



Article Examining the Effects of Tree Canopy Coverage on Human Thermal Comfort and Heat Dynamics in Courtyards: A Case Study in Hot-Humid Regions

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Abstract: Providing thermal comfort in the courtyards of academic buildings is important and increasing tree canopy coverage (TCC) presents a convenient and feasible method to achieve this; however, few studies have comprehensively evaluated the cooling effects of TCC, considering both outdoor thermal comfort and heat dynamics. In this study, we selected two typical academic buildings at Guangzhou University, each with courtyards having different height-to-width ratios (H/W ratios). We employed both field measurements and ENVI-met-based numerical models to simulate scenarios with varying TCCs. The results demonstrated that the cooling effects caused by arranging trees increase with the TCC values. During the hottest hours of the day, trees arranged in courtyards with high H/W ratios exhibited a superior cooling effect compared to those in courtyards with low H/W ratios, with a difference of up to 0.6 °C in the PET (physiological equivalent temperature); however, over the entire daytime, the total sensible heat reduction achieved by trees in courtyards with low H/W ratios surpassed that of courtyards with high H/W ratios, with a difference of up to 0.25 \times 10⁴ J/m². Our findings underscore the crucial role of TCC in enhancing cooling in the courtyard of academic buildings, with important implications for university planning and design.

Keywords: tree canopy coverage; outdoor thermal comfort; sensible heat dynamic; courtyard; hot-humid regions

1. Introduction

In recent years, rapid urbanization and the impacts of climate change have intensified the urban heat island (UHI) effect in dense cities. Urban heat islands refer to urban areas with higher temperatures than the surrounding rural areas, leading to more frequent occurrences of extreme weather conditions [1,2]. Exposure to extreme heat environments can pose severe threats to human health and well-being [3–5]. Consequently, high temperatures encourage people to spend more time indoors, relying on artificial air conditioning to achieve comfort [6,7]; however, this growing trend contributes to a sedentary lifestyle, negatively impacting human health and significantly increasing building energy consumption [8–10]. Therefore, addressing this issue requires prioritizing the design for urban climate resilience, a crucial aspect to reduce carbon emissions and enhance urban livability [11,12].

Among the various mitigation strategies aimed at achieving resilient urban design, the most extensively studied perspectives in the literature include the utilization of urban geometry [13,14], shading [15,16], greenery [17,18], and reflective technologies [19,20]. Another highly effective strategy for mitigating the UHI effect is the implementation of courtyards as "Urban Cool Islands" [21]. Courtyards have been widely adopted in different climatic regions, particularly in hot and arid climates and temperate climate zones, as well as in cold regions and hot-humid regions. The advantages of courtyards for such diverse climates are noteworthy; they create more shading in hot climates, enhance natural



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ventilation in humid climates, and provide protection against cold winds in temperate and cold climates [22].

Buildings and trees play crucial roles in determining the human thermal comfort of courtyards, as they collectively influence the redistribution of the occupant thermal sensations in outdoor spaces. Buildings provide shade, effectively preventing the surface from heating up due to solar radiation [23]. Additionally, the arrangement and form of buildings impact the air flow, facilitating heat dispersion [24]. Many design measures have been proposed to enhance the outdoor thermal comfort of courtyards. Eduardo Diz-Mellado et al. discovered that when the aspect ratio (AR) of a courtyard exceeds three, the comfort level is achieved for 90-100% of the day's hours, and when the AR is between two and three, it reaches approximately 70–80%. Moreover, the cooling requirements of courtyards vary significantly based on their AR, with differences of up to 18% [25,26]. Similarly, Nazanin Nasrollahi et al. found that courtyards with high height-to-width (H/W)ratios and a southward orientation offered better shading during summer while permitting solar radiation in and regulating the wind speed during winter [27]. This finding aligns with the research of Rodriguez-Algeciras, Jose, et al., which suggests that orienting a courtyard's long axis away from the east to west direction results in a lower level of T_{mrt} (mean radiant temperature) in the summer [28].

Furthermore, trees not only regulate the outdoor microclimate through shading, by absorbing and reflecting solar radiation, but they also regulate the environmental conditions through transpiration. Previous studies have investigated and generally confirmed the cooling effects of trees on the city to the neighborhood scales. For instance, Jin et al. conducted a study demonstrating that increasing the number of trees in an open space by threefold of the advisory guidelines led to a significant reduction of the average air temperature by 0.9 °C, the mean radiant temperature by 11.0 °C, the physiological equivalent temperature by $4.5 \,^{\circ}$ C, and the wind speed by $0.30 \,\text{m/s}$ [29]. In another study, Zhao et al. found that at 15:00 hours, trees arranged along a street can provide a cooling effect of $1-1.5 \,^{\circ}\text{C}$ (PET) to the human body at the pedestrian level. Although adjusting the position of the trees may cause a slight loss in the air temperature cooling effect of 0.05 °C, this can still achieve a T_{mrt} cooling effect of 0.1 °C, which is three times the temperature cooling effect [30]. Furthermore, Zhang et al. discovered that planting trees in courtyards can reduce the PET by 20.0 °C and decrease the cooling demand by approximately 2.6% [31]; however, these studies primarily focused on microclimatic parameters, including the air temperature (T_a) , relative humidity (RH), globe temperature (T_g) , and wind speed (V_a) .

Heat fluxes of urban landscapes exhibit variation at different times and seasons, and these energy dynamics significantly affect the thermal comfort of urban residents [32]. For example, Li et al. found that tree evapotranspiration and enhanced hydrological processes in different urban land use types in Singapore led to varying increases in the latent heat flux and reductions in the sensible heat flux [33]. Another study by Heusinger, Jannik et al. revealed that the difference in the urban excess heat reduction between green roofs and common roofs can be as high as 3% [34]. Furthermore, the aspect ratio and building height also exert notable effects on local energy fluxes. For instance, at noon, increasing the aspect ratio from 0.5 to 10.0 can result in a reduction of 300.0 W/m^2 in the sensible heat flux [35,36]; therefore, it is essential to adopt comprehensive methods to evaluate the cooling capacity of thermal mitigation strategies, including tree arrangements in courtyards. The microclimate simulation software, ENVI-met, provides the possibility to achieve this goal. ENVI-met is a three-dimensional microclimate computational fluid dynamics (CFD) software capable of simulating microscale interactions within built environments. It provides physical quantities such as the T_a , RH, V_a , and T_{mrt} [37,38]. Moreover, ENVI-met is able to simulate the effects of detailed vegetation, making it widely used for microclimate simulation in urban spaces, especially in hot-humid regions [39,40], which aligns well with the objectives of this research [41,42].

Therefore, in this study, we aim to address the above-mentioned insufficiency by utilizing the human thermal comfort index and the total sensible heat change to evaluate

the cooling efficiency provided by TCC in academic building courtyards with different W/L ratios. The evaluation was conducted under typical summer climate conditions in hot-humid areas. Furthermore, based on our findings, we propose recommendations for the construction and renovation of courtyards in academic buildings.

2. Materials and Methods

2.1. Climate Conditions

Guangzhou (23°12′ N; 113°20′ E), the capital of Guangdong Province, is located on the subtropical coast of China. It experiences a monsoon-influenced humid subtropical climate, characterized by hot and humid summers, abundant rainfall, and relatively temperate and dry winters. The annual mean temperature and humidity are 22.0 °C and 77% [43], respectively. July is the hottest month, with an average temperature of 28.7 °C. The prevailing wind directions in Guangzhou exhibit seasonality. During the summer, south-easterly winds dominate due to the influence of subtropical highs and the South China Sea lows.

2.2. Study Area and Field Measurement

As shown in Figure 1, we selected two adjacent academic buildings of Guangzhou University as the research object, of which the academic building on the east side was named DZXX, and the academic building on the west side was named LX. These academic buildings are similar in size, with both having a height of 24 m and a total of 7 floors, with the ground floors serving as overhead spaces. Their difference is the H/W ratio of their respective courtyards. Among them, the courtyard of DZXX has a height of 24 m and a width of 27 m, while the courtyard of LX has a height of 24 m and a width of 33 m; therefore, their H/W are defined as 0.9 and 0.7, respectively. To evaluate the thermal environment and verify the accuracy of the simulation model, we conducted field measurements on 21 July 2022. Previous studies have shown that low airflow velocity and high radiation load conditions may have a significant impact on the accuracy of some measurement instruments' results [44,45]; therefore, in this study, a total of 5 measurement points were distributed in the overhead space of two academic buildings, avoiding direct sunlight measurement instruments. The overhead space refers to the bottom floor of a building, which is completely open and has no walls or windows [46]. Each measurement point was set at 1.5 m above ground. The measurement instruments and their respective parameters used for the field measurements are listed in Table 1. Among them, the globe thermometer (JTR 04) used was 150 mm in diameter with an emissivity equal to 0.95.



Figure 1. The field survey in this research.

Instrument	Parameter	Measuring Range	Accuracy
HOBO Pro	Air temperature	–40.0 to 70.0 °C	±0.5 °C
HOBO Pro	Relative humidity	0 to 100%	$\pm 2.5\%$
Kestrel5500	Wind speed	0 to 5 m \cdot s ⁻¹	$\pm 0.05~\mathrm{m}{\cdot}\mathrm{s}^{-1}$
JTR04	Black bulb temperature	10.0 to 85.0 $^\circ \text{C}$	$\pm 0.5~^\circ \mathrm{C}$

Table 1. Measuring instruments for the numerical model validation.

2.3. Model Validation

The validation of the ENVI-met model is vital to ensure reliable simulation outputs [47]. In many previous studies, the reliability of the ENVI-met model output was assessed by comparing it with the measured T_a and RH [48–50]; therefore, the air temperature and RH of each point were measured on-site and compared with the simulated values of the ENVI-met model. Subsequently, the model reliability was assessed. The correlation coefficients (R^2), mean absolute error (MAE), and root mean square error (RMSE) were used to test the model accuracy [51], as calculated using Equations (1)–(3):

$$RMSE = \sqrt{\frac{\sum_{i=1}^{n} (X_{obs,i} - X_{model,i})^2}{n}}$$
(1)

$$MAE = \frac{\sum_{i=1}^{n} \left| X_{obs,i} - X_{model,i} \right|}{n}$$
(2)

$$R^{2} = 1 - \frac{\sum_{i=1}^{n} (X_{obs,i} - X_{model,i})^{2}}{\sum_{i=1}^{n} (X_{obs,i} - X_{obs})^{2}}$$
(3)

where X_{obs} is the measured value, X_{model} is the simulated value, and *n* is the number of data values.

2.4. Case Studies

In this study, two models were constructed according to the current situation. In both models, the height of the building was 24 m tall, with ordinary concrete vertical walls and a flat roof. The underlying surface was mainly composed of asphalt and red bricks. In addition, trees surrounding the buildings have also been established. The main difference between the two models was the H/W ratio of the academic building, which was 0.9 (DZXX) and 0.7 (LX), respectively. The input parameter settings for the ENVI-met model are presented in Table 2. The geographical location coordinates were set to 113.20 °E and 23.12 °N, and the time zone was set to UTC/GMT + 08:00. This model accurately reproduced the building where the test site was located as well as the surrounding greenery. The wind speed, hourly temperature and humidity data were derived from data recorded by meteorological stations. The weather station used in this study was the HOBO meteorological station, which was shielded by ventilated boxes to avoid direct sunlight. The meteorological station was located on the roof of the academic building on the north side of the DZXX, with a distance of approximately 100 m. Solar radiation data were calculated using the geographic location data system input into the ENVI-met model, and the solar radiation correction ratio input was 1.0 [50].

Variable	Settings		
Circ and moduli in	51 imes 48 imes 20		
Size and resolution	x = 3 m, $Y = 3 m$, and $Z = 3 m$		
Date	21 July 2022		
Duration	7:00 a.m.–18:00 p.m.		
Solar radiation correction ratio	1.0		
Initial T_a and RH	29.3 °C/79.1%		
Wind velocity and wind direction at 10 m	$1.1 \mathrm{~m/s}, 135^{\circ}$		
Specific humidity at 2500 m	10.76 g/kg		
Soil initial tomporature	31.5 °C (0–20 cm)/33.9 °C (20–50 cm)/32.9 °C		
Son mitiai temperature	(<50 cm)		
Soil initial humidity	30% (0–20 cm)/40% (20–50 cm)/50% (<50 cm)		
	Wall: 0.30		
. 11 . 1	Roof: 0.45		
Albedo	Asphalt: 0.20		
	Brick road: 0.30		

Table 2. ENVI-met input parameters for the simulations.

During the field investigation, the surrounding vegetation type was determined to be *Michelia able*. To ensure a more precise prediction of the tree canopy coverage's impact on the thermal environments of courtyards with different H/W ratios, a specific ENVI-met model of *Michelia able* was established for subsequent simulations. The model parameters of *Michelia able* were set as follows: a tree height of 10.46 m, crown diameter of 6 m, underbranch height of 3 m, and leaf area index (LAI) value of $2.46 \text{ m}^2/\text{m}^2$ [52]. The trees were planted 6 m away from the academic buildings. Considering the uniform distribution of tress in each courtyard, six TCC scenarios were implemented for each courtyard, with percentages of 21%, 26%, 31%, 36%, 47%, and 68%, respectively. Additionally, a 0% scenario was included, representing the absence of greenery inside each courtyard, serving as a control.

2.5. Thermal Comfort Assessment Indices

Many thermal comfort indices derived from the human energy balance have been developed to evaluate the outdoor environment, such as the wet-bulb globe temperature (WBGT), physiological equivalent temperature (PET), and the universal thermal climate index (UTCI) [53,54]. Among them, the PET is determined using the Munich energy balance model for individuals (MEMI) [55]. It represents the equivalent air temperature in a typical indoor condition and approximates the human body's thermal perceptions in an outdoor setting [56]. Meanwhile, independent physiological parameters, such as height, age, and the human metabolic rate of activity, were considered for calculating the PET index [57]. Furthermore, the PET is one of the most widely used thermal indices for assessing thermal comfort in degrees Celsius (°C) and it has been adopted in numerous studies and practical applications [40,58–60]; therefore, we selected the PET as the evaluation index to measure the thermal environments of the courtyards in the academic buildings. It is worth noting that the thermal comfort perception can vary across different regions. For instance, Lai et al. pointed out that residents in the north are more receptive to cold environments compared to in Europe and Taiwan [61]. Additionally, Lin and Matzarakis reported diverse grades of thermal perception in a subtropical area, highlighting the adaptive comfort effect on human thermal perception across various climatic settings [62]. Thus, as shown in Table 3, the thermal sensations for different stress categories and PET values specific to Guangzhou were selected for this study. In this study, the PET output was obtained through the BIOmet module of ENVI-met. Considering that the main activity group comprised students, the characteristics of a standard person were set as a 19-year-old male, 1.71 m tall and 60.14 kg in weight [57,63], with a basic clothing insulation value of 0.4 clo. In addition, students mostly walk slowly in the outdoor spaces of the academic buildings; therefore, the metabolic rate was set to 2.0 met.

PET Value	Thermal Sensation Grade of Physiological Stre	
-	Very cold	Extreme cold stress
-	Cold	Strong cold stress
<11.3 °C	Cool	Moderate cold stress
11.3–19.2 °C	Slightly cool	Slight cold stress
19.2–24.6 °C	Comfortable	No thermal stress
24.6–29.1 °C	Slightly warm	Slight heat stress
29.1–36.3 °C	Warm	Moderate heat stress
36.3–53.6 °C	Hot	Strong heat stress
>53.6 °C	Very hot	Extreme heat stress

Table 3. Range for PET assessment in Guangzhou [57].

2.6. Estimation of the Sensible Heat Dynamic

An increase in sensible heat contributes to the warming of the atmosphere, which is the main cause of UHIs [64,65]. Evapotranspiration from vegetation, in combination with shading effects, can lower the ambient air temperature by a reduction in the sensible heat fluxes into the atmosphere. The energy savings from the cooling effect of green spaces can be estimated by measuring the sensible heat reduction; therefore, in this study, the sensible heat reduction of different tree species with different TCC scenarios was calculated using Equation (4) [66]:

$$\Delta E = C_p \cdot \Delta T \cdot \rho \cdot V \tag{4}$$

where ΔE is the energy variation (J), C_p is the specific heat of the air, which was set as 1.0×10^3 J/kg °C, ρ is the air density, which was set as 1.29 kg/m³, ΔT is the air temperature difference between the two scenarios, and *V* is the air volume of different atmospheric layers.

Previous research on the thermal environment of courtyards has predominantly focused on the pedestrian-level thermal environment, which directly influences human thermal comfort [67–69]; however, the cooling effects of vegetation affect not only the near-surface thermal environmental layer but also extend to the higher atmospheric layers [66,70]. Therefore, to predict the effects of different TCCs on sensible heat reduction at various heights, the space was cut into seven layers according to the grid size in the Z-direction of the ENVI-met model, including 1.5 m, 2.1 m, 2.7 m, 4.5 m, 7.5 m, 11 m, and 14.5 m layers. In this study, the lower layers of the tree crown were situated at heights of 1.5 m, 2.1 m, and 2.7 m, while the upper layer of the tree crown was at a height of 14.5 m.

3. Results

3.1. Statistical Summary of the Thermal Environment and Model Accuracy Assessment

Table 4 shows the variation of T_a , T_g , RH and V_a at each measurement point. The average values of T_a and T_g at each measurement point were found to be greater than 32.6 °C. The RH ranged from 56.4% to 77.0%, and the average wind speed ranged from 0.3 m/s to 0.7 m/s. Thus, these climate conditions on the measurement days represent a typical summer climate in hot-humid areas.

Figure 2 displays the comparison between the simulated and measured air temperatures and RH values at each measured point. The R^2 between the measured and simulated values for T_a and RH were 0.88 and 0.94, respectively. The corresponding RMSE values ranged from 1.62 to 2.11 for the T_a and 2.62 to 3.73 for the RH, while the *MAE* ranged from 0.33 to 0.48 for the T_a and 0.41 to 0.63 for the RH. These values fall within the acceptable range based on previous studies, where *RMSE* values between 0.52 and 4.30 and *MAE* values between 0.27 and 3.67 have been considered acceptable [71,72]; therefore, the R^2 , *RMSE* and *MAE* values obtained in this research indicate that the ENVI-met predictions in the context of this study were accurate enough. Regarding the air velocity, the software output value generally underestimated the air velocity level of the overhead layer [73]. Because the transitional space was ventilated on all sides, the actual wind field was subject to a large change in the wind speed and direction in real time. In addition to natural wind, the wind speed experienced by pedestrians in dynamic situations also includes the disturbance wind speed caused by walking [50]. Regarding the mean radiant temperature, wind speed is one of the main factors affecting the calculation of the mean radiant temperature, and the simulated differences in air velocity will lead to a difference in the mean radiant temperature. Although there are certain differences between the simulated and measured values, the changing trends in air velocity and mean radiant temperature can still reflect the impact of tree canopy coverage on the outdoor thermal environment.

Monitoring Points	Parameters	Minimum	Maximum	Mean	Standard Deviations
Point 1	T_a (°C)	29.3	33.9	32.7	1.19
	T_g (°C)	30.5	34.3	32.9	1.21
	RH (%)	58.7	76.0	65.5	5.39
	V_a (m/s)	0	1.5	0.4	0.39
Point 2	T_a (°C)	30.1	33.9	32.6	1.17
	T_g (°C)	30.4	34.1	32.8	1.10
	RH (%)	58.2	75.8	64.5	5.33
	V_a (m/s)	0	0.8	0.3	0.27
Point 3	T_a (°C)	30.0	33.9	32.6	1.25
	T_g (°C)	30.2	34.3	32.9	1.34
	RH (%)	57.9	77.0	64.8	5.68
	V_a (m/s)	0	2.2	0.6	0.47
Point 4	T_a (°C)	30.3	34.4	33.0	1.30
	T_g (°C)	28.8	34.5	32.9	1.68
	RH (%)	57.4	76.4	64.4	5.59
	$V_a (m/s)$	0	2.8	0.5	0.64
Point 5	T_a (°C)	30.1	34.3	32.8	1.34
	T_g (°C)	29.2	34.8	33.1	1.74
	RH (%)	56.4	76.3	63.9	5.80
	V_a (m/s)	0	1.7	0.7	0.55

Table 4. Statistical results of microclimate parameters.



Figure 2. Correlation between the measured and simulated *Ta* and RH. (**a**–**e**) were *Ta* of point 1–5; (**f**–**j**) were RH of point 1–5.

3.2. Variation in T_a

Figure 3 illustrates the average T_a at a 1.5 m height of each courtyard with TCC from 0% to 68% at different times of the day. In the scenarios without trees (0% TCC), the T_a was

higher in the DZXX between 8:00 a.m. and 13:00 p.m., and in the LX between 14:00 p.m. to 18:00 p.m., with the maximum T_a difference being 0.2 °C. This indicates that during the daytime, the T_a increased more slowly in the courtyards with higher H/W ratios than in those with lower H/W ratios. As the TCC increased, the T_a in each courtyard decreased, and scenarios with different TCCs simulated various cooling effects in courtyards with different H/W ratios. During the time period from 10:00 AM to 13:00 PM, the trees in the courtyard with a higher H/W ratio (LX) exhibited better cooling effects compared to the courtyard with a lower H/W ratio (DZXX). For example, when the TCC was 21%, there was essentially no reduction in the T_a in the DZXX; however, after 13:00 p.m., the temperature drop in the two courtyards became almost the same at the same TCC, with a difference of not more than 0.1 °C. When the TCC was 68%, the difference in the T_a between the two courtyards was 0.2 °C.



Figure 3. Average T_a at 1.5 m height of each courtyard with tree canopy cover from 0% to 68% at different times of the day. (a) DZXX and (b) LX.

3.3. Variation in T_{mrt}

Figure 4 shows the average T_{mrt} at a 1.5 m height of each courtyard with TCC from 0% to 68% at different times of the day. From 11:00 a.m. to 17:00 p.m., the average T_{mrt} values at a 1.5 m height in the LX were significantly higher than those in the DZXX, with the maximum difference in T_{mrt} between the two courtyards reaching up to 2.4 °C. As shown in Figure 5, the direct sun hours in the courtyards of the two academic buildings under typical summer conditions in hot-humid areas were simulated by using a Rhino's ladybug plugin (0% TCC). It is evident that the LX courtyard received more solar radiation than the DZXX under treeless conditions. As the TCC increased, the T_{mrt} values of each courtyard decreased substantially. The T_{mrt} values for each courtyard decreased the most when the TCC was 68%, by 10.6 °C and 10.7 °C, respectively. Furthermore, the maximum difference in the T_{mrt} between the two courtyards was reduced to 1.7 °C. This indicates that arranging trees can effectively reduce the differences in solar radiation between courtyards with different H/W ratios.



Figure 4. Average T_{mrt} at 1.5 m height of each courtyard with tree canopy cover from 0% to 68% at different times of the day. (a) DZXX and (b) LX.



Figure 5. Direct sun hours of each courtyard (Daylight hour of the cases in a full day). (**a**) DZXX and (**b**) LX.

3.4. Thermal Comfort Assessment

The effects of different TCCs on the PET in different courtyards at each time period is shown in Figure 6. Based on the PET scale applied to Guangzhou, both courtyards made people feel "hot" at all times of the day under the treeless scenario. Compared to the courtyard of DZXX, the courtyard of LX had higher PET values, with a maximum difference of 0.7 °C at 16:00 p.m. Although arranging trees in each courtyard can reduce the PET values, the PET values in both courtyards remained at the "hot" level during each time period; however, as the TCC continued to rise to 68%, the PET values in each courtyard decreased by up to 5.4 °C (DZXX) and 5.5 °C (LX) at 9 a.m., respectively. This indicates that although planting trees can improve the outdoor thermal environment, it may be challenging to reduce the level of outdoor thermal comfort to a "warm" or lower category. Furthermore, at 14:00 p.m., which is the hottest time of the day, the difference in the PET between the two courtyards was only 0.2 °C (0% TCC); however, when the TCC



was 68%, the PET difference between the two courtyards was 0.6 °C. This suggests that courtyards with a high H/W ratio combined with trees have a greater cooling effect than courtyards with a low H/W ratio.

Figure 6. Average PET at 1.5 m height of each courtyard with tree canopy cover from 0% to 68% at different times of the day. (**a**) DZXX and (**b**) LX.

3.5. Sensible Heat Reduction

The results of a total sensible heat reduction for both courtyards, including all layers and time periods, are presented in Figure 7a,b. The total sensible heat reduction showed a significant and continuous increase with increasing the TCC in each courtyard. In the DZXX courtyard, the total sensible heat reductions for each TCC were 2.98×10^4 J/m² (21%), 3.64×10^4 J/m² (26%), 4.42×10^4 J/m² (31%), 4.98×10^4 J/m² (36%), 5.87×10^4 J/m² (47%), and 6.63×10^4 J/m² (68%), respectively. Similarly, in the courtyard of LX, the total sensible heat reductions for each TCC were 3.24×10^4 J/m² (21%), 3.92×10^4 J/m² (26%), 4.66×10^4 J/m² (31%), 5.30×10^4 J/m² (36%), 6.12×10^4 J/m² (47%), and 6.85×10^4 J/m² (68%), respectively. It is evident that when the TCC increased from 31% to 36%, the increase in the total sensible heat reduction in both courtyards decreased. Furthermore, Figure 7c,d show the percentage of the sensible heat reduction at different TCCs in the DZXX and LX courtyards for each height. As the TCC increased, the percentage of sensible heat reduction gradually increased at the lower levels (1.5–4.5 m) and decreased at the higher levels (11.0–14.5 m). This is because with the increase in the TCC, more trees were arranged in the center of the courtyard exposed to direct sunlight, resulting in a stronger cooling effect. However, due to the high level layer being more distance from the tree crown, the cooling ability of the tree canopy to that height is limited; therefore, the percentage of sensible heat reduction gradually decreased. In addition, the change in the percentage of sensible heat reduction in each level of the courtyards with low H/W ratios was more pronounced compared to that of the high H/W ratios.



Figure 7. Reduction and percentage of sensible heat at different heights. (**a**) Sensible heat reduction of DZXX; (**b**) sensible heat reduction of LX; (**c**) percentage of sensible heat reduction at different heights in DZXX; (**d**) percentage of sensible heat reduction at different heights in LX.

4. Discussion

The influence of coverage of urban green spaces on mitigating the thermal environment has been widely recognized at the city to the neighborhood scale; however, few studies have focused on the cooling effects of vegetation at the courtyard scale [74–76]. In the present study, we analyzed the cooling effects of different TCCs in relation to courtyards with different H/W ratios. Consequently, trees planted in courtyards with high H/W ratios had a larger cooling effect during the hottest period of the day compared to courtyards with low H/W ratios. The results of this study were similar to the finding of Randa Mohamed Ahmed Mahmoud and Amr Sayed Hassan Abdallah, who investigated the effect of outdoor shading a narrow courtyard with a H/W ratio of 0.7 compared to a wide courtyard with a H/W ratio of 0.4 [77]; however, it is worth noting that the academic buildings they surveyed were only 10 m high and enclosed on three sides, which could lead to different shadowing effects due to varying building heights and enclosure forms [41,78].

Moreover, Li et al. found that in residential areas with a building height of 33 m, a total sensible heat reduction of 7.08×10^4 J/m² was achieved with a 45% canopy coverage [70];

however, one of the findings of the present study is that the total sensible heat reduction for 47% TCC in courtyards with a high H/W ratio (0.9) was $5.87 \times 10^4 \text{ J/m}^2$, while the total sensible heat reduction in courtyards with a low H/W ratio (0.7) was $6.12 \times 10^4 \text{ J/m}^2$. This indicates that the lower the H/W ratio of a courtyard, the greater the sensible heat reduction achieved by planting trees. Additionally, when compared to outdoor open spaces, an increase in TCC in semi-outdoor spaces results in smaller cooling effects. This can be attributed to the higher percentage of building shadows in courtyards with higher H/W ratios. Furthermore, previous studies have also shown that trees located in building shadows have weaker cooling effects than those exposed to direct solar radiation [79–81]. In addition, It is essential to consider tree height as a significant factor affecting the reduction in sensible heat at different height layers; therefore, when planning green spaces in the built environment, the selection of tree species should take into account not only the leaf area index (LAI) value but also the tree height to optimize the cooling benefits.

This research does have certain limitations that should be acknowledged to better interpret the results. Firstly, the study assumed a uniform arrangement of trees in each courtyard, which may not represent the real-world diversity of tree distribution in courtyards. Future studies could consider more realistic scenarios with varied tree arrangements to better reflect the actual urban greenery patterns. Secondly, this study focused solely on the impact of tree canopy coverage on the thermal environment and sensible heat reduction during the summer season. As climate conditions and vegetation responses vary across different seasons, it would be beneficial to conduct further research exploring the cooling effects of different TCCs and tree species in various seasons throughout the year. Finally, from the perspective of site selection, our study only focused on two typical courtyards in Guangzhou. The cooling effect of trees also varies in cities located in different climates because the surface thermal fluxes are related to solar radiation [82]. Other types of courtyards should also be considered, because different dominant courtyard forms are found in different cities [83,84].

Despite these limitations, the study provides valuable insights into the cooling potential of the tree canopy coverage in academic building courtyards with different H/W ratios under hot-humid climate conditions. The findings contribute to the understanding of how urban green spaces can play a role in enhancing thermal comfort and mitigating urban heat island effects at the courtyard scale, which has been less explored in previous research.

5. Conclusions

This study presents the findings of an investigation into the impact of varying tree canopy coverage on the cooling of courtyards with different height-to-width (H/W) ratios, achieved by combining modeling with on-site measurements. The research was conducted in two similar academic buildings and their courtyard H/W ratios were 0.9 and 0.7. The results showed: (1) Arranging trees in courtyards with different H/W ratios has different effects, which produces variations in the microclimate. During the hottest period of the day, the PET value of courtyards with high H/W ratios decreases by up to 0.6 °C compared to courtyards with low H/W ratios. (2) Arranging trees in courtyards with different H/W ratios has different H/W ratios has different effects for sensible heat reduction. The maximum difference between the courtyards in this study with low H/W ratios and courtyards with high H/W ratios was 0.25×10^4 J/m². Some suggestions for good thermal environment in the local climate are:

- 1. Incorporate trees strategically: consider the strategic placement of trees in courtyards, particularly in courtyards with high H/W ratios, as they significantly contribute to cooling and improving microclimatic conditions.
- 2. Optimize tree canopy coverage: carefully select an appropriate percentage of tree canopy coverage to achieve the desired cooling effect, taking into account the specific conditions of each courtyard.
- 3. Select suitable tree species: in addition to considering the leaf area index (LAI) values, carefully choose tree species based on their height, as it significantly influences the sensible heat reduction at different height layers.

This study offers valuable insights into the distinct effects of trees on human thermal comfort and heat dynamics in courtyards of academic buildings with varying H/W ratios. These findings can be instrumental for university planners and designers in formulating comprehensive guidelines for courtyard design in academic buildings.

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