

Technical Note



The Effect of Salinity on N₂O Emissions during Domestic Wastewater Partial Nitrification Treatment in a Sequencing Batch Reactor

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Abstract: Previous studies have highlighted the salinization caused by the use of seawater to flush toilets and industrial wastewater entering the urban wastewater systems in coastal areas. Thus, in this study, the effect of salinity on N₂O emissions during the partial nitrification process, as well as the emission mechanism, was investigated using a partial nitrification system of wastewater as the research object. The results showed that (1) the increase in salinity decreased the oxidation rate of NH₄⁺ and the formation rate of NO₂⁻ during partial nitrification; (2) the increase in salinity increased the N₂O emissions during NH₄⁺ oxidation and NH₂OH oxidation and decreased the formation rate of NO₂⁻ -N during hydroxylamine oxidation; (3) the total N₂O emissions during hydroxylamine oxidation, and a greater amount of NO₂⁻ was reduced to N₂ instead of N₂O during hydroxylamine oxidation; and (4) a novel finding was that, during partial nitrification with the available organic matter, the N₂O emissions via heterotrophic denitrification by heterotrophic bacteria should not be ignored, and the increase in salinity can increase the N₂O emissions generated via heterotrophic denitrification. These results would provide a theoretical basis for reducing the N₂O emissions in the wastewater treatment process.

Keywords: N₂O; domestic wastewater; partial nitrification; mechanism; greenhouse gas reduction

1. Introduction

Recent years have witnessed rapid economic development in the coastal areas of China, with an increased population density and greater demand for fresh water, along with a severe shortage of water. Thus, seawater utilization is considered as critical to alleviating the shortage of freshwater resources in coastal areas. Seawater flushing [1], as an important means of seawater utilization, has been paid more and more attention; however, the resultant salt-containing wastewater treatment needs more focus for urban wastewater treatment. In addition, this high-salt industrial wastewater has been shown to enter the municipal wastewater network due to its non-standard discharge, resulting in a change in the salinity of municipal wastewater, along with an increase in the salt load of the wastewater plant. This increase in salinity has the potential to affect the nitrogen removal efficiency of biological wastewater treatment, because salinity can cause changes in the metabolic enzymes and cell structure in microorganisms [2,3].

Currently, the studies on the influence of salinity on the wastewater treatment process at home and abroad have mostly been limited to the analysis of the influence of salinity on the traditional nitrification and denitrification of wastewater. In addition, the studies investigating the influence of salinity on the changes in nitrogen and phosphorus contents in the wastewater treatment process have mainly been focused on evaluating its impact on N₂O production and rarely on its mechanism in the nitrification and denitrification process.



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). N_2O is a super greenhouse gas, with a greenhouse effect of 300 times that of CO_2 [4]; it is also associated with the occurrence of the ozone hole [5]. N_2O can be produced in both the nitrification and denitrification processes of wastewater biological treatment. Currently, there are many studies on the influence of salinity on N_2O in the denitrification process, but there is a scarcity of research on the influence of salinity on N_2O in the nitrification process and its mechanism.

In the nitrification process of wastewater biological treatment, N₂O is produced mainly during the oxidation of NH₃ by Ammonia-Oxidizing Bacteria (AOB) to NO₂⁻ [5,6]. In this process, there are three possible production paths: (1) N₂O is the byproduct of the incomplete oxidation of hydroxylamine in the oxidation process [7–10]; (2) N₂O is the product of the autotrophic denitrification of AOB using NO₂⁻ as an electron acceptor [8,11]; and (3) the chemical reaction of NH₂OH with NO₂⁻ or O₂ can also produce partial N₂O [12,13]. Additionally, similar to the denitrification process, N₂O might also be produced during nitrification due to the denitrification of heterotrophic bacteria [14]. However, there have been no studies documenting the influence of salinity on the N₂O produced by heterotrophic denitrification.

Partial nitrification is a novel process for wastewater treatment in practical engineering. Compared to whole-process nitrification, the partial biological nitrogen removal process offers several advantages, such as reducing oxygen supply by 25%, saving carbon sources by 40%, reducing sludge production by approximately 50%, shortening the reaction time, and reducing the reactor volume [15]. However, in the partial nitrification process of the AOB enrichment system, the yield of N₂O is higher than that of the whole-process nitrification system because the end product of NH₃ oxidation is NO₂⁻ rather than NO₃⁻, and because NO₂⁻ is a receptor for autotrophic denitrification and reacts with NH₂OH [16]. This study investigated the effect and mechanism of salinity on the N₂O production in short-cut nitrification system sludge enriched with AOB. The results would provide a theoretical basis for the reduced emissions of N₂O in the wastewater treatment process under the background of "carbon neutrality".

2. Methods

2.1. Sludge, Wastewater, and SBR (Sequencing Batch Reactor) Operations

A 12 L SBR was used for cultivating the partial nitrification sludge. Table 1 shows the index of domestic wastewater inflow. The partial nitrification operation mode was as follows: the average operational cycle (420 min), including feeding (30 min), aeration (240 min), anoxic denitrification (120 min), and settling (30 min), three cycles per day, with the DO at 1 mg/L and Mixed Liquid Suspended Solids (MLSS) at 3000 mg/L. The Sludge Retention Time (SRT) was 11 days, and the running temperature was 30 °C. The effluent's composition consisted of NH₄⁺-N, NO₂⁻-N, and NO₃⁻-N, which were all <1 mg/L. The sludge taken from the SBR was aerated for 12 h, followed by repeated washing. The effluent's COD was less than 50 mg/L and could not be oxidized further.

	COD (mg/L)	NH4 ⁺ -N (mg/L)	NO ₂ N (mg/L)	NO ₃ ⁻ -N (mg/L)	TN (mg/L)	pН	Alkalinity
Minimum	88	39.6	0	0	56.4	6.9	262
Maximum	276	91.2	2.8	1.2	98.5	7.7	343
Average	182	65.4	1.4	0.6	77.4	7.3	303

Table 1. The quality of real domestic wastewater.

2.2. Batch Test Rules

Figure 1 shows the experimental batch test reactor. The effective volume of the reactor was 3 L. At the beginning of each batch test, 1 L of concentrated sludge was added into the reactor, followed by 2 L of wastewater, and the Mixed Liquor Suspended Solids (MLSS) was controlled at 3000 mg/L. The nitrogen compounds, DO, and pH levels were then adjusted



for the batch set upon commencing the operation (Table 2). The running time for the batch tests was 180 min.

Figure 1. Schematic diagram of batch-mode SBR system.

Batch Test Number	Salinity (mg/L NaCl)	Sludge-Water Mixture Type	Initial pH	ATU (mg/L)	NH4 ⁺ -N (mg/L)	NH ₂ OH-N (mg/L)	NO ₂ ⁻ -N (mg/L)	DO (mg/L)
1	0 10 20 30	Partial nitrification sludge/effluent	7.5 7.5 7.5 7.5		20 20 20 20			0.5 0.5 0.5 0.5
2	0 10 20 30	Partial nitrification sludge/effluent	7.5 7.5 7.5 7.5			20 20 20 20		0.5 0.5 0.5 0.5
3	0 10 20 30	Partial nitrification sludge/effluent	7.5 7.5 7.5 7.5		10 10 10 10		10 10 10 10	0.5 0.5 0.5 0.5
4	0 10 20 30	Partial nitrification sludge/effluent	7.5 7.5 7.5 7.5			10 10 10 10	10 10 10 10	0.5 0.5 0.5 0.5
5	0 10 20 30	Partial nitrification sludge/inflow	7.5 7.5 7.5 7.5	20 20 20 20		20 20 20 20		0.5 0.5 0.5 0.5
6	0 10 20 30	Partial nitrification sludge/effluent	7.5 7.5 7.5 7.5	20 20 20 20		20 20 20 20		0.5 0.5 0.5 0.5

Note(s): ATU: Allylthiourea, an ammonia nitrogen oxidation inhibitor.

2.3. Detection Method

The NH₄⁺-N, NO₂⁻-N, and NO₃⁻-N were measured according to methods described in previous studies [17]. The DO, pH, and T were measured using an oxygen, pH, and

temperature meter (WTW 340i, WTW Company, Munich, Germany), and the temperature and DO were controlled using an appropriate sensor and PLC, respectively. The Mixed Liquid Suspended Solids concentration was measured at the beginning and end of each test to obtain an average value, which was used for the calculation of the NH₄⁺-N oxidation rate, NO_x^- -N production rate, and N₂O emission rate. The total N₂O production comprised the N₂O emitted in the gaseous phase (emission gas N₂O) and the N₂O dissolved in the mixed liquid phase (dissolved N₂O). The N₂O concentrations in the gas samples were analyzed in triplicate using a gas chromatograph (Agilent 6890N, Santa Clara, CA, USA). The overhead space method was used to analyze the dissolved N₂O. Water and N₂O samples were taken at 30 min intervals.

3. Results and Discussion

3.1. Effect of Salinity on N₂O Emissions in Ammonia Nitrogen Oxidation Process

Figure 2 shows the changes in the nitrogen levels (initial $NH_4^+-N = 20 \text{ mg/L}$) at salinity: 0 mg/L NaCl. The oxidation of NH_4^+ caused N_2O to reach its maximum value (0.26 mg/L) at 60 min. Next, with the gradual completion of NH_4^+ oxidation, even though there was still a high amount of NO_2^--N produced in the system, the output of N_2O gradually decreased and tended to 0. This indicated that, during the oxidation of NH_4^+ , the NH_4^+ oxidation process was the source of the electrons produced by the N_2O . When the oxidation of NH_4^+ ended, NO_2^- could not be denitrified due to the high concentration of no electron donor in the system. During the reaction time of 180 min, the total yield of N_2O was 0.75 mg/L.



Figure 2. The variations in N₂O during NH₄⁺ oxidation (0 mg/L NaCl), Batch Test Rules 1.

Figure 3 shows the rate of the nitrogen change in organic-free water (effluent +20 mg/L NH₄⁺-N) under varying salinity gradients. With a gradual increase in the concentration of NaCl in the system from 0 mg/L to 30 mg/L, the oxidation rate of NH₄⁺ and the formation rate of NO₂⁻-N showed downward trends. However, the rate of N₂O emissions increased from 0.08 mgN/(gMLSS·L·h) to 0.25 mgN/(gMLSS·L·h). This indicated that the increase in salinity increased the N₂O emissions in the NH₄⁺ oxidation process of the AOB enrichment system.



Figure 3. The variations in N conversion rates during NH_4^+ oxidation under different salinity gradients.

During the oxidation of NH₃, NH₃ is first oxidized to NH₂OH under the action of AOB, and then NH₂OH is oxidized to NO_2^{-} [18]. The first step in this process is catalyzed by ammonia oxidase (AMO), where molecular oxygen acts as an electron acceptor [7]. The second step is performed under the action of hydroxylamine oxidase (HAO), where molecular oxygen is the primary electron acceptor [7]. The current literature has shown that the effect of N_2O on AOB might be caused by the following two ways: (1) N_2O as a product of the autotrophic denitrification of AOB using NO_2^- as an electron acceptor [8,11]; or (2) N_2O as a byproduct of the incomplete oxidation of hydroxylamine [7–10]. In the first pathway of N₂O production, NO_2^- is reduced to N₂O by NO in the presence of coppercontaining enzymes, NO_2^- reductase and NO reductase. With an increase in salinity, the ammonia oxidation rate and NO_2^- formation rate both decreased, indicating that the increase in salinity inhibited the nitrification of AOB, which could have been due to the fact that salinity inhibited both AMO and HAO during the oxidation of NH₃, resulting in incomplete NH_3 . The ammonia oxidation rate in the system was always found to be greater than the NO_2^- generation rate under different gradient salinification, indicating that a part of the generated NO_2^- was denitrified during NO_2^- generation (Figure 3). With an increase in salinity, the ammonia oxidation rate and NO₂⁻ production rate both decreased, but the N₂O emission rate increased, indicating that salinity had an inhibitory effect on the reduction in N_2O . The mechanism of action might involve the inhibitory effect of salinity on N₂O reductase.

3.2. Effect of Salinity on N₂O Emissions in the Hydroxylamine Oxidation Process

Figure 4 shows the change in N₂O during the initial addition of 20 mg/L of NH₂OH-N when the salinity was 0. When 20 mg/L of NH₂OH-N was initially added to the outflow water, the maximum yield of N₂O (0.20 mg/L) appeared at 30 min, and the speed of reaching the maximum yield was faster than that of NH₄⁺ alone, which could have been due to the fact that, compared to NH₄⁺, the oxidation from NH₂OH was one step less than the oxidation from NH₄⁺. Furthermore, the NO₂⁻ levels continued to increase as the reaction progressed, which indicated that NH₂OH was being continuously oxidized. With the continuous oxidation of NH₂OH, the emissions of N₂O decreased in turn. During the reaction time of 180 min, the total yield of N₂O was 1.19 mg/L.



Figure 4. The variations in N₂O during NH₂OH oxidation (0 mg/L NaCl), Batch Test Rules 2.

Figure 5 shows the trend in the variation of N₂O during the oxidation of NH₂OH at salinity = 0. With a gradual increase in salinity from 0 mg/L to 30 mg/L, the rate of NO₂⁻ generation showed a downward trend, i.e., 0.00197 mgN/(gMLSS·L·h) and 0.00172 mgN/(gMLSS·L·h) at 0 mg/L and 30 mg/L, respectively. The N₂O emission rate increased from 0.13 mgN/(gMLSS·L·h) at a salinity of 0 mg/L to 0.17 mgN/(gMLSS·L·h) at a salinity of 30 mg/L. This suggested that an increase in salinity increased the N₂O emissions in the hydroxylamine oxidation process with the salinity load.



Figure 5. The variations in N conversion rates during NH2OH oxidation under different salinity gradients.

Figures 2 and 4 show that the total amount of N₂O emissions with the initial addition of 20 mg/L of NH₂OH in the outflow water was more than that produced by the initial addition of 20 mg/LNH₄⁺, which was the same as that reported by Kim [11] and Wunderlin [19]. The study by Kim reported that four electrons were produced during the NO₂⁻ oxidation by NH₂OH from HAO, of which two electrons were consumed during the NH₄⁺ oxidation to NH₂OH from AMO; thus, only two electrons were used for the autotrophic denitrification of NO₂⁻.

However, when NH₂OH was used as a nitrification substrate, all four electrons were used for the autotrophic denitrification of NO_2^- , resulting in a greater N₂O production. The NO_2^- production rate showed a downward trend under four salinity gradients, indicating

that the nitrification with NH₂OH as substrate was inhibited, which could have been due to the salinity-induced inhibition of hydroxylamine oxidase (HAO) (Figure 5). When NO₂⁻ decreased with an increase in salinity, the N₂O emissions increased with an increase in salinity, which could have been due to the inhibitory effect of salinity on N₂O reductase during the autotrophic denitrification of AOB using NO₂⁻ as an electron acceptor.

3.3. Effect of Salinity on N₂O Emissions in the Autotrophic Denitrification Process

Figure 6 shows the variation trend in N₂O during the autotrophic denitrification at salinity = 0. In this experiment, 10 mg/L of NH_4^+ -N and 10 mg/L of NO_2^- -N were added to the mud–water mixture of the partial nitrification effluent, and then nitrification was performed at 0.5 mg/L DO. With the oxidation of NH_4^+ -N, N₂O rapidly reached its maximum value (0.33 mg/L) at 30 min. In this reaction process, both the N₂O emissions due to the oxidation of NH_4^+ -N itself and the electrons provided by the oxidation of NH_4^+ -N were used to conduct denitrification, with the addition of NO_2^- as an electron acceptor. In the whole reaction process, the total N₂O emissions were 0.54 mg/L. The study by Kim [11] showed that the autotrophic denitrification of AOB in the nitrification process is the primary pathway for N₂O emissions. Therefore, in this experiment, the effect of salinity on the N₂O emissions during autotrophic denitrification was mainly affected.



Figure 6. The variations in N₂O during autotrophic denitrification (10 mg/L NH_4^+ -N, 10 mg/L $NaNO_2$ -N at initial reaction, 0 mg/L NaCl), Batch Test Rules 3.

Figure 7 shows the variation trend in N₂O in autotrophic denitrification under the influence of salinity. There was a decrease in the oxidation rate of NH_4^+ -N with an increase in salinity, and the formation rate of NO_2^- -N also decreased with an increase in salinity. There was a successive increase in the emission rate of N₂O-N with an increase in the salinity load. At salinity = 0 mg/L, 10 mg/L, 20 mg/L, and 30 mg/L, the values were 0.22 mgN/(gMLSS·L·h), 0.28 mgN/(gMLSS·L·h), 0.31 mgN/(gMLSS·L·h), and 0.63 mgN/(gMLSS·L·h). At salinity (0 mg/L to 20 mg/L), the rate of N₂O-N rapidly increased relatively slowly. At salinity = 30 mg/L, the formation rate of N₂O-N rapidly increase in N₂O emissions during partial nitrification.



Figure 7. The variations in N conversion rates during autotrophic denitrification ($10 \text{ mg/L NH}_4^+\text{-N}$, $10 \text{ mg/L NaNO}_2\text{-N}$ at initial reaction, 0 mg/L NaCl) under different salinity gradients.

Figure 8 shows the variation trend in N₂O during autotrophic denitrification (10 mg/LNH₂OH-N and 10 mg/L NaNO₂-N) under the influence of salinity. There was a rapid increase in N₂O-N to 0.16 mg/L at 30 min. The NaNO₂ levels increased during the whole reaction process, which indicated that NH₂OH was continuously oxidized by microorganisms. As the reaction progressed, there was an insignificant increase in NO₂⁻-N, and the N₂O emissions were stabilized and gradually declined, which indicated that the presence of NH₂OH was critical for the N₂O emissions. During the whole reaction process, the total N₂O emissions were 0.68 mg/L.



Figure 8. The variations in N₂O during autotrophic denitrification (10 mg/L NH₂OH-N, 10 mg/L NaNO₂-N at initial reaction, 0 mg/L NaCl) under different salinity gradients, Batch Test Rules 4.

Figure 9 shows the variations in the nitrogen rate during autotrophic denitrification (10 mg/LNH₂OH-N and 10 mg/L NaNO₂-N) under the influence of salinity. The formation rate of NO₂⁻-N decreased with an increase in salinity. At salinity = 0 mg/L, 10 mg/L, 20 mg/L, and 30 mg/L NaCl, the formation rates of NO₂⁻-N were as follows: 0.79 mgN/(gMLSS·L·h), 0.75 mgN/(gMLSS·L·h), 0.71 mgN/(gMLSS·L·h), and 0.69 mgN/(gMLSS·L·h), respectively. However, the N₂O emission rate showed a gradual

upward trend, with N₂O production rates of 0.10 mgN/(gMLSS·L·h), 0.11 mgN/(gMLSS·L·h), 0.12 mgN/(gMLSS·L·h), and 0.18 mgN/(gMLSS·L·h), respectively. At salinity levels of < 30 mg/L, the increasing trend of N₂O was not apparent, but at salinity = 30 mg/L, the N₂O rapidly increased to 0.18 mgN/(gMLSS·L·h).



Figure 9. The variations in N conversion rates during autotrophic denitrification (10 mg/L NH₂OH--N, 10 mg/L NaNO₂-N at initial reaction, 0 mg/L NaCl) under different salinity gradients.

For nitrification using NH_4^+ and NH_2OH as substrates, the formation rate of NO_2^- showed a downward trend, but the N_2O emissions increased with an increase in salinity. This indicated that high levels of salinity had an inhibitory effect on N_2O reductase; consequently, the N_2O emissions of AOB in autotrophic denitrification with NO_2^- as an electron acceptor could not be further reduced, in turn increasing N_2O emissions.

3.4. Effect of Salinity on N_2O Emissions of Heterotrophic Denitrification during the Nitrification Process

Figure 10 shows the variation in the N_2O emissions during heterotrophic denitrification under the influence of salinity. When 20 mg/L of NH_2OH-N was added to the partial nitrification effluent, the N_2O of the nitrification process mainly resulted from the self-oxidation of NH₂OH and autotrophic denitrification of AOB. However, when 20 mg/L of NH₂OH-N and ATU were added to the influent, the nitrification began with the oxidation of NH_2OH , because ATU could completely inhibit the oxidation of NH_4^+ . However, since there was a greater amount of biostable organic matter in the inlet than in the effluent, the available organic matter might have affected the N_2O emissions during nitrification. The total N₂O yield of the influent water used as test water was reduced from that of the effluent water. The N_2O emissions after the reduction were not 0, which could have been due to the denitrification of NO_2^- by heterotrophic bacteria using organic matter during the nitrification (Figure 10). When in the effluent water, the N_2O emissions of the NH₂OH oxidation and AOB autotrophic denitrification increased with an increase in salinity, and the values under four salinity gradients were 0.79 mg/L, 1.02 mg/L, 1.08 mg/L, and 1.19 mg/L, respectively. The N_2O emissions due to the denitrification of heterotrophic bacteria also increased with an increase in salinity, and the values were 0.017 mg/L, 0.024 mg/L, 0.044 mg/L, and 0.067 mg/L, respectively. The ratios of the N₂O emissions due to heterotrophic denitrification to the total N2O emissions of the influent as the test object were: 2.1%, 2.3%, 3.9%, and 5.4%, respectively. During nitrification, the N₂O produced by heterotrophic denitrification could not be ignored, and the effect of the N₂O emissions due to heterotrophic denitrification was enhanced at a high salinity. This could have been due to the inhibitory effect of salinity on N₂O reductase.



Figure 10. The variations in N₂O during heterotrophic denitrification under different salinity gradients, (Batch Test Rules 5, 6).

4. Conclusions

This study investigated the AOB enrichment system cultured in actual domestic wastewater along with the influence of salinity on N_2O emissions in a partial nitrification system and their mechanism. The following conclusions were drawn:

- The increase in salinity decreased the oxidation rate of NH₄⁺ and the formation rate of NO₂⁻ during the reaction.
- (2) The increase in salinity increased the N₂O emissions during the oxidation of NH₄⁺ and NH₂OH, and decreased the production rate of NO₂⁻-N during the oxidation of hydroxylamine.
- (3) The total amount of N₂O emissions in the hydroxylamine oxidation process was less than that during ammonia nitrogen oxidation, and more NO₂⁻ might have been reduced to N₂ instead of N₂O during hydroxylamine oxidation.
- (4) During partial nitrification with the available organic matter, the N₂O emissions due to heterotrophic denitrification by heterotrophic bacteria could not be ignored, and the increase in salinity could increase the amount of N₂O emissions due to heterotrophic denitrification.

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