

## Article

# Research on Fractal Characteristics and Influencing Factors of Pore-Throats in Tight Sandstone Reservoirs: A Case Study of Chang 6 of the Upper Triassic Yanchang Formation in Huaqing Area, Ordos Basin, China

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**Abstract:** In recent years, tight sandstone oil and gas have been an important area for unconventional oil and gas exploration and development in China. It is of great significance to clarify the pore-throat structure characteristics of tight sandstone reservoirs to guide production practices. This study takes the tight sandstone of the sixth member of the Yanchang Formation in the Huaqing area, Ordos Basin, as an example, based on experimental methods such as high-pressure mercury intrusion, cast thin sections and scanning electron microscopy. At the same time, the pore-throat structure of tight sandstone reservoirs is divided into three types using the tube-bundle and spherical fractal models. The corresponding pore and throat radius distribution, pore-throat combination mode and influencing factors of various pore-throats are studied. The results show that the fractal dimension of type I pore-throats is the smallest, and the distribution of their pore-throat radii is the most uniform. They are dominated by intercrystalline pores and dissolution pores with tube-bundle throats and small pores with small throats. Type II pore-throats have the largest fractal dimension and the worst pore-throat uniformity. They are dominated by residual primary intergranular pores with necked throats and large pores with small throats. The type III pore-throat fractal dimension is in the middle, mainly composed of residual dissolved intergranular pores with pore-reduced throats, sheet-like and curved sheet-like throats, and large pores with large throats. The influence of different pore-throat combinations on the reservoir is reflected in the different characteristics of mercury injection parameters. The main influencing factors for the differences in the fractal dimensions of different pore-throats are diagenesis, rock composition and pore-throat combination type. Diagenesis and rock composition, in turn, affect the type and development degree of pore-throats, as well as the combination of pore-throats. The purpose of this study was to clarify the internal connection modes of different homogeneous pore-throats and their influencing factors, enrich the theoretical basis for the study of tight sandstone reservoirs and provide theoretical guidance for their exploration and development.

**Keywords:** pore-throat structure; fractal dimension; influencing factors; member 6 of Yanchang Formation; Huaqing area; Ordos Basin



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## 1. Introduction

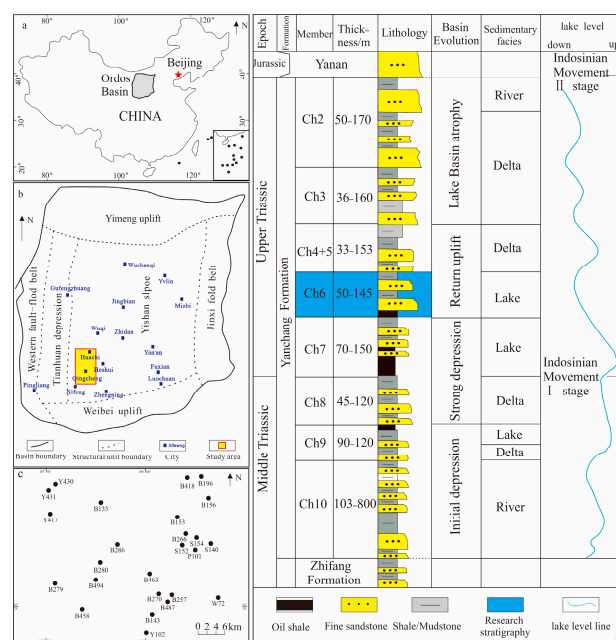
The fractal dimension was first proposed by mathematician Mandelbrot in 1975 [1–3]. The fractal dimension is a general term for figures, structures and phenomena that have no characteristic length but have similarities. It reflects the basic properties of a wide range of objects in nature, that is, the self-similarity between part and part and between part and

whole in form, function and information [4,5]. It is a mathematical statistical theory to study the self-similarity of objects, and it is a relatively accurate quantitative representation reflecting the inhomogeneity of the basic properties of a formation in three-dimensional space [6,7]. After decades of exploration and research, the fractal dimension has become relatively mature in the fields of physics [8], mathematics [9], geology [10,11] and materials [12] and has achieved corresponding results. In the field of geology, it is mainly used in coal seams [13,14], tight sandstone reservoirs [15], mud shale [16,17] and other pore structure characterization [18,19]; reservoir heterogeneity characterization [20]; and determining the influencing factors of reservoir densification [21]. The data relied on mainly come from experiments such as high-pressure mercury intrusion [2,3,5], constant-rate mercury intrusion [22], nitrogen adsorption [16], CT scanning [23] and nuclear magnetic resonance [24,25].

Previous researchers have performed much research on the pore-throat structure of different tight sandstone reservoirs based on mercury intrusion data using fractal dimensions [3,5,15]. However, most of them only use a fractal model to study the pore-throat structure, and the results obtained are not comprehensive and objective. Research on the factors that cause differences in the different types of pore-throat structures is not detailed enough [21,22]. In this study, the sixth member of the Upper Triassic Yanchang Formation (hereafter referred to as the Chang 6 Member) in the Huaqing area of the Ordos Basin was examined, based on high-pressure mercury intrusion data, combined with experimental methods such as cast thin sections, scanning electron microscopy and two fractals (a sphere and a tube bundle), which were used at the same time. A model was developed to study the fractal characteristics of tight sandstone reservoirs. Innovations were achieved in the methodology for classifying pore-throats, classifying the pore-throat types and clarify the relationships between the fractal characteristics of different types of pore-throat and reservoir physical properties and parameters related to mercury intrusion. The reasons for the different pore-throat types were studied in detail, and the main pore and throat combination types in various pore-throat types were clarified. This study provides a theoretical basis for the exploration and exploitation of tight sandstone reservoirs.

## 2. Geological Setting

The Ordos Basin mainly experienced the Luliang Movement, the Jinning Movement, the Caledonian Movement [26,27], the Hercynian Movement [28,29], the Indosinian Movement and the Himalayan Movement [30,31]. The contour of the basin tends to be obvious from the late Indosinian Movement, when the deposition centre is biased to the south of the basin, but the subsidence centre is biased to the west of the basin [32]. The overall uplift of the basin occurred during the Himalayan Movement, when the lake basin tended to disappear, forming the current basin pattern. The entire basin is relatively complete from bottom to top, and the Silurian to Lower Carboniferous strata are mainly missing [33]. The Huaqing area is located southwest of the Yishaan slope (Figure 1b). The Upper Triassic Yanchang Formation is divided into 10 oil layers from bottom to top, which are called Chang 10 to Chang 1. The lake basin had the largest area during the Chang 7 period after experiencing the process of water inflow and outflow during lake basin expansion [34,35], shrinkage and disappearance, and the lake basin in the Chang 6 period was in the shrinking stage [36] (Figure 1c). Gravity flow deposits were mainly developed in the study area [37], and the scale of sand body deposits is large, forming favourable reservoirs.



**Figure 1.** The location of the study area and the stratigraphic column of the Yanchang Formation. (a) The location of the Ordos Basin; (b) the location of the study area; (c) the key well locations in the study area; (d) the stratigraphic column of the Yanchang Formation in the study area (modified from [34]).

The distribution of sand bodies in the Chang 6 reservoir in the study area varies greatly on the plane, with different thicknesses [38]. The sedimentary environment is mainly delta and lake [39,40]. The frequencies of mudstone interlayers are also different, and mudstone interlayers have a certain impact on the continuity of the reservoir [41]. The lithology is mainly composed of siltstone, fine sandstone, argillaceous siltstone, silty mudstone, etc. [42,43]. The reservoir belongs to tight sandstone reservoirs with low porosity ( $5 \leq \text{porosity} \leq 10$ ), extra-low porosity (porosity  $\leq 5$ ) and ultra-low permeability (permeability  $\leq 1$ ), and the relationship between porosity and permeability is good [44]. Affected by compaction, the macroscopic and microscopic heterogeneity of the reservoir is considerable [45,46].

### 3. Experimental Data and Methods

#### 3.1. Experimental Data

In this study, the research on the rock composition and storage space type of the Chang 6 reservoir in the Huaqing area was based on 546 cast thin section data, scanning electron microscopy and other experimental testing methods. The thin sections were impregnated with red-dyed epoxy. Parameters such as reservoir porosity, permeability, sorting coefficient, mercury removal efficiency, capillary pressure and mercury injection saturation were obtained through 59 high-pressure mercury intrusion experiments. Scanning electron microscopy was performed using a JSM-7500F instrument at room temperature. The cast thin sections were identified using a ZEISS Z1 polarizing microscope at 20 °C and ambient humidity of 50% for rock composition and pore types. The experimental instruments used for high-pressure mercury porosimetry were an American Corelab CM300 and an American Autopore IV9505 mercury porosimeter. The samples were dried at 105 °C to constant weight before testing. The mercury intrusion experiment included pressurized mercury injection and reduced-pressure mercury removal. The maximum experimental pressure was 200 MPa.

The calculation of the pore-throat radius was obtained using the capillary pressure calculation formula (Equation (1)) [2,3], where  $P_c$  = the capillary pressure between the mercury and air,  $R$  is the pore-throat radius,  $\sigma$  is the interfacial tension taken as 480 dyn/cm

and  $\theta$  is the contact angle between mercury and the rock surface, which is  $140^\circ$ . The fractal dimension of the capillary pressure was obtained through the establishment of a spherical fractal model and a tube-bundle fractal model.

$$P_c = \frac{2\sigma \cos\theta}{R} \quad (1)$$

### 3.2. Fractal Dimension Model

Currently, there are two main methods for calculating the fractal dimension of the high-pressure mercury intrusion capillary pressure curve: the sphere-type model and the tube-bundle-type model. The calculation formula is as follows (Table 1). According to the calculation formulas of the two models, the two models should be suitable for pore-throats with a mercury injection gradient of less than 1 ( $\lg(1 - S_{Hg})$ ) and greater than 1 ( $\lg S_{Hg}$ ). In this study, two models are used to obtain the fractal dimension of the high-pressure mercury intrusion capillary pressure to characterize the full pore-throat. The fractal dimension of the sphere can be determined using the double logarithmic curve relationship between  $1 - S_{Hg}$  and  $P_c$ . The fractal dimension of the tube bundle can be determined using the double logarithmic curve relationship between  $S_{Hg}$  and  $P_c$ . The fractal dimension of porous lithology is mostly distributed between 2 and 3. The smaller the fractal dimension value, the more uniform the pore-throat size distribution and the smaller the reservoir heterogeneity. The larger the value, the more disordered the pore-throat size distribution of the reservoir and the greater the heterogeneity of the reservoir.

**Table 1.** Statistical table of formulas of two fractal models.

Models	Formulas
Spherical fractal model	$P_c = \frac{2\sigma \cos\theta}{r} \quad (2)$
	$S_{Hg} = S(> r) = 1 - \frac{r^{3-D}}{r_{min}^{3-D}} \quad (3)$
	$S_{Hg} = \left(\frac{P_{min}}{P_c}\right)^{3-D} \quad (4)$
	$\lg(1 - S_{Hg}) = (D - 3)LgP_c + (D - 3)LgP_{min} \quad (5)$
	$D = 3 + k \quad (6)$
Tube-bundle fractal model	$S_{Hg} = \frac{V_{Hg}}{V_p} \quad (7)$
	$S_{Hg} \propto P_c^{-(2-D_f)} \quad (8)$
	$Lg(S_{Hg}) = (D - 2) \times Lg(P_c) + \alpha \quad (9)$
	$D = 2 + k \quad (10)$

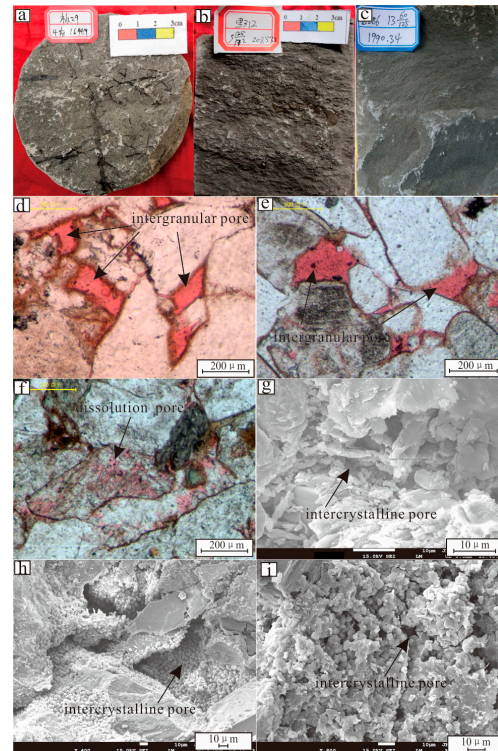
## 4. Results

### 4.1. Petrological Features

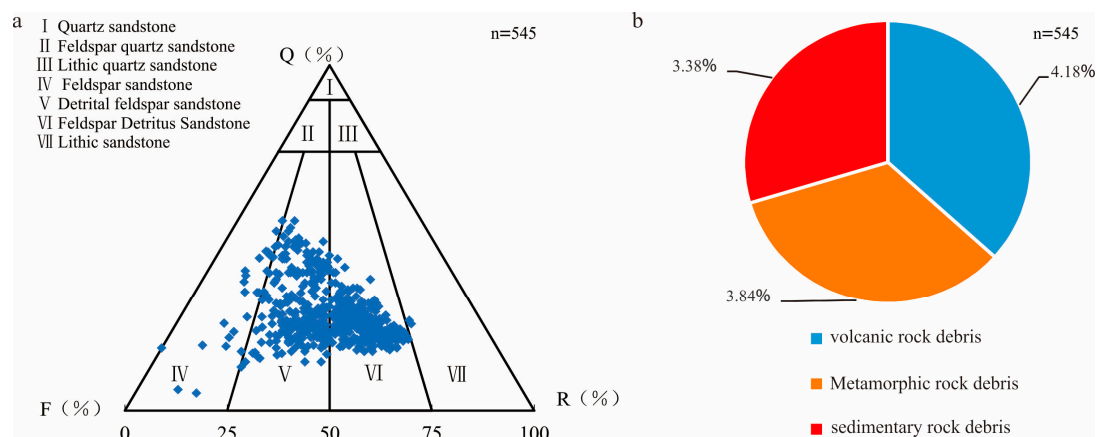
The lithology of the Chang 6 reservoir in the study area is mainly grey-dark grey fine siltstone, and plant debris and stem fossils can be seen in the core (Figure 2a–c). The sedimentary environment comprises a delta and shallow lake. According to the Folk sandstone classification standard, the Chang 6 reservoir sandstone in the study area is mainly composed of feldspar lithic sandstone and lithic feldspar sandstone and a small amount of feldspar sandstone and lithic sandstone (Figure 3). The quartz content is between 5% and 55%, with an average of 27.61%. The feldspar content is between 9.2% and 59%, with an average of 36.72%. The content of debris is between 2% and 34.7%, with an average of 11.41%. Among them, the content of volcanic debris is the highest, with an average of 4.18%, followed by metamorphic debris, with an average of 3.84%, and the content of sedimentary debris is the lowest, with an average of 3.38% (Figure 3), of which carbonate debris is dominant. The mica content is between 1% and 28.3%, with an average of 8.01%. The clay mineral content is between 0.2% and 69%, with an average of 9.31%. The carbonate cement content is between 0.2% and 73%, with an average of 4.86%. The siliceous content



is between 0.2% and 6%, with an average of 1.59% (Table 2). The particles are mainly in point-line contact, the sorting is poor–medium, and the rounding is mainly subangular (Figure 2d–f).



**Figure 2.** Rocks and microscopic characteristics of Chang 6 reservoir in Huaqing area. (a) Grey fine sandstone with obvious calcareous cementation, from Well B29, 1644.9 m, core image; (b) dark grey massive dense fine sandstone, from Well L312, 2085.62 m, core image; (c) grey massive fine sandstone, from Well B286, 1990.34 m, core image; (d) intergranular pores, from Well B136, chang63, 2115.62 m, thin sections image; (e) intergranular pores, from Well B143, chang63, 1951.4 m, thin sections image; (f) development of dissolution pores, from Well B217, chang63, 2214.53 m, thin sections image; (g) development of intercrystalline pores and microcracks, from Well B163, chang63, 2141.41 m, SEM image; (h) intercrystalline pores and microcracks, from Well B143, 1926.79 m, SEM image; (i) intercrystalline pores, from Well B458, 1947.8 m, SEM image.



**Figure 3.** Petrological characteristics of 6 reservoirs in the study area. (Q: quartz, F: feldspar, R: rock detritus). (a) Triangulation of sandstones in the Long 6 reservoir in the study area; (b) Sector map of rock chip content.

**Table 2.** Statistical table of the rock composition of the Chang 6 reservoir in the Huaqing area ( $n = 545$ ).

Rock Composition	Quartz/%	Feldspar/%	Debris/%	Mica/%	Clay Minerals/%	Carbonate Cement/%	Silica/%
Max	55	59	34.7	28.3	69	73	6
Min	5	9.2	2	1	0.2	0.2	0.2
Average	27.61	36.72	11.41	8.01	9.31	4.86	1.59

#### 4.2. Reservoir Characteristics

The pore types of the Chang 6 reservoir in the Huaqing area mainly include intergranular pores, dissolved pores, intercrystalline pores and microfractures, among which intergranular pores and feldspar-dissolved pores are the most developed. The intergranular pore volume is distributed between 0.1% and 6.5%, with an average of 1.32%, accounting for 58.93% of the total pore space. The feldspar-dissolved pores are distributed in the range of 0.1%–3%, with an average of 0.66%, accounting for 29.46% of the total pore space. The intergranular dissolved pores are distributed between 0.2% and 1.5%, with an average of 0.01%, accounting for 0.45% of the total pore space. The distribution of dissolved pores in debris is between 0.1% and 1%, with an average of 0.13%, accounting for 5.8% of the total pore space. The distribution of intercrystalline pores is between 0.1% and 2.3%, with an average of 0.08%, accounting for 3.57% of the total pore space. Microcracks are distributed between 0.1% and 1.8%, with an average of 0.04%, accounting for 1.79% of the total pore space (Table 3).

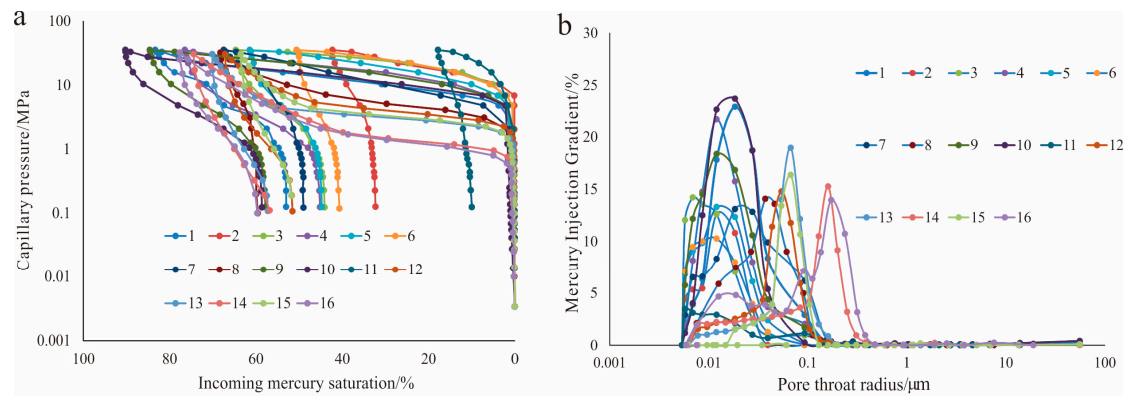
**Table 3.** Statistics of pore types in the Chang 6 reservoir in the Huaqing area ( $n = 128$ ).

Pore Type	Inter P/%	Inter DP/%	FDP/%	DDP/%	Inter CP/%	MC/%
Max	6.5	1.5	3	1	2.3	1.8
Min	0.1	0.2	0.1	0.1	0.1	0.1
Average	1.32	0.01	0.66	0.13	0.08	0.04
Proportion of total pore space/%	58.93%	0.45%	29.46%	5.80%	3.57%	1.79%

Inter P: intergranular pores; Inter DP: intergranular dissolved pores; FDP: feldspar-dissolved pores; DDP: debris-dissolved pores; Inter CP: intercrystalline pores; MC: microcracks.

Analysis of the pore-throat structure and pore-throat radius of Chang 6 reservoir samples in the study area was conducted using mercury intrusion capillary pressure (MICP). The maximum mercury saturation is distributed between 17.79% and 90.22%. The displacement pressure distribution is 0.832–10.782. The mercury removal efficiency is distributed between 13.91 and 44.05. The sample with the maximum mercury saturation is sample 10, and that with the smallest is sample 11, with values of 90.22% and 17.79%, respectively (Figure 4a). However, the peak distribution of the pore-throat radius of the two is basically the same, and both are distributed in the range of 0.008–0.04  $\mu\text{m}$  (Figure 4b). This shows that the maximum mercury saturation does not reflect the distribution of the pore-throat radius in the reservoir but reflects the connectivity and homogeneity between the pore-throats. The greater the maximum mercury saturation, the better the pore-throat connectivity in the reservoir. According to the median pressure, the curves were divided into three categories: greater than 9.17 MPa, including samples 1, 3, 4, 5, 6, 7, 9 and 10; greater than 3.78 MPa and less than 9.17 MPa, including samples 8, 12, 13 and 15; and greater than 0 and less than 3.78 MPa, including samples 14 and 16. The pore-throat radius peaks of these three types of samples are distributed in the ranges of 0.008–0.04  $\mu\text{m}$ , 0.04–0.1  $\mu\text{m}$  and 0.1–0.5  $\mu\text{m}$ , corresponding to three different peaks from small to large in the pore-throat radius distribution diagram. This shows that the median pressure has a good corresponding relationship with the pore-throat radius distribution, and the smaller

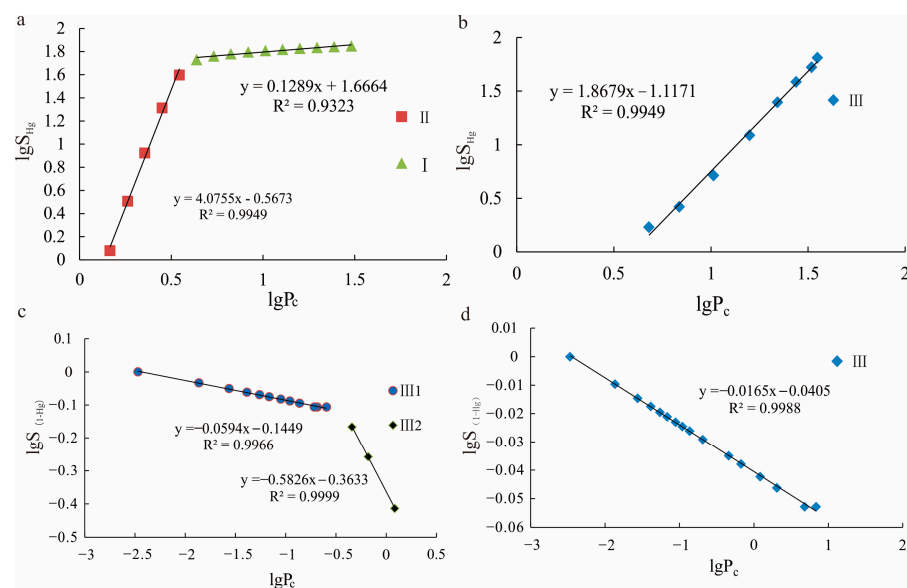
the median pressure, the larger the peak value of the pore-throat radius. The distribution span of each mercury injection parameter in the Chang 6 reservoir is large, indicating that the Chang 6 reservoir in the study area has a diverse pore-throat size distribution, complex pore-throat connectivity, and strong reservoir heterogeneity.



**Figure 4.** Capillary curve characteristics and pore-throat radius distribution of Chang 6 reservoirs in the study area. (a) high pressure mercury piezo tube pressure curve; (b) pore-throat radius distribution curve.

#### 4.3. Fractal Features

It can be seen from the related formulas of the spherical fractal model and the tube-bundle fractal model (Equations (2)–(10)) that the two models should be suitable for mercury injection gradients of less than 1 ( $\lg(1 - S_{Hg})$ ) and greater than 1 ( $\lg S_{Hg}$ ). Rather than choosing one of them to characterize reservoir physical properties and pore structure as previously thought [47,48]. This study adopted the above two fractal models at the same time and used the high-pressure mercury intrusion data of the above 16 samples to study the pore structure of the Chang 6 reservoir in the study area. Taking a mercury input gradient value of 1 as the boundary, the tube-bundle fractal model was used for pore-throats with a mercury input gradient of greater than 1, and the tube-bundle fractal model was used for pore-throats with a mercury input gradient of less than 1. The typical curves of the two models are shown in Figure 5.

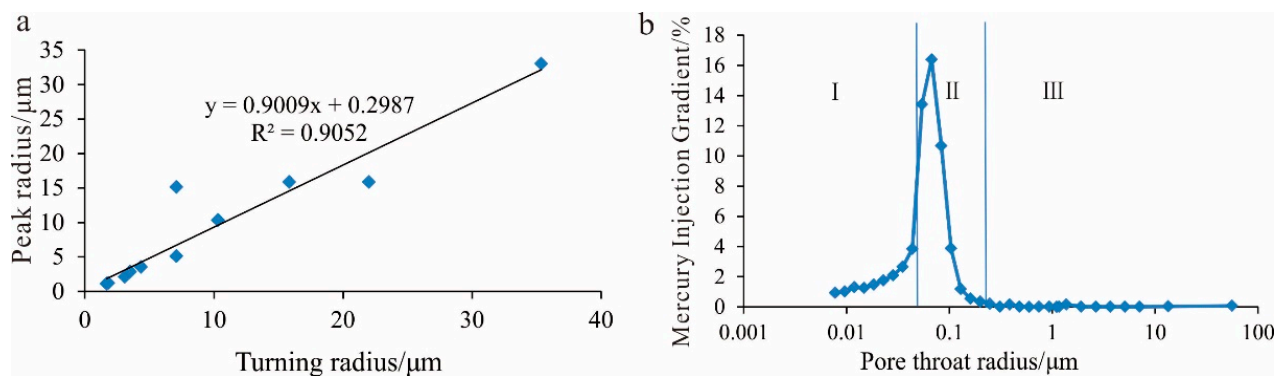


**Figure 5.** Typical curves of tube-bundle and spherical fractal models. (a,b) Typical curve of tube-bundle fractal model; (c,d) typical curve of spherical fractal model.

The tube-bundle fractal model can be divided into two types according to whether there are obvious turning points in the curve. The curves with obvious turning points were divided into two categories: I and II (Figure 5a). Curves without turning points were classified into Class I or Class II according to the size of their fractal dimension and the distribution range of the abscissa and ordinate values of the curve (Figure 5b). The typical curve of the spherical fractal model was also classified into two categories according to the presence or absence of distinct inflection points (Figure 5c,d). For pore-throat samples with two segments in the spherical fractal model, the proportion of the porosity of the two sections and the contribution of each section to the total porosity were calculated separately. Finally, using the weighted average of the porosity of each pore space, the total fractal dimension of the entire pore space was obtained (Formula (11)). In the formula,  $D$  is the average fractal dimension,  $D_1$  and  $D_2$  are the fractal dimensions of the two segments, respectively, and  $\varphi_1$  and  $\varphi_2$  are the proportions of the pore-throats of the two segments.

$$D = \frac{D_1 \times \varphi_1 + D_2 \times \varphi_2}{\varphi_1 + \varphi_2} \quad (11)$$

The correlation between the capillary pressure corresponding to the inflection point of the class I and class II curves and the capillary pressure corresponding to the peak value of the pore-throat radius is relatively good ( $R^2 = 0.9052$ ) (Figure 6a). This shows that the inflection point of the fractal dimension of the tube bundle has good correspondence with the peak value of the pore-throat radius, which can be used as the basis for dividing the pore-throat size. Combined with the boundary between the tube-bundle fractal model and the spherical fractal model, the pore-throats corresponding to the spherical model were classified as class III. Therefore, the pore-throat structure of the reservoir was divided into three categories (Figure 6b). Class I represents smaller pore-throats, class II represents medium pore-throats, and class III represents larger pore-throats.



**Figure 6.** Correlation between inflection point and turning radius of tube-bundle fractal model and pore-throat classification. (a) Correlation of inflection radius corresponding to fractal dimension with pore-throat turning radius; (b) Typical classification curve for pore-throat radius.

The statistics of the three types of pore-throat fractal numbers for the 16 samples are shown in Table 4.  $\lg(1 - S_{Hg})$  and  $\lg(P_c)$ , and  $\lg(S_{Hg})$  and  $\lg(P_c)$  have good correlation. The average  $R^2$  values are 0.9619, 0.9646 and 0.9441, respectively. This shows that the pore-throat structure of the Chang 6 reservoir in the Huaqing area has obvious fractal characteristics.

**Table 4.** Statistics of three types of pore-throat fractal features.

Number	Type I Pore-Throat			Type II Pore-Throat			Type III Pore-Throat		
	FD	R <sup>2</sup>	Porosity	FD	R <sup>2</sup>	Porosity	FD	R <sup>2</sup>	Porosity
1	2.5287	0.9314	1.5826	4.7429	0.9898	1.5826	2.5220	0.9999	2.9674
2	2.8586	0.9995	0.4286	4.6896	0.9809	0.4286	2.9835	0.9988	2.1429
3	/	/	/	3.8679	0.9949	2.2273	2.3789	0.9753	2.3864
4	2.5801	0.9905	0.9364	3.9706	0.9933	2.3409	2.9031	0.9899	7.0227
5	/	/	/	3.3180	0.9291	4.4182	2.4457	0.9687	1.8409
6	/	/	/	3.9485	0.9860	4.1591	2.8793	0.9809	1.9409
7	2.5538	0.9993	1.7739	4.0738	0.9928	1.7739	2.4259	0.9087	3.3261
8	2.2827	0.9391	1.5636	4.9592	0.9997	1.9545	2.3120	0.9782	2.5409
9	2.9477	0.9877	2.7429	4.3918	0.9766	3.6571	2.9562	0.9985	6.4000
10	2.7323	0.9309	2.6909	3.1433	0.7204	7.4000	2.1376	0.8222	4.7091
11	/	/	/	3.1722	0.9902	0.8050	2.5840	0.9997	0.7475
12	2.2052	0.9581	2.6667	6.2220	0.9858	1.6667	3.3559	0.9981	3.3333
13	2.1289	0.9323	2.3344	6.0755	0.9949	1.2969	2.9256	0.9956	4.6688
14	2.1948	0.9760	4.3273	4.4089	0.9467	1.8030	2.7484	0.9996	2.8848
15	2.1414	0.9321	2.3182	5.2803	0.9821	1.5455	2.7426	0.6952	2.3182
16	2.1896	0.9654	5.2826	4.0901	0.9707	2.9348	2.3993	0.7963	2.6413
max	2.9477	0.9995	5.2826	6.2220	0.9997	7.4000	3.3559	0.9999	7.0227
min	2.1289	0.9309	0.4286	3.1433	0.7204	0.4286	2.1376	0.6952	0.7475
average	2.4453	0.9619	2.3873	4.3972	0.9646	2.4996	2.6688	0.9441	3.2419

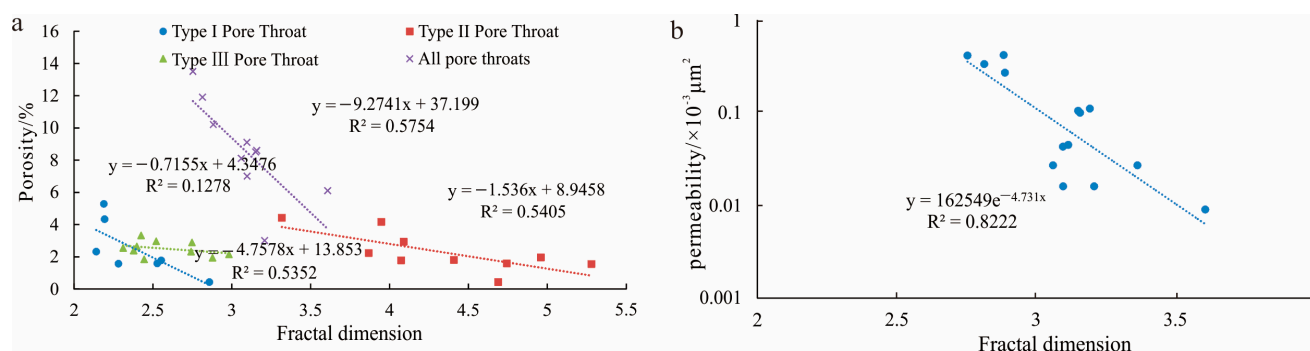
FD: fractal dimension.

The fractal dimension of class I pores and throats is distributed in the range of 2.1289 to 2.9477, with an average of 2.4453. The contribution to porosity is distributed in the range of 0.4286~5.2826, with an average of 2.3873. The fractal dimension of class II pore-throats is distributed in the range of 3.1433 to 6.222, with an average of 4.3972. The contribution to porosity is distributed in the range of 0.4286 to 7.4, with an average of 2.4996. The fractal dimension of class III pore-throats is distributed in the range of 2.1376 to 3.3559, with an average of 2.6688. The contribution to porosity ranges from 0.7475 to 7.0227, with an average of 3.2419. The type I pore-throat fractal dimension is the smallest, and the type II pore-throat fractal dimension is the largest. The heterogeneity of small pore-throats is weaker than that of large pore-throats, and the heterogeneity of medium pore-throats is the strongest. Type III pore-throats contribute the most to reservoir porosity, followed by type II pore-throats, and type I pore-throats contribute the least. In tight sandstone reservoirs, the major influences on porosity are large and medium pore-throats.

#### 4.4. Relationships between Fractal Features and Reservoir Physical Properties

In addition to characterizing the uniformity of pore-throats in the reservoir, the fractal dimension can also characterize the roughness of the particle surface. The roughness of the particle surface affects the migration and accumulation of oil and gas in the reservoir. These effects will manifest in the porosity and permeability of the reservoir. Therefore, studying the correlation between the fractal dimension and porosity and permeability is of great significance to clarify the contribution of various pore-throats to porosity and permeability. The relationships between the fractal dimensions of types I, II and III and the total fractal dimension and their corresponding porosities are negatively correlated (Figure 7a). The R<sup>2</sup> values are 0.5352, 0.5405, 0.1278 and 0.5754, respectively. There is an obvious negative correlation between the total fractal dimension and the total permeability, with an R<sup>2</sup> of 0.8222 (Figure 7b). The smaller the fractal dimension, the greater the porosity and permeability, the smaller the difference between the pore and throat radii in the reservoir, the better the average distribution of the pore-throats and the better the permeability. The larger the fractal dimension, the rougher the particle surface and the larger the difference between the pore and throat radii, which is not conducive to the migration and accumulation of oil and gas.





**Figure 7.** Correlation between fractal dimension and porosity. (a) Correlation between fractal dimension and porosity of pore throats without using types of pores; (b) Fractal dimension and permeability correlation.

#### 4.5. Pore-Throat Distribution Characteristics

Many studies have been performed on the distribution of pore-throat radii in tight sandstone reservoirs, and it is believed that the pore-throat radius is mainly distributed between 0.01 and 0.2  $\mu\text{m}$  [49,50]. Through the classification of pore-throat radii by fractal dimension, combined with the high-pressure mercury injection experiment, the percentage of different types of pore-throat radius volume in the total pore-throat volume was calculated (Table 5). The results show that the main types of pore-throats in the Chang 6 reservoir in the study area are nanoscale pore-throats, and microscale pore-throats are less developed (Figure 8). Among them, macropores ( $>200$  nm) account for 1.4% of the total pore-throat volume, mesopores (54–200 nm) account for 5.1% of the total pore volume, and micropores ( $<54$  nm) account for 93.5% of the total pore volume. Small pores with pore-throat radii of  $<54$  nm are the main storage space of tight sandstone reservoirs.

**Table 5.** Statistical table of the volume of various pore-throats in the total pore-throat volume.

Sample Number	Macropores	Mesopores	Micropores	Sample Number	Macropores	Mesopores	Micropores
1	6.5%	3.7%	89.8%	9	0.1%	0.1%	99.7%
2	0.4%	0.1%	99.5%	10	2.5%	0.7%	96.9%
3	0.7%	0.6%	98.6%	11	1.0%	1.1%	97.9%
4	1.0%	0.3%	98.7%	12	0.3%	5.5%	94.2%
5	3.9%	1.1%	95.1%	13	0.5%	10.3%	89.2%
6	2.0%	0.6%	97.4%	14	0.7%	24.1%	75.2%
7	0.4%	0.5%	99.1%	15	0.6%	4.8%	94.6%
8	0.7%	3.3%	96.0%	16	1.6%	24.5%	73.8%
Average	1.4%	5.1%	93.5%				

#### 4.6. Effects of Different Types of Pore-Throats on Reservoirs

The sorting coefficient is a parameter that reflects the concentration of pore-throat distribution in the reservoir. The smaller the sorting coefficient, the more uniform the pore-throat distribution. Among the three types of pore-throats in the Chang 6 reservoir in the study area, only type II pore-throats have an obvious negative correlation with the sorting coefficient ( $R^2 = 0.6049$ ). The correlation between type I and type III pore-throats and the sorting coefficient is not obvious, and the  $R^2$  values are 0.0073 and 0.0434, respectively (Figure 9a). This shows that the concentration degree of medium pore-throats in tight sandstone reservoirs is closely related to the fractal dimension. The larger the fractal dimension of the medium pore-throat, the more uniform the pore-throat distribution.



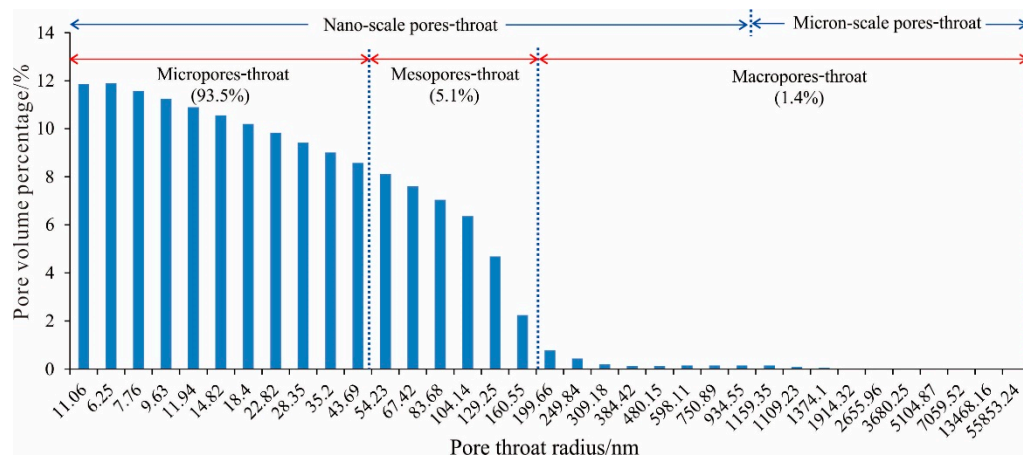


Figure 8. Distribution of various pore-throat volumes in total pore volume.

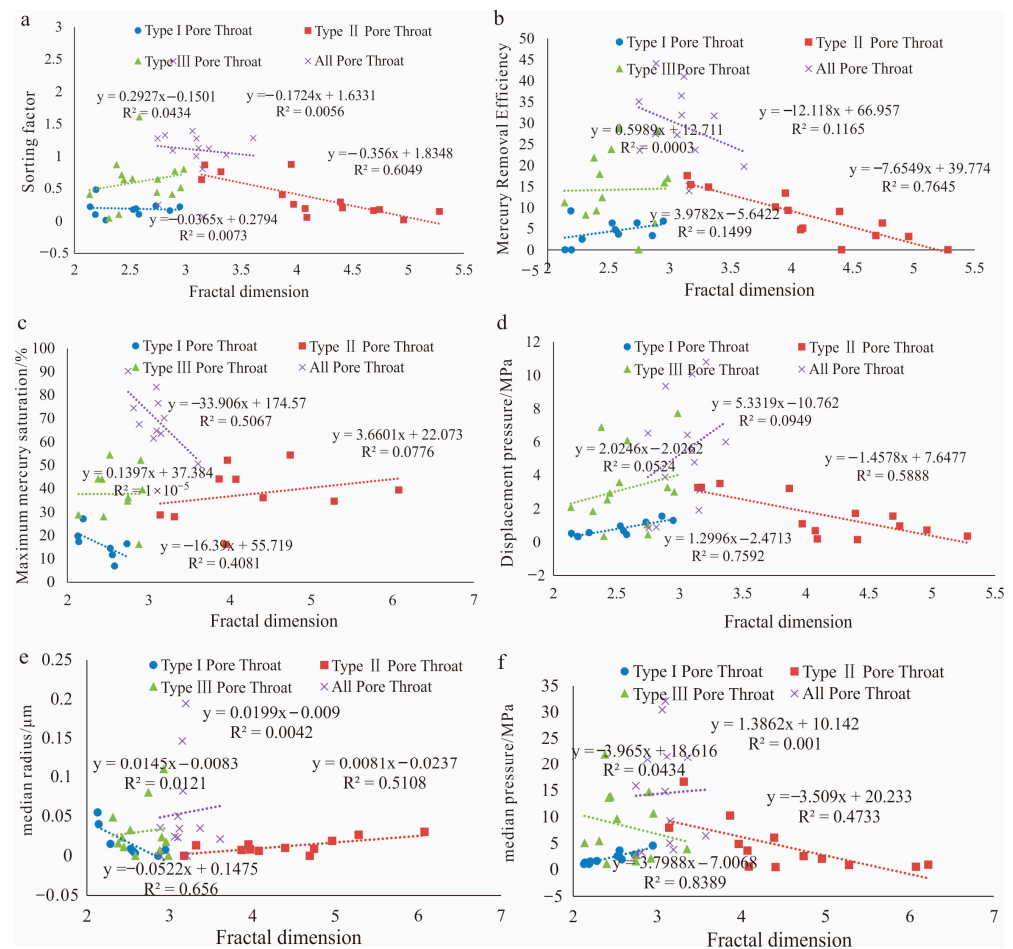


Figure 9. Correlation between fractal dimensions of different types of pore-throats and mercury intrusion parameters. (a) Correlation of fractal dimensions and sorting coefficients for different types of pore-throats; (b) Correlation between the fractal dimension of different types of pore-throats and mercury removal efficiency; (c) Correlation between fractal dimensions and maximum mercury saturation for different types of pore-throats; (d) Correlation of fractal dimensions of different types of pore-throats with displacement pressures; (e) Correlation between fractal dimension and median radius for different types of pore-throats; (f) Correlation between fractal dimension and median pressure for different types of pore-throats.

The mercury removal efficiency can reflect the uniformity of pore and channel size in the reservoir. The greater the mercury removal efficiency, the more uniform the size of the pores and throats. The fractal dimension of type II pore-throats is significantly negatively correlated with mercury removal efficiency ( $R^2 = 0.7645$ ). There is no obvious correlation between the fractal dimensions of the pore-throats of type I and type III and the mercury removal efficiency, with  $R^2$  values of 0.1499 and 0.0003, respectively (Figure 9b). This shows that the uniformity of the pore-throats in the reservoir is mainly controlled by the medium pore-throats. The more uniform the distribution of medium pore-throats, the more uniform the distribution of pore-throats in the reservoir.

The fractal dimension of type I pore-throats is significantly negatively correlated with the maximum mercury saturation ( $R^2 = 0.4081$ ). There is no significant correlation between the fractal dimensions of type II and type III pore-throats and the maximum mercury saturation, and the  $R^2$  values are 0.0776 and 0.00005, respectively (Figure 9c). It is shown that the smaller pore-throats with the upper limit of oil and gas content in the reservoir, the more uniform the distribution of the smaller pore-throats, and the greater the potential for oil and gas accumulation in the reservoir.

The displacement pressure refers to the minimum pressure at which mercury enters the rock sample. Type I pore-throats are significantly positively correlated with displacement pressure ( $R^2 = 0.7592$ ). Type II pore-throats are significantly negatively correlated with displacement pressure ( $R^2 = 0.5888$ ). There is no obvious correlation between the type III pore-throat and the displacement pressure ( $R^2 = 0.052$ ) (Figure 9d). This shows that in the type I pore-throats, the displacement pressure gradually increases with the deterioration of the uniformity of the pore-throats. In type II pore-throats, the displacement pressure gradually decreases as the uniformity of the pore-throats deteriorates. The homogeneity of type III pore-throats has no significant effect on the displacement pressure.

The median radius can approximately represent the average pore-throat radius. The fractal dimension of class I pore-throats is significantly negatively correlated with the median radius ( $R^2 = 0.656$ ). The fractal dimension of class II pore-throats is positively correlated with the median radius ( $R^2 = 0.5108$ ). The fractal dimension of class II pore-throats is positively correlated with the median radius ( $R^2 = 0.5108$ ) (Figure 9e). This shows that in the type I pore-throat, with the decrease in pore-throat uniformity, the average pore-throat radius decreases. In type II pore-throats, the average pore-throat radius gradually increases as the pore-throat uniformity decreases. Type III pore-throats have no significant effect on the average pore-throat radius.

The smaller the median pressure, the better the permeability of the rock. The fractal dimension of the type I pore-throat is significantly positively correlated with the median pressure ( $R^2 = 0.8389$ ). Type II pore-throats are significantly negatively correlated with the median pressure ( $R^2 = 0.4733$ ). There is no significant correlation between class III pore-throats and median pressure ( $R^2 = 0.043$ ) (Figure 9e,f). This shows that the more uniform the pore-throats in the type I pore-throats, the better the rock infiltration performance. In type II pore-throats, the worse the pore-throat uniformity, the better the rock percolation. Type III pore-throats have no significant effect on rock percolation.

It can be seen from the abovementioned analysis that the effects of the three types of pore-throats on the displacement pressure, median pressure and median radius show diametrically opposite results, indicating that the effects of different pore-throat radii on the reservoir are different.

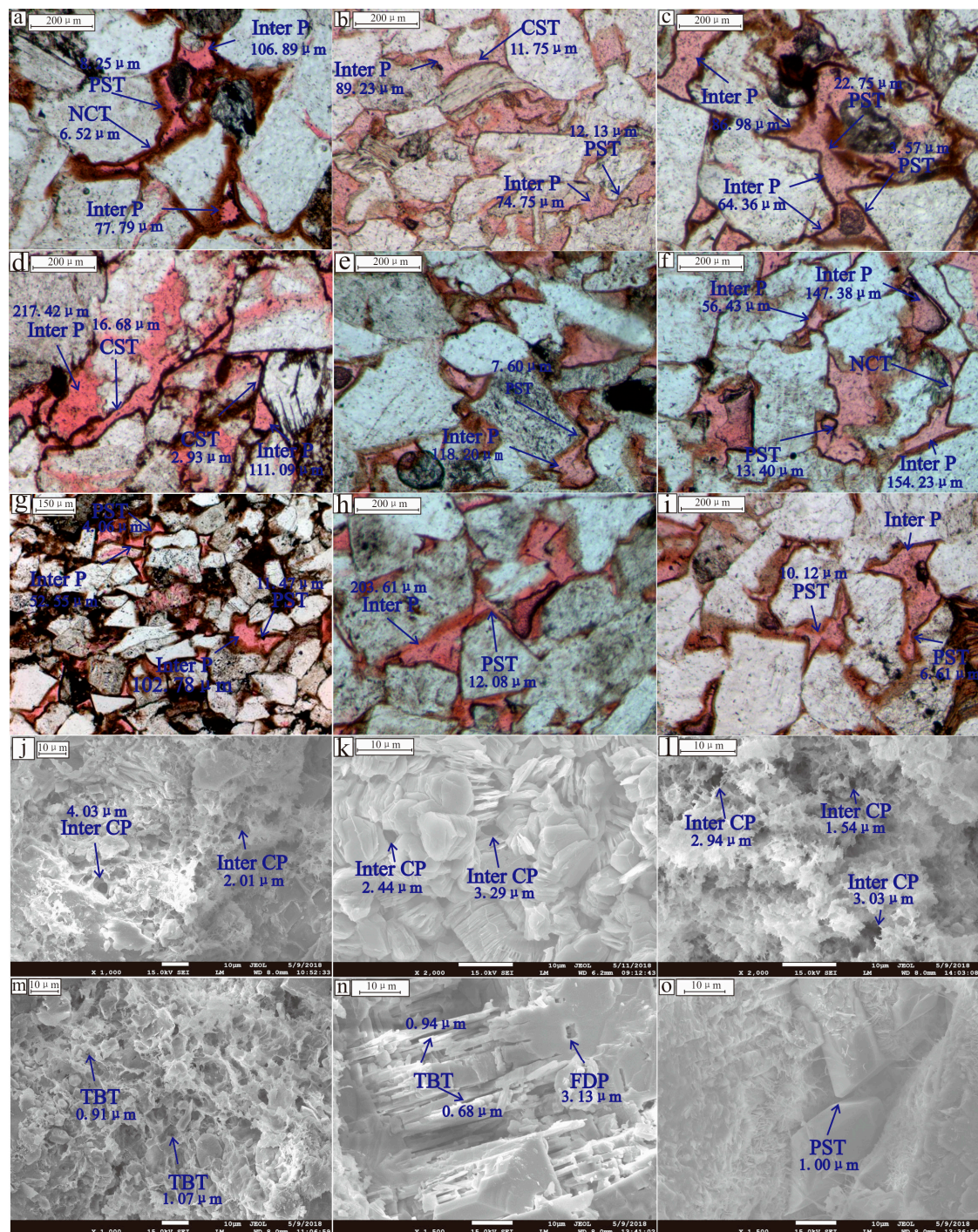
## 5. Discussion

### 5.1. The Features of Pore-Throats

The factors affecting the uniformity of different types of pore-throats are mainly the pore-throat size and the combination relationship between pores and throats [51–55]. The pore radius of intergranular pores (inter P) in the Chang 6 tight sandstone reservoir in the study area is generally distributed in the range of 5.5–210  $\mu\text{m}$  (Figure 10a,b,g,f). The radius of the feldspar dissolution pores (FDP) is generally in the range of 3.1–146  $\mu\text{m}$

(Figure 10n). The radius of intercrystalline pores (inter CP) is generally developed in the range of 3.1~146  $\mu\text{m}$  (Figure 10j,k,l). The pore-shrinking throats (PSTs), slice-shaped throats (SSTs) and curved sheet throats (CSTs) generally have a radius greater than 2  $\mu\text{m}$ , and the maximum can reach more than 10  $\mu\text{m}$  (Figure 10c,e,f). The radii of neck-contracted throats (NCTs) and tube-bundle throats (TBTs) are generally less than 1  $\mu\text{m}$  (Figure 10 m,n) (Table 6).



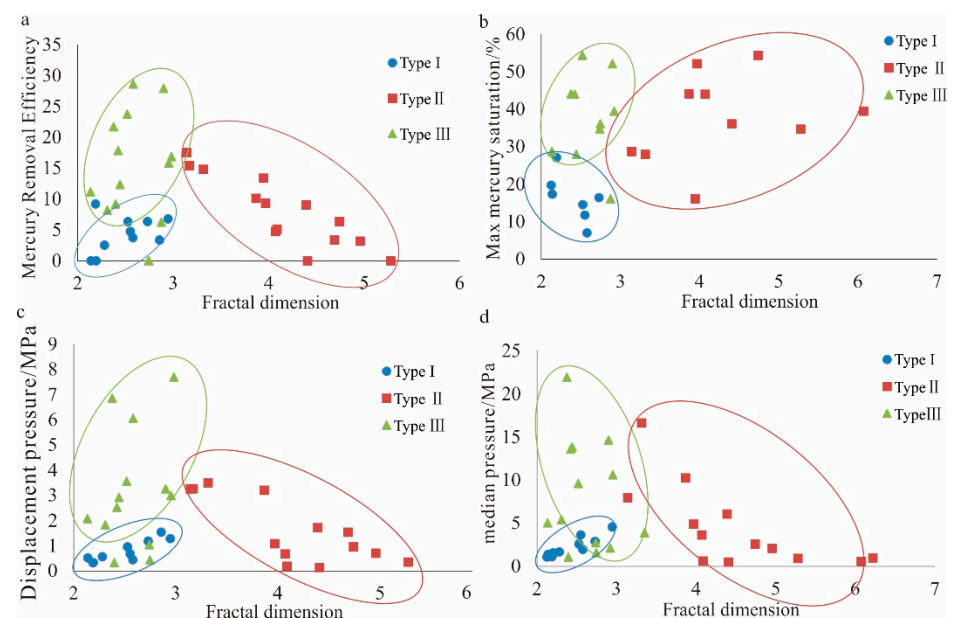


**Figure 10.** Sizes and types of pores and throats in Chang 6 reservoirs in the study area. (a) Well B266, 1984.7 m, thin sections image; (b) Well B156, 2066.42 m, thin sections image; (c) Well B156, 1938.32 m, thin sections image; (d) Well B196, 1894.58 m, thin sections image; (e) Well W51, 1951.04 m, thin sections image; (f) Well B212, 2075.87 m, thin sections image; (g) Well B142, 1982.9 m, thin sections image; (h) Well B143, 1927.5 m, thin sections image; (i) Well B304, 2078.5 m, thin sections image; (j) Well B401, 1947.3 m, SEM image; (k) Well B418, 1874.5 m, SEM image; (l) Well B487, 1857.1 m, SEM image; (m) Well B135, 2016.8 m, SEM image; (n) Well B153, 2191.75 m, SEM image; (o) Well B163, 2116.44 m, SEM image. Inter P: intergranular pore; Inter CP: intercrystalline pore; FDP: feldspar dissolution pore; TBT: tube-bundle throat; PST: pore-shrinking throat; NCT: neck-contracted throat; SST: slice-shaped throat; CST: curved sheet throat.

**Table 6.** Distribution of pore radius and throat radius.

Type of Pore-Throat	Main Pore Type	Main Throat Type	Pore Radius Distribution/ $\mu\text{m}$	Throat Radius Distribution/ $\mu\text{m}$
Type I	Inter CP, FDP	TBT	0.025~2	0.1~0.5
Type II	Inter P	NCT	3.1~146	0.3~3.5
Type III	Inter P	SST, CST	5.5~210	0.2~1.3

From the distribution of the fractal dimensions of different types of pore-throats (Figures 10 and 11), it can be seen that the fractal dimensions of type I and type III pore-throats are generally lower. The fractal dimension of class II pore-throats is generally larger. The distribution of type I and type III pore-throats is relatively uniform, and the differences between the pore and throat radii of type II pore-throats is large. Combined with the distribution of the pore-throat radius, it is considered that type I pore-throats are mainly composed of small pores equipped with small throats, type III pore-throats are mainly composed of large pores equipped with large throats, and type II pore-throats are mainly composed of large pores equipped with small throats.



**Figure 11.** Distribution of different types of pore-throat high-pressure parameters. (a). Distribution of mercury removal efficiency for different types of pore-throats fractal dimensions; (b). Distribution of fractal dimensions and maximum mercury saturation for different types of pore-throats; (c). Distribution of fractal dimensions and displacement pressure of different types of pore-throats; (d). Distribution of fractal dimension and median pressure for different types of pore-throats.

Intergranular pores (inter P), pore-shrinking throats (PSTs), slice-shaped throats (SSTs) and curved sheet throats (CSTs) are mainly developed in type III reservoirs. The pore-throat combination modes are mainly inter P—PST, inter P—SST, and CST (Figure 10b,c,e). They are mainly composed of large pores with large throats and strong pore-throat connectivity, which is conducive to oil and gas migration and accumulation. Type II pore-throats are mainly composed of residual primary intergranular pores and necked throats. Type II pore-throats are mainly composed of inter P—NCT (Figure 10f). The radius of the NCT is small, and oil and gas are easily blocked by it during the migration process. The connectivity between the two pores connected by it is poor, and no effective connection can be generated, which is not conducive to oil and gas migration and accumulation. Type I pore-throats are mainly composed of inter CP—TBT (Figure 10j,k,l) and FDP—TBT (Figure 10n) and are equipped with small throats for small pores. In general, from the perspective of pore-throat



combinations, the reservoir connectivity corresponding to type III pore-throats is the best, that of type I reservoirs is poor, and that of type II reservoirs is the worst.

#### 5.1.1. The Distribution of Mercury Intrusion Parameters

There are obvious differences in the distribution of mercury removal efficiency, maximum mercury injection saturation, displacement pressure and median pressure corresponding to different pore-throat types (Figure 11). The reason for this difference is mainly the size difference in various pores and throats and their combined relationships.

The pores in type I pore-throats are mainly inter CP of clay minerals and FDP with a small radius. The throats are mainly TBT in clay minerals and feldspar-dissolved pores. The pore and throat radii are generally small, and the gap is not large. Therefore, the distribution of the fractal dimension and mercury intrusion parameters is relatively concentrated, and a larger displacement pressure is generated by overcoming the smaller throat size.

The pore types in type II are mainly inter P, and the throats are mainly NCT produced via compaction. The pore radius is large, the distribution range is wide, the throat radius is small and the gap between the pore radius and the throat radius is large (Figure 10). The combination of pore-throats with different sizes determines that this type of pore-throat has a larger fractal dimension. The mercury removal efficiency and the maximum mercury saturation vary widely.

The pore types in type III pore-throats are mainly inter P with larger pore diameters, and the throat types only include PST, SST and CST. Type III pore-throats are mainly large pores with large throats. Therefore, the fractal dimension is smaller, and the mercury removal efficiency and maximum diameter mercury saturation are higher than those of type I pore-throats.

#### 5.1.2. Analysis of the Reasons for the Difference

The sorting coefficient and mercury removal efficiency can reflect the uniformity of pore-throats in the reservoir. Only the fractal dimension of type II pore-throats has a significant correlation with the sorting coefficient and mercury removal efficiency (Figure 11a,b). This indicates that pore-throats with large radius differences are mainly developed in the reservoirs corresponding to type II pore-throats.

The fractal dimension of type I pore-throats is significantly negatively correlated with the maximum mercury saturation, while the fractal dimensions of type II and III pore-throats have no significant correlation with it (Figure 11c). This shows that the pores with small radii have a controlling effect on the amount of mercury input. This shows that the content and connectivity of small pores in the reservoir also affect the oil saturation.

The fractal dimensions of type I pore-throats and type II pore-throats are significantly positively correlated with displacement pressure, while the fractal dimension of type III pore-throats has no significant correlation with displacement pressure and median pressure (Figure 11d,e). This shows that the minimum pressure affecting the entry of mercury into the rock sample is determined by tube-bundle throats and necked throats with small throat radii.

### 5.2. Different Factors of Pore-Throat Homogeneity

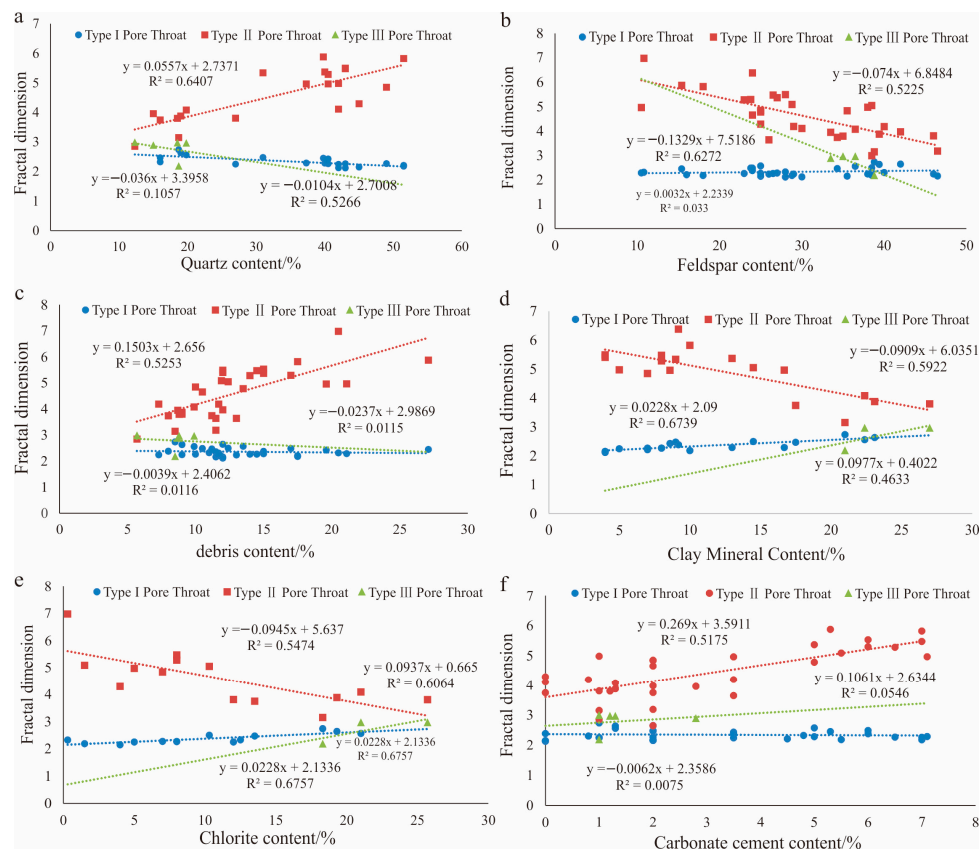
On the basis of using fractal dimensions to study the pore-throat structure of reservoirs based on various experimental methods, predecessors believe that the main factors causing the differences in the properties of various pore-throats are sedimentation [56,57], diagenesis [58–60], rock composition and pore-throat structure.

#### 5.2.1. The Influence of Rock Composition

The fractal dimension of type I pore-throats has an obvious negative correlation with the quartz content ( $R^2 = 0.5266$ ). The fractal dimension of type II pore-throats has an obvious positive correlation with the quartz content ( $R^2 = 0.6407$ ). There is no obvious correlation between type III reservoirs and quartz ( $R^2 = 0.1057$ ) (Figure 12a). The fractal



dimensions of type II and III pore-throats and feldspar content have obvious negative correlations, with  $R^2$  values of 0.5225 and 0.6272, respectively. There is no obvious correlation between the fractal dimension of class I pore-throats and feldspar ( $R^2 = 0.033$ ) (Figure 12b). The fractal dimension of type II pore-throats have a significant positive correlation with the debris content ( $R^2 = 0.5253$ ). There is no obvious correlation between the fractal dimension of type I and type III pore-throats and the content of debris, and the  $R^2$  values are 0.0116 and 0.0115, respectively (Figure 12c). The three types of pore-throat fractal dimensions have good correlations with clay minerals and chlorite. The fractal dimension of class I pore-throats is significantly positively correlated with clay minerals and chlorite, with  $R^2$  values of 0.6739 and 0.6757, respectively. The fractal dimension of type II pore-throats is significantly negatively correlated with clay minerals and chlorite, with  $R^2$  values of 0.5922 and 0.5474, respectively. The fractal dimension of type III pore-throats is significantly positively correlated with clay minerals and chlorite, with  $R^2$  values of 0.4633 and 0.6757, respectively (Figure 12d,e). There is a good positive correlation between the fractal dimension of the type II pore-throat and the carbonate cement content ( $R^2 = 0.5175$ ). There is no obvious correlation between type I and type III pore-throats and carbonate cements, and the  $R^2$  values are 0.0075 and 0.0546, respectively (Figure 12f).

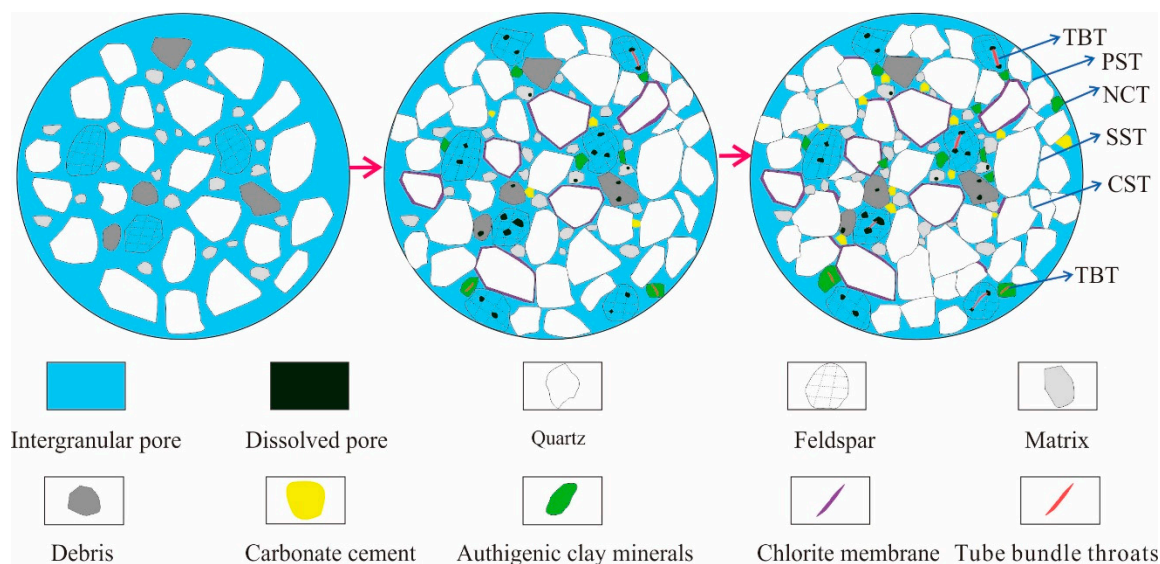


**Figure 12.** Relationships between fractal dimensions of various pore-throats and rock composition. (a) Correlation between fractal dimension and quartz content of different types of pore-throats; (b) Correlation between fractal dimension and feldspar content of different types of pore-throats; (c) Correlation between fractal dimension and rock chip content of different types of pore-throats; (d) Correlation between fractal dimension and clay mineral content of different types of pore-throats; (e) Correlation between fractal dimension and chlorite content in different types of pore-throats; (f) Correlation between fractal dimension of different types of pore-throats and carbonate cement content.

In conclusion, quartz has a positive effect on the homogeneity of smaller pore-throats, and clay minerals have a destructive effect on the homogeneity of smaller pore-throats. Quartz and carbonate cements are not conducive to the preservation of the homogeneity of medium pore-throats, while feldspar, clay minerals and chlorite have positive significance for the preservation of the homogeneity of medium pore-throats. Feldspar has a positive effect on the homogeneity of larger pore-throats, and clay minerals and chlorite have a destructive effect on the homogeneity of larger pore-throats. Therefore, the fractal dimension can be used to evaluate the effect of rock composition on the uniformity of various pore-throats in the reservoir.

### 5.2.2. The Influence of Diagenesis

Previous researchers have performed much research on the effect of diagenesis on the pore-throats of reservoirs [56,59–61]. It is generally believed that compaction will cause the reservoir porosity loss rate of tight sandstone reservoirs in the study area to reach approximately 30%~50% [62–64]. Compaction reduces the content of primary intergranular pores in the reservoir, making point–line, concave–convex contact between particles. The throats produced via compaction mainly include PST, NCT, SST and CST (Figure 13). Cementation is another important factor for porosity reduction in reservoirs [62,63], resulting in a large amount of pore space being filled with cement. The resulting throat is mainly NCT. Dissolution is a rare diagenesis in reservoirs that can increase the storage space [65,66]. Dissolution pores produced via dissolution are mainly connected by TBT [56,67]. The pore types in Class I reservoirs are mainly inter CP and FDP, and throats are mainly TBT, which are greatly affected by dissolution and less affected by compaction. The pore types in Type II and Type III reservoirs are mainly inter P and FDP, and the throats are mainly PST, SST, CST and NCT. The transformation of storage space is more obvious.



**Figure 13.** Model diagram of pore-throat combination mode under the influence of diagenesis. PST: pore-shrinking throats; SST: slice-shaped throats; CST: curved sheet throats; TBT: tube-bundle throat; NCT: neck-contracted throats.

In conclusion, the factors affecting the mercury injection parameters of various pore-throats in the Chang 6 tight sandstone reservoir in the study area are the pore-throat radius and the combination of pores and throats of different sizes. The factors that cause the difference in pore-throat properties mainly include rock composition and diagenesis.

## 6. Conclusions

Based on high-pressure mercury intrusion data, combined with cast thin sections and scanning electron microscopy, this study also uses the tube-bundle model and spherical model to study the fractal dimensions of pore-throat structures in tight sandstone reservoirs and classify pore-throats. The influencing factors of pore-throat differences are discussed, and the following main conclusions are drawn.

1. We divide the pore-throat structure of tight sandstone reservoirs into three categories. Types I, II and III represent small, medium and large pore-throats, respectively. The fractal dimension of type I pore-throats is distributed in the range of 2.1289~2.9477, with an average of 2.4453, and these pore-throats have the best uniformity. The fractal dimension of type II pore-throats is distributed in the range of 3.1433 to 6.222, with an average of 4.3972, and their pore-throat homogeneity is the worst. The fractal dimension of type III pore-throats is distributed in the range of 2.1376 to 3.3559, with an average of 2.6688, and the uniformity of these pore-throats is moderate.
2. Type I pore-throats are mainly tube-bundle throats with intercrystalline pores and dissolution pores and small throat with small pores. Type II pore-throats are mainly necked throats with residual primary intergranular pores and small throats with large pores. Type III pore-throats are mainly composed of pore-reduced throats, lamellar and curved lamellar throats with residual primary intergranular pores, and large throats with large pores.
3. Different types of pore-throats have different responses to high-pressure mercury intrusion parameters in the reservoir, mainly due to the differences in the sizes of various types of pores and throats and their combinations. Type III pore-throats are the most favourable for hydrocarbon migration, followed by type I pore-throats, and the migration ability of oil and gas in type II pore-throats is the worst.
4. Diagenesis, rock composition and pore-throat collocation are the reasons for the differences in the fractal dimensions of different types of pore-throats. Diagenesis and rock composition jointly affect the combination of different types of pore-throats, which is reflected in the differences in the characteristics of the high-pressure mercury intrusion parameters between different types of pore-throats.

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