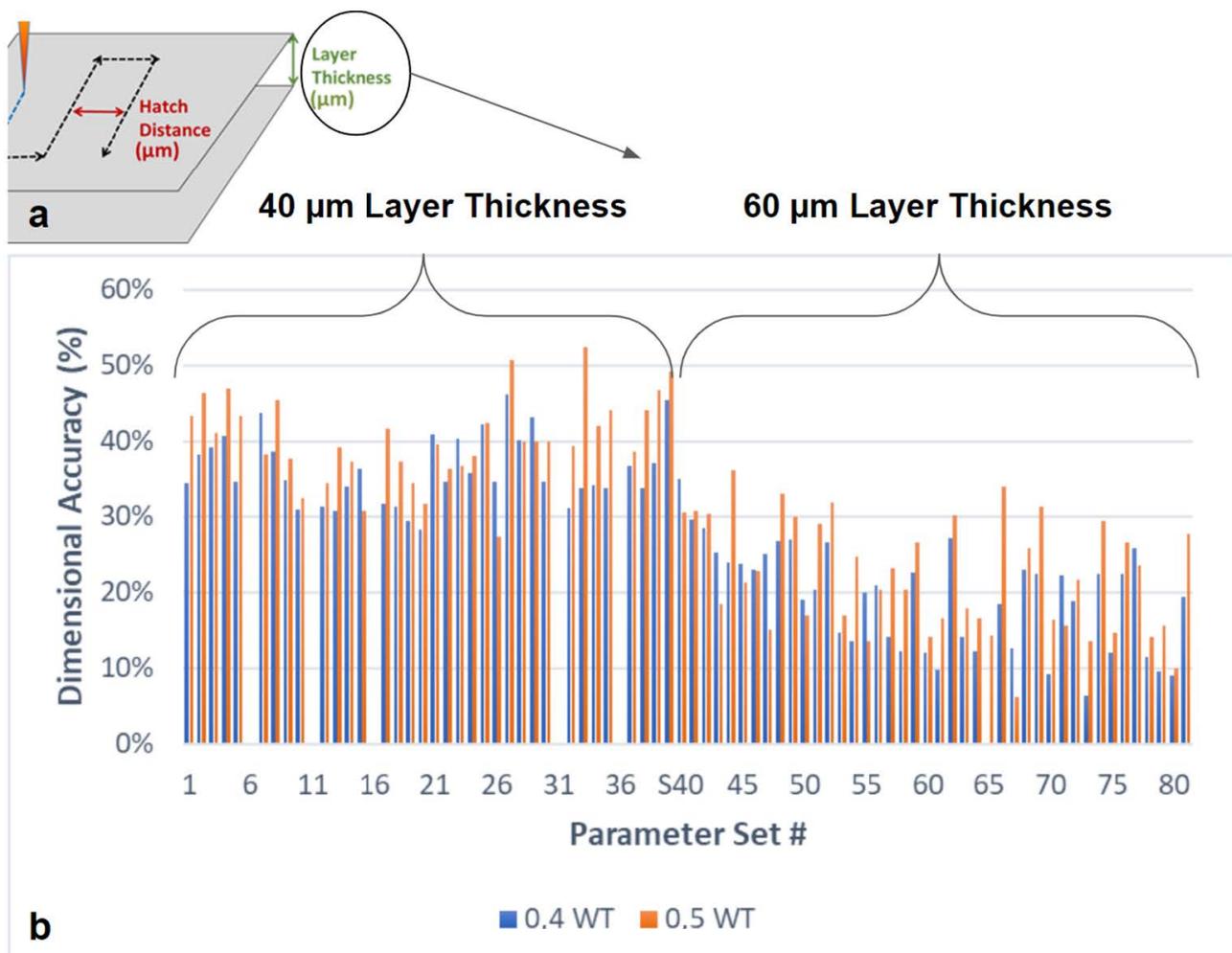


**Figure 5.** Porosity types classified between the nearly same VED values. (a) Almost fully dense part with 35 J/mm<sup>3</sup> VED. (b) Small pores with 35 J/mm<sup>3</sup> VED value. (c) Almost fully dense with 30 J/mm<sup>3</sup> VED value. (d) Lack of fusion porosity with 25 J/mm<sup>3</sup> VED value. (e) Almost fully dense with 57 J/mm<sup>3</sup> VED value. (f) Keyhole porosity with 56 J/mm<sup>3</sup> VED value.



**Figure 6.** Laser power and scan speed graphs present density results. Boundary lines separate almost full dense parts from keyhole and lack of fusion porous parts. VED and LED values are shown per graph (a) 40  $\mu\text{m}$  layer thickness (LT) and 90  $\mu\text{m}$  hatch distance (HD); (b) 40  $\mu\text{m}$  LT and 110  $\mu\text{m}$  HD; (c) 60  $\mu\text{m}$  LT and 90  $\mu\text{m}$  HD; (d) 60  $\mu\text{m}$  LT and 110  $\mu\text{m}$  HD.

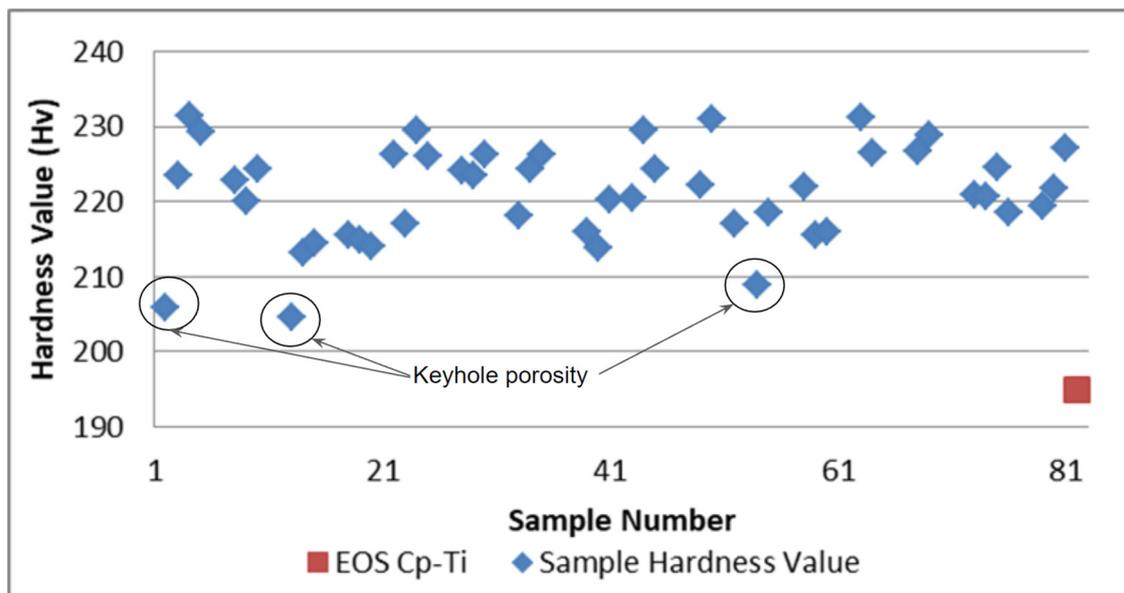
As a result, 40  $\mu\text{m}$  layer thickness can form sufficient melt pool dimensions and melt track when it is combined with the right process parameters, and dimensional error can be tolerated with design compensation. Another advantage of 40  $\mu\text{m}$  LT is greater performance on density results, as indicated in Section 3.1. The individual effects of scan speed, laser power, and hatch distance were, moreover, less noticeable on wall thickness after evaluation of all parameter sets.



**Figure 7.** (a) Presentation of layer thickness. Reproduced with permission from Oliveira et al. [20]; [Mater. Des]; [Elsevier]; [2020]. (b) Dimensional error and parameter set graph of Cp-Ti thin walls that have blue and orange bars present 0.4 mm and 0.5 mm thin walls, respectively. 40  $\mu\text{m}$  LT is presented from 1 parameter set to S40 (EOS Ti6Al4V standard 40  $\mu\text{m}$  LT parameter set), while 60  $\mu\text{m}$  LT includes the parameter sets from 41 to S60 (EOS Ti6Al4V standard 60  $\mu\text{m}$  LT parameter set).

### 3.3. Mechanical Testing Results

The hardness test was applied to samples with high density and, additionally, to 3 samples with keyhole pores. The average Vickers hardness values of the tested highly dense samples are in the 210–230 HV range, while the specified hardness value for Cp-Ti in the material data is 195 HV [29], as seen in the distribution graph in Figure 8. Ataei et al. [8] stated that the hardness value of fabricated Cp-Ti with L-PBF is 232 HV, and thus the test results of this study are consistent with the literature. Three samples with keyhole pores showed the lowest hardness values in the graph (Figure 8). Therefore, the hardness values of the samples were wholly correlated with the density results; in other words, the VED parameter has an excellent impact on the hardness. Individual effects of process parameters on the material hardness were not observed.



**Figure 8.** Hardness values of highly dense Cp-Ti samples were compared to Cp-Ti material data (195 HV) at the Vickers hardness test.

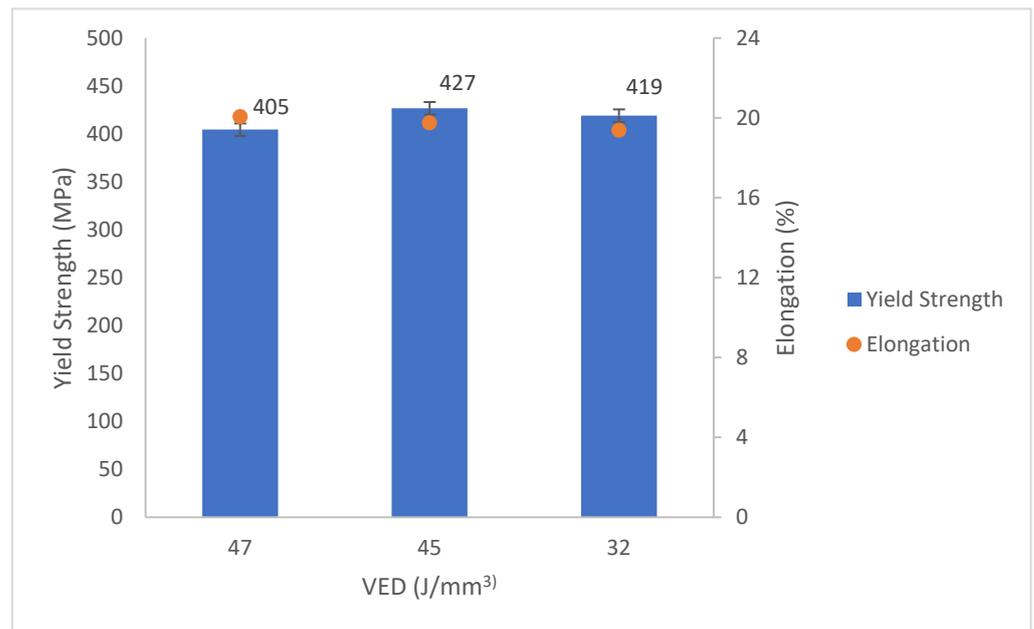
Tensile tests were carried out on highly dense samples in accordance with the E8 standard. The aim of the test is to see whether the obtained properties with the L-PBF optimized process parameters are close to the material properties in the literature. Three parameter sets with 32, 45, and 47 J/mm<sup>3</sup> VED values were produced as three samples per set.

Yield strength (YS) and ultimate tensile strength (UTS) of the material property datasheet [27] of Cp-Ti were indicated as 445 MPa and 570 MPa, respectively, and referenced for this study. Yield strength and elongation values of manufactured parts by 3 parameter sets are shown in Figure 9, and 542 MPa UTS was also measured for all VED values (see Table 3). Experimental test results exhibited slightly lower values than referenced mechanical properties. The lowest YS value (405 MPa) was almost 9% lower than referenced YS, and UTS was measured 5% less for tensile samples, although all parameter sets for tensile tests were chosen from the optimum process parameter ranges to provide high density. The reason might be that the heat treatment was applied to tensile samples with 780 °C in this study, while referenced values were obtained with 700 °C heat treatment. On the other hand, hardness test specimens were higher than the reference values since no heat treatment was applied.

**Table 3.** Tensile test results of three different parameter sets.

Tensile Parameters	VED (J/mm <sup>3</sup> )	UTS (MPa)	Yield Strength (MPa)	Elongation (%)
C1	47	542	405	20.0
C2	45	542	427	19.7
C3	32	542	419	19.4

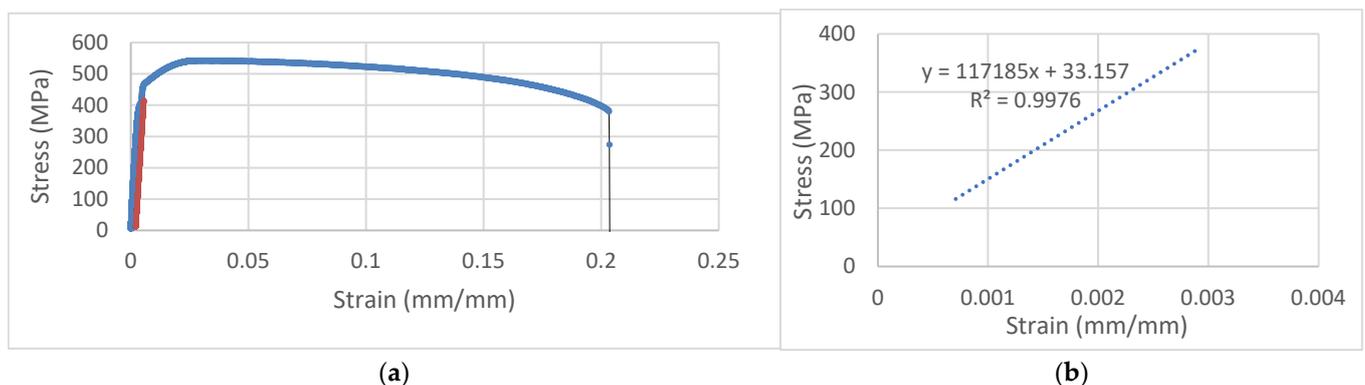
The yield strength obtained with the 47 J/mm<sup>3</sup> VED parameter set was slightly lower than the 45 and 32 J/mm<sup>3</sup> samples, as shown in Figure 9. The reason might be 250 W laser power value of 47 J/mm<sup>3</sup> causes a low amount of small pores formation and resulting lower mechanical behavior than the 200 W laser power of 45 and 32 J/mm<sup>3</sup> parameter sets. On the other hand, UTS values of 542 MPa were measured to be approximately the same for three sets which are very close to the 570 MPa UTS reference value.



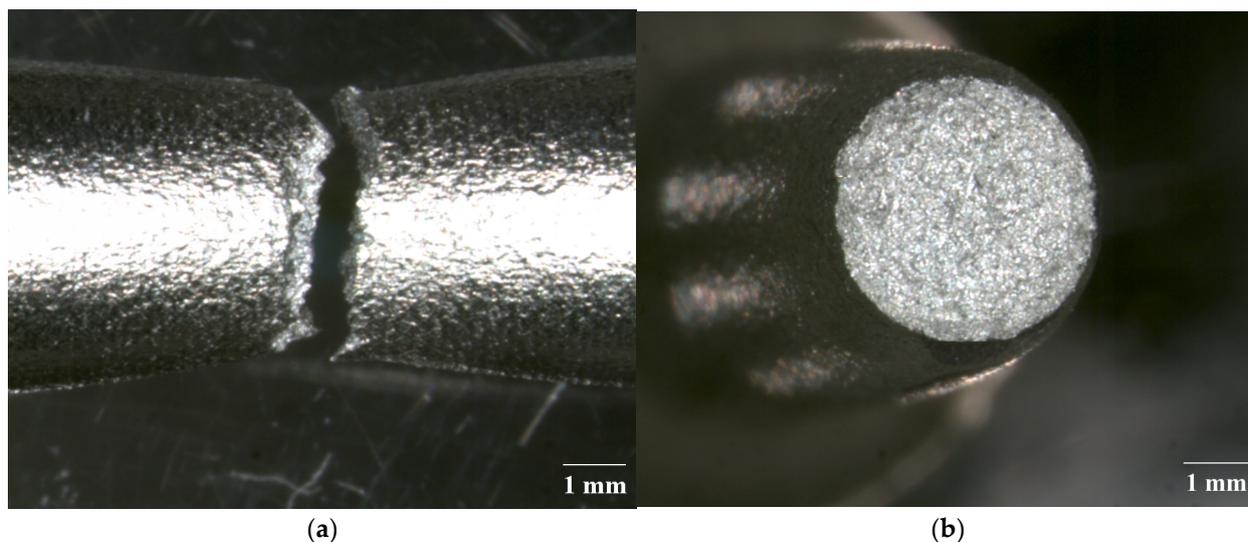
**Figure 9.** Yield strength, elongation, and VED values graph for Cp-Ti tensile test results.

It should be noted that in some other references, depending on the grade and production parameters, the obtained mechanical properties show a high scatter. As given in [30,31], grade 2 Cp-Ti can lead to a tensile strength of 345 MPa, which is significantly lower than the reference value that is obtained with a layer thickness of 30  $\mu\text{m}$  and the results obtained in this study. Moreover, another reference material datasheet, which can be found in [31], states that the UTS is 570 Mpa, whereas YS is 430 MPa maximum. These results were also obtained with 30  $\mu\text{m}$  by the same machine vendor and are closer to the results of the current work. Another powder supplier [32] specifies that the minimum UTS shall be 345 MPa with typical UTS values in the range of 510–605 MPa, while the minimum YS shall be 275 MPa with typical YS values in the range of 335–545 MPa. This also proves that the mechanical properties obtained here are well above the minimum and satisfy the typical ranges.

One of the tensile test sample's stress–strain graph is shown in Figure 10a, and its 117 GPa elastic modulus value was determined via linear regression equation in Figure 10b. Elongation at break was measured at almost 20%, while 26% elongation was stated in the reference data [27]. In addition, the necking of the tensile sample with a reduction in diameter is indicative of the ductile fracture in Figure 11. Additionally, Attar et al. [14] found 18% elongation and higher than 250 HV hardness in samples with 99,5% relative density.



**Figure 10.** (a) Stress–strain graph of tensile test sample. (b) Elastic modulus of tensile test sample.



**Figure 11.** (a) Necking of tensile test sample's fracture. (b) Top view of tensile fracture.

#### 4. Conclusions

The current L-PBF process parameter optimization study was carried out on Cp-Ti, investigating the fabricability of thin walls with high density and good mechanical properties. A wide range of scan speed, laser power, hatch distance, and layer thickness values were investigated, leading to the fact that a VED value in the range of 32–47 J/mm provided high density and adequate mechanical properties.

- Within the tested ranges, a low layer thickness and a high hatch distance are recommended with high scan speed and moderate laser power values. The laser power and scan speed parameters have a higher influence on the density.
- The wall thicknesses obtained with the tested parameters were lower than the nominal 400 and 500  $\mu\text{m}$ , while 60  $\mu\text{m}$  led to smaller dimensional errors and achieved closer to the nominal thickness values. However, to increase the resolution along the z-axis and obtained density for small features, it is recommended to use smaller layer thicknesses.
- In terms of mechanical properties, in comparison to the literature, satisfying results are obtained with the selected process parameters well above the minimum requirements.
- It is concluded that low layer thickness and low laser power favored the producibility of thin-walled Cp-Ti structures, while high scan speed and moderate laser power were able to achieve almost full density.

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## References

1. Rahmatabadi, D.; Soltanmohammadi, K.; Aberoumand, M.; Soleyman, E.; Ghasemi, I.; Baniassadi, M.; Abrinia, K.; Bodaghi, M.; Baghani, M. Development of Pure Poly Vinyl Chloride (PVC) with Excellent 3D Printability and Macro-and Micro-Structural Properties. *Macromol. Mater. Eng.* **2022**, *2200568*. [[CrossRef](#)]
2. Ahmadi, M.; Tabary, S.B.; Rahmatabadi, D.; Ebrahimi, M.S.; Abrinia, K.; Hashemi, R. Review of Selective Laser Melting of Magnesium Alloys: Advantages, Microstructure and Mechanical Characterizations, Defects, Challenges, and Applications. *J. Mater. Res. Technol.* **2022**, *19*, 1537–1562. [[CrossRef](#)]
3. Abedi, H.R.; Hanzaki, A.Z.; Azami, M.; Kahnooji, M.; Rahmatabadi, D. The high temperature flow behavior of additively manufactured Inconel 625 superalloy. *Mater. Res. Express* **2019**, *6*, 116514. [[CrossRef](#)]
4. Sing, S.L.; Huang, S.; Goh, G.D.; Goh, G.L.; Tey, C.F.; Tan, J.H.K.; Yeong, W.Y. Emerging metallic systems for additive manufacturing: In-situ alloying and multi-metal processing in laser powder bed fusion. *Prog. Mater. Sci.* **2021**, *119*, 100795. [[CrossRef](#)]
5. Yuan, L.; Ding, S.; Wen, C. Additive manufacturing technology for porous metal implant applications and triple minimal surface structures: A review. *Bioact. Mater.* **2019**, *4*, 56–70. [[CrossRef](#)]
6. Khorasani, A.M.; Goldberg, M.; Doeven, E.H.; Littlefair, G. Titanium in biomedical applications—Properties and fabrication: A review. *J. Biomater. Tissue Eng.* **2015**, *5*, 593–619. [[CrossRef](#)]
7. Navi, N.U.; Tenenbaum, J.; Sabatani, E.; Kimmel, G.; David, R.B.; Rosen, B.A.; Eliaz, N. Hydrogen effects on electrochemically charged additive manufactured by electron beam melting (EBM) and wrought Ti–6Al–4V alloys. *Int. J. Hydrogen Energy* **2020**, *45*, 25523–25540. [[CrossRef](#)]
8. Ataee, A.; Li, Y.; Brandt, M.; Wen, C. Ultrahigh-strength titanium gyroid scaffolds manufactured by selective laser melting (SLM) for bone implant applications. *Acta Mater.* **2018**, *158*, 354–368. [[CrossRef](#)]
9. Depboylu, F.N.; Yasa, E.; Poyraz, Ö.; Minguella-Canela, J.; Korkusuz, F.; De los Santos López, M.A. Titanium based bone implants production using laser powder bed fusion technology. *J. Mater. Res. Technol.* **2022**, *17*, 1408–1426. [[CrossRef](#)]
10. Wang, D.W.; Zhou, Y.H.; Shen, J.; Liu, Y.; Li, D.F.; Zhou, Q.; Yan, M. Selective laser melting under the reactive atmosphere: A convenient and efficient approach to fabricate ultrahigh strength commercially pure titanium without sacrificing ductility. *Mater. Sci. Eng. A* **2019**, *762*, 138078. [[CrossRef](#)]
11. Wysocki, B.; Maj, P.; Krawczyńska, A.; Roźniatowski, K.; Zdunek, J.; Kurzydłowski, K.J.; Świążkowski, W. Microstructure and mechanical properties investigation of CP titanium processed by selective laser melting (SLM). *J. Mater. Process. Technol.* **2017**, *241*, 13–23. [[CrossRef](#)]
12. Li, X.P.; Van Humbeeck, J.; Kruth, J.-P. Selective laser melting of weak-textured commercially pure titanium with high strength and ductility: A study from laser power perspective. *Mater. Des.* **2017**, *116*, 352–358. [[CrossRef](#)]
13. Na, T.W.; Kim, W.R.; Yang, S.M.; Kwon, O.; Park, J.M.; Kim, G.H.; Kim, H.G. Effect of laser power on oxygen and nitrogen concentration of commercially pure titanium manufactured by selective laser melting. *Mater. Charact.* **2018**, *143*, 110–117. [[CrossRef](#)]
14. Attar, H.; Calin, M.; Zhang, L.C.; Scudino, S.; Eckert, J. Manufacture by selective laser melting and mechanical behavior of commercially pure titanium. *Mater. Sci. Eng. A* **2014**, *593*, 170–177. [[CrossRef](#)]
15. Gu, D.; Hagedorn, Y.C.; Meiners, W.; Meng, G.; Batista, R.J.S.; Wissenbach, K.; Poprawe, R. Densification behavior, microstructure evolution, and wear performance of selective laser melting processed commercially pure titanium. *Acta Mater.* **2012**, *60*, 3849–3860. [[CrossRef](#)]
16. Dong, Y.P.; Tang, J.C.; Wang, D.W.; Wang, N.; He, Z.D.; Li, J.; Yan, M. Additive manufacturing of pure Ti with superior mechanical performance, low cost, and biocompatibility for potential replacement of Ti–6Al–4V. *Mater. Des.* **2020**, *196*, 109142. [[CrossRef](#)]
17. Loginov, Y.N.; Stepanov, S.I.; Ryshkov, N.M.; Yudin, A.V.; Tretyakov, E.V. Effect of SLM parameters on the structure and properties of CP-Ti. In *AIP Conference Proceedings*; AIP Publishing LLC: Melville, NY, USA, 2018; p. 040052. [[CrossRef](#)]
18. Pfaff, A.; Jäcklein, M.; Schlager, M.; Harwick, W.; Hoschke, K.; Balle, F. An empirical approach for the development of process parameters for laser powder bed fusion. *Materials* **2020**, *13*, 5400. [[CrossRef](#)] [[PubMed](#)]
19. Ferro, P.; Meneghello, R.; Savio, G.; Berto, F. A modified volumetric energy density–based approach for porosity assessment in additive manufacturing process design. *Int. J. Adv. Manuf. Technol.* **2020**, *110*, 1911–1921. [[CrossRef](#)]
20. Oliveira, J.P.; Lalonde, A.D.; Ma, J. Processing parameters in laser powder bed fusion metal additive manufacturing. *Mater. Des.* **2020**, *193*, 108762. [[CrossRef](#)]
21. Ahmed, N.; Barsoum, I.; Haidemenopoulos, G.; Al-Rub, R.A. Process parameter selection and optimization of laser powder bed fusion for 316L stainless steel: A review. *J. Manuf. Process.* **2022**, *75*, 415–434. [[CrossRef](#)]
22. Mohr, G.; Altenburg, S.J.; Hilgenberg, K. Effects of inter layer time and build height on resulting properties of 316L stainless steel processed by laser powder bed fusion. *Addit. Manuf.* **2020**, *32*, 101080. [[CrossRef](#)]
23. Pazon, C.; Leicht, A.; Klement, U.; Forêt, P.; Hryha, E. Effect of the process gas and scan speed on the properties and productivity of thin 316L structures produced by laser-powder bed fusion. *Metall. Mater. Trans. A* **2020**, *51*, 5339–5350. [[CrossRef](#)]

24. Zhang, Z.; Yang, X.; Song, F.; Yao, X.; Zhang, T.; Liu, S.; Tang, H. Assessment of microstructural evolution and associated tensile behavior in thin-walled Ti6Al4V parts manufactured via selective laser melting. *Mater. Charact.* **2022**, *194*, 112481. [[CrossRef](#)]
25. Chaudry, M.A.; Mohr, G.; Hilgenberg, K. Experimental and numerical comparison of heat accumulation during laser powder bed fusion of 316L stainless steel. *Prog. Addit. Manuf.* **2022**, *7*, 1071–1083. [[CrossRef](#)]
26. Montufar, E.B.; Tkachenko, S.; Casas-Luna, M.; Škarvada, P.; Slámečka, K.; Diaz-de-la-Torre, S.; Kaiser, J. Benchmarking of additive manufacturing technologies for commercially-pure-titanium bone-tissue-engineering scaffolds: Processing-microstructure-property relationship. *Addit. Manuf.* **2020**, *36*, 101516. [[CrossRef](#)]
27. EOS Titanium TiCP Grade 2, EOS GmbH Electro Optical Systems, Finland. 2016. Available online: [www.eos.info](http://www.eos.info) (accessed on 21 January 2023).
28. Bertoli, U.S.; Wolfer, A.J.; Matthews, M.J.; Delplanque, J.P.R.; Schoenung, J.M. On the limitations of volumetric energy density as a design parameter for selective laser melting. *Mater. Des.* **2017**, *113*, 331–340. [[CrossRef](#)]
29. Zhang, Z.; Ali, U.; Mahmoodkhani, Y.; Huang, Y.; Shahabad, S.I.; Kasinathan, A.R.; Toyserkani, E. Experimental and numerical investigation on the effect of layer thickness during laser powder-bed fusion of stainless steel 17-4PH. *Int. J. Rapid Manuf.* **2020**, *9*, 212. [[CrossRef](#)]
30. EOS Titanium TiCP Grade 2, EOS GmbH Electro Optical Systems. Finland. 2009. Available online: [https://www.3dimpuls.com/sites/default/files/dok\\_book/m\\_materials\\_en.pdf](https://www.3dimpuls.com/sites/default/files/dok_book/m_materials_en.pdf) (accessed on 21 January 2023).
31. EOS Titanium TiCP Grade 2, EOS GmbH Electro Optical Systems. Finland. 2017. Available online: [https://www.eos.info/03\\_system-related-assets/material-related-contents/metal-materials-and-examples/metal-material-datasheet/titan/ticp\\_9011-0036\\_m404\\_material\\_data\\_sheet\\_12-17\\_flexline\\_en.pdf](https://www.eos.info/03_system-related-assets/material-related-contents/metal-materials-and-examples/metal-material-datasheet/titan/ticp_9011-0036_m404_material_data_sheet_12-17_flexline_en.pdf) (accessed on 21 January 2023).
32. EOS Titanium TiCP Grade 2, EOS GmbH Electro Optical Systems. Finland. 2000. Available online: <https://www.carpentertechnology.com/hubfs/7407324/Material%20Saftey%20Data%20Sheets/Ti%20CP%20Grade%202.pdf> (accessed on 21 January 2023).

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