



Emission of Volatile Organic Compounds in Crumb Rubber Modified Bitumen and Its Inhibition by Using Montmorillonite Nanoclay

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Abstract: Bitumen emits a large amount of volatile organic compounds (VOCs) during the production and construction of asphalt mixture, which can cause both environmental hazards and health risks. In this study, a setup was designed to collect the VOCs released by base and crumb rubber-modified bitumen (CRMB) binders and their composition was characterized by thermal desorption-gas chromatography-mass spectrometry (TD-GC-MS). Next, organic montmorillonite (Mt) nanoclay was added into CRMB binder and its inhibiting effect on the VOCs emission of the binder was investigated. Finally, the VOCs emission models for the CRMB and Mt-modified CRMB (Mt-CRMB) binders were established according to reasonable assumptions. The results indicated that the VOCs emission of CRMB binder was 3.2 times larger than that of the base binder. Due to its intercalated structure, the nanoclay can reduce the VOCs emission of CRMB binder by 30.6%. Especially, its inhibition effects on alkanes, olefins, and aromatic hydrocarbons were more significant. After finite element verification, the established model based on the Fick's second law can describe the emission behavior of CRMB and Mt-CRMB binders well. Overall, the Mt nanoclay can be used as an effective modifier to inhibit the VOCs emission of CRMB binder.

Keywords: VOCs; crumb rubber; bitumen; organic montmorillonite; inhibition

1. Introduction

Every year, over 1.6 billion new tires and around 1 billion waste tires are generated [1]. Approximately 18 million tons of waste tires in China are produced yearly, but their recycling rate is less than 40% [2]. The accumulation of a large number of waste tires occupies land resources, and it has the risk of auto-ignition, which can produce a large amount of harmful smoke [3]. At present, a broad application of the waste tires is to produce crumb rubber (CR) powder to modify bitumen binder. Many studies have shown that asphalt mixture with crumb rubber-modified bitumen (CRMB) binder can effectively improve the resistance to the high-temperature deformation, fatigue performance, and rheological performance [4–7].

Bitumen can emit large amounts of volatile organic compounds (VOCs) during the production of asphalt mixture and the construction of asphalt pavement [8]. The CRMB mixture needs a higher production temperature, and its VOCs emission is larger than the traditional hot-mix asphalt [9]. Bitumen is composed of saturate, aromatic, resin, and asphaltene. Among them, aromatic is the most harmful and contains benzene, naphthalene, anthracene, phenanthrene, pyridine, acridine, carbazole, phenol, and other volatile substances [10]. With long-term exposure to such an environment, the harmful substances will enter the human body through skin contact and the respiratory tract, seriously harming the health of humans [11,12]. The influence of bitumen fumes, including VOCs, is attracting



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). more and more attention. The International Agency for Research on Cancer listed bitumen fumes as a suspected carcinogen in 1987 [13]. In 2015, China implemented new regulations (GB31570-2015), which set the emission standard of asphalt fumes at 20 mg/m³ [14,15]. Therefore, the emission problem of bitumen VOCs is one of the important factors limiting the further expansion of bitumen applications.

Lots of research has been carried out on how to inhibit the emission of bitumen VOCs. Temperature is an important factor affecting the VOCs emission of bitumen [16]. Compared with the traditional hot-mix asphalt (HMA), the warm-mix asphalt (WMA) technology can reduce the construction temperature by 20–40 °C, down to 100–140 °C [17]. The WMA containing the CR powder can effectively reduce polycyclic aromatic hydrocarbon emissions [18]. However, the warm-mix agents decreased the low-temperature cracking and moisture damage resistances of the asphalt mixture [19]. The nano-sized calcium carbonate and styrene butadiene styrene copolymer (SBS) can be used to absorb the VOCs emission of bitumen [20]. However, SBS polymer is susceptible to aging and degradation at high temperatures, which will reduce the inhibition effect of SBS on bitumen VOCs [21,22]. In addition, some inorganic materials such as zeolite, layered double hydroxides, and expanded graphite have been proven to be used as asphalt VOCs inhibitors, but the compatibility between the inorganic materials and asphalt is poor, tending to cause segregation problems at high temperatures [23–25].

Montmorillonite (Mt) is a widely available and inexpensive mineral. Its unit cell has a crystal structure comprising a 2:1 layered silicate, two silicon-oxygen tetrahedron layers, and a sandwiched layer of aluminum-oxygen octahedrons [26,27]. The surface of its silicate lamellar layer is negatively charged and is composed of accumulation by electrostatic interaction between layers [28]. Montmorillonite has unique one-dimensional layered nanostructures and cation exchange properties, which makes it possible to modify and expand the application field [29,30]. Modification by organic compounds can significantly improve its utilization rate. It has been reported that organic Mt can improve the anti-aging performance of bitumen, and the anti-aging performance was better than SBS-modified bitumen when the content exceeded 3% [31]. In addition, the physical and chemical stability of montmorillonite sheet can further enhance the flame-retardant performance of polymers [32]. Moreover, 5 wt.% Mt containing alkyl surfactants reduced VOCs emissions of base bitumen by more than 50% through interlayer restriction of volatilization of the light components of the bitumen [33]. Organic Mt with a particle size greater than 200 mesh size significantly reduced the types and quantities of SBS-modified bitumen VOCs [34]. The research above indicates that Mt can not only effectively improve the performance of bitumen, but also has great potential in inhibiting VOCs emission. However, using Mt to inhibit the VOCs emission of CRMB has not been reported.

This study aimed to characterize the VOCs emission of CRMB binder and evaluate the effect of Mt nanoclay on its inhibition. Firstly, a homemade setup was used to collect the VOCs of base and CRMB binders during the heating process, and their composition was characterized. Next, nanoclay was used to modify the CRMB binder, and its inhibition effect on the VOCs emission of the CRMB binder was evaluated. Finally, based on the Fick's second law, the VOCs emission models for the CRMB and Mt-modified CRMB (Mt-CRMB) binders were established.

2. Experimental

2.1. Materials

Base bitumen (IRPC-70) with a penetration grade of 70 was imported from Thailand and used in this study. The basic properties of the base bitumen are presented in Table 1.

Properties	Values	Standard
Penetration at 25 $^{\circ}$ C (0.1 mm)	66	ASTM D5
Softening point (°C)	48	ASTM D36
Ductility at 15 °C (cm)	181	ASTM D113
Viscosity at 60 °C (Pa·s)	166	ASTM D4402
Viscosity at 135 °C (Pa·s)	0.54	ASTM D4402

Table 1. Basic properties of base bitumen.

One waste tire from a passenger car was chosen to produce the CR powder. Its preparation process was as follows: first, the electric grinder was adopted to grind the tread part of the waste tire to produce the CR powder; next, the magnet was used to remove iron impurities; then, the CR powder was sieved and collected with a typical particle size between 40 and 60 mesh number (i.e., $250-425 \ \mu m$) to be used in this study; finally, it was washed by the water to remove other impurities (e.g., dust) and dried at 60 °C in the oven for 12 h.

The organic Mt produced by Zhejiang Fenghong Clay Chemical Co. Ltd. (Huzhou, China) was used to modify the CRMB binder, and distearylammonium chloride was used as the surfactant with the content of 9%. The physical properties of montmorillonite are presented in Table 2.

Table 2. Physical properties of montmorillonite.

Properties	Values		
Basal spacing (nm)	1.3		
Density (g/cm^3)	1.7538		
Appearance	White powder		
Weight content of surfactant (%)	9		

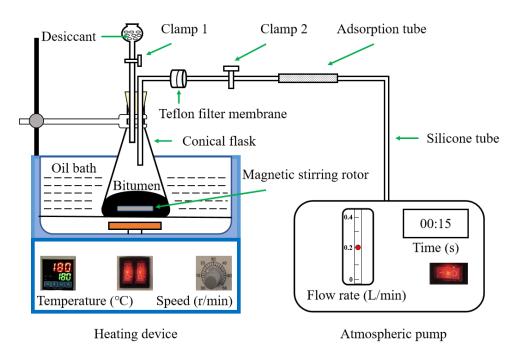
2.2. Modified Bitumen Preparation

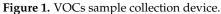
During the preparation of the CRMB or Mt-CRMB binders, 250 g of base binder was melted and poured into a cylindrical container on the heating plate. Then, 45 g of CR powder (18% by weight) was added to the base binder, dispersing with a low-speed mixer (JJ-1, Shanghai Loikaw Instrument) at 200 rpm for 10 min, at a temperature of 150 °C. For the Mt-CRMB binder, 10 g of Mt (4% by weight) was simultaneously added with the CR powder into the base binder. Next, the temperature was increased to 180 °C, and the binder was sheared with a high-speed shearing mixer (ESR-500, Shanghai ELE Mechanical and Electrical Equipment, Shanghai, China) at 4500 \pm 500 rpm for 1 h. All samples were cooled to room temperature and stored for further testing. More information about the bitumen binder modification process in this study can be found in the previous research [33].

2.3. Test Methods

2.3.1. VOCs Collection Methods

The VOCs sample collection device is shown in Figure 1. Two VOCs sampling methods were used in this study. Method 1 was used to compare the VOCs characteristics of CR powder, base, and CRMB binders, by opening or closing the clamps, and Method 2 was not only used to characterize the VOCs emission of the binders at different heating times, but also could be used to calculate the VOCs emission rates in order to understand the entire VOCs emission behavior. The specific collection processes for these two methods are outlined below.





Method 1: First, 50 g of binder or the CR powder sample was put into the conical flask, and Clamps 1 and 2 were closed (see Figure 1). When the temperature of the heating device rose to 180 °C, the magnetic stirring switch was turned on and the temperature was held for 10 min. Then, the two clamps were opened, and the VOCs were adsorbed into the ATD (automatic tube dispenser) by using an atmospheric pump at a gas flow rate of 0.2 L/min for 15 s.

Method 2: The CRMB binder or Mt-CRMB binder with the weight of 50 g was poured into the conical flask (see Figure 1). As shown in Figure 2, the VOCs at 180 $^{\circ}$ C were collected at five sampling points (i.e., 10, 30, 60, 90, and 120 min) to simulate the VOCs release characteristics of the asphalt mixture during the process of mixing, transporting, and paving. The collection time for each point was 15 s, with a flow rate of 0.2 L/min using the pump. Before each collection, the clamps were closed for 10 min to preserve enough VOCs to be absorbed by the ATD.

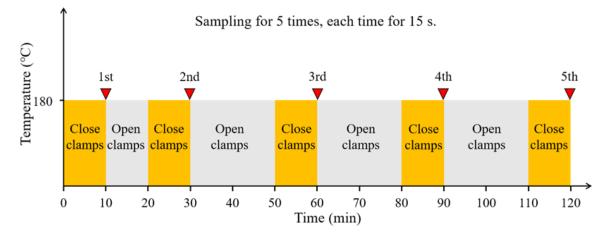


Figure 2. Operation process for Method 2 (sampling five times).

2.3.2. VOCs Characterization

Atomx P&T-Agilent 7890B-5977B thermal desorption-gas chromatography-mass spectrometry (TD-GC-MS, Agilent, Santa Clara, CA, USA) was used to characterize the VOCs emission of the binder. The gas temporarily adsorbed in the automatic tube dispenser (ATD, PerkinElmer, Waltham, MA, USA) was desorbed in the thermal desorption system and then transferred to the ultra-inert capillary column ($30 \text{ m} \times 250 \text{ mm} \times 0.25 \text{ mm}$) using high-purity helium (\geq 99.999%) at a flow rate of 40 mL/min. The GC-MS system was kept at 30 °C for 3 min and then heated up to 200 °C at 11 °C/min for 3 min. Finally, it was kept at 280 °C for 5 min. The ion-source temperature was maintained at 230 °C, and the MS detector (Agilent, Santa Clara, CA, USA) was operated in full-scan electron ionization (EI) mode, where data over 35–400 m/z were acquired [35,36].

2.3.3. X-ray Diffraction (XRD) Test

A D/Max-RB X-ray diffractometer (Rigaku, Tokyo, Japan) was used to analyze the structural changes of the organic montmorillonite in the CRMB binder, with the conditions: Cu K α rays ($\lambda = 1.54184$ Å), the tube voltage of 40 kV, the tube current of 40 Ma, the step size of 0.02°, the scanning range of 1–10° (2 θ), and the scanning rate of 5°/min.

3. Results and Discussion

3.1. VOCs Composition of Base and CRMB Binders

Figure 3 shows the GC-MS chromatograms of VOCs emitted by the base binder, CRMB binder, and pure CR powder. Based on the NIST database, there were 123 organic compounds detected in the base binder VOCs. Commonly, the bitumen VOCs can be classified into alkanes (ALK), olefins (OLE), hydrocarbon derivatives (HYD), aromatic hydrocarbons (ARH), and aromatic hydrocarbon derivatives (ARHD). Among these compounds, there were 49 ALKs, 31 OLEs, 19 HYDs, 24 ARHs, and 0 ARHD. It was indicated that most compounds in the base binder VOCs belonged to the ALK and OLE.

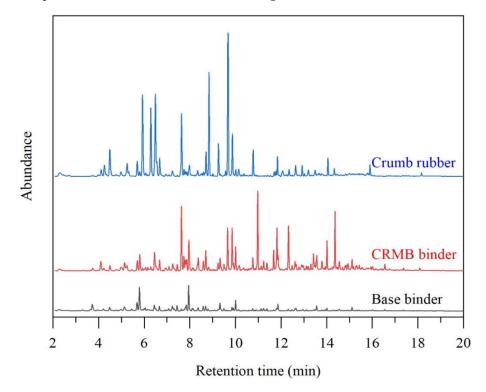


Figure 3. VOCs GC-MS chromatograms of CR powder, base, and CRMB binders.

For the CR powder, 116 VOCs were detected, containing 17 ALKs, 29 OLEs, 62 HYDs, 6 ARHs, and 2 ARHDs. It was indicated that the hydrocarbon derivatives dominated the VOCs of CR powder. Meanwhile, there were two aromatic hydrocarbon derivatives.

The GC-MS results indicated that there were 144 compounds in the CRMB binder VOCs. Among them, there were 42 ALKs, 43 OLEs, 28 HYDs, 29 ARHs, and 2 ARHDs. Compared with the base binder VOCs, all the species numbers increased, except in the ALE. Maybe some alkane compounds in the binder were absorbed by the rubber, and the ALE

volatilization decreased. Two aromatic hydrocarbon derivatives were detected, possibly originating from the CR powder with the same VOCs.

In terms of ionic peak intensities, the CR power, base binder, and CRMB binder VOCs were significantly different. For the CR powder VOCs, the abundances of methyl acrolein, methyl vinyl ketone, benzene, 2-ethenyl-2-butenal, and methyl isobutyl ketone were larger. For the base binder VOCs, the abundances of n-hexane and heptane were larger. For the CRMB VOCs, the abundances of benzene, 4-ethenyl-cyclohexene, and D-limonene were larger.

Figure 4 shows the distribution of VOCs species for the CR powder, base, and CRMB binders. Three areas were defined: Area 1 meant the overlap of 21 VOCs among the CR powder, base, and CRMB binders, Area 2 meant 51 joint VOCs between the base and CRMB binders, and Area 3 represented 14 joint compounds between the CR powder and the CRMB binder. It was noted that 51 VOCs in the base binder and 83 VOCs in the CR powder were not detected in the CRMB binder. However, there were 58 new VOCs in the CRMB binder.

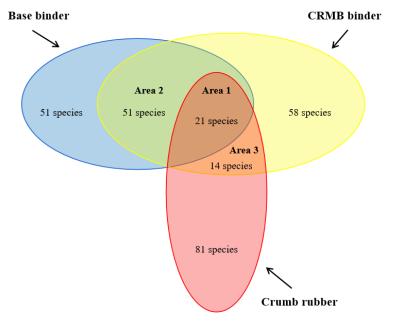


Figure 4. VOCs species overlap for crumb rubber, base, and CRMB binders.

Figure 5 shows the peak area changes of 21 compounds in Area 1 based on the GC-MS chromatograms of the CRMB binder. It indicated that except for pentane and n-hexane, the peak areas of the other 19 compounds increased compared with the base binder. Among them, the peak areas of benzene, cyclohexene, toluene, m-xylene, p-xylene, and propyl benzene increased by 28 times, 10 times, 10 times, 14 times, 17 times, and 11 times, respectively. It can be seen that because the waste CR powder itself contains these compounds, adding the CR powder to the base binder will have a direct impact on the emissions of these compounds in VOCs.

The CR powder mainly introduced 14 VOCs in Area 3. Among them, ethanol, methyl isobutyl ketone, ethyl acetate, 1-pentanol, and D-limonene are often used as essential solvents in the rubber tire. The 4-ethenyl-cyclohexene and styrene are critical raw materials for synthesizing rubber. Benzothiazole was used as the rubber vulcanization accelerant, while 2-methyl-furan, heptanal, octanal, nonanal, (E)-6-dodecane, and 2-ethenyl-2-butenal were used as the intermediates in the rubber synthesis.

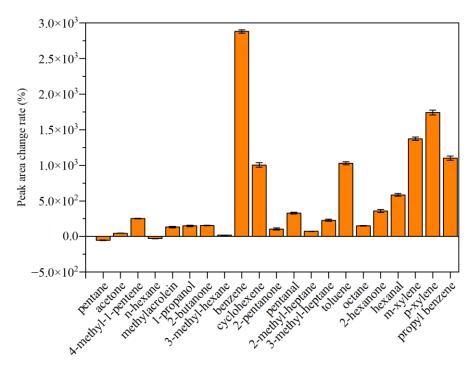


Figure 5. Peak area changes of 21 compounds in Area 1 based on the GC-MS chromatograms of the CRMB binder.

Based on the previous research [37–39], 23 normally used VOCs were selected as the fingerprint compounds for the CRMB binder (see Table 3). Among them, there were 12 species from Area 1, 5 from Area 2, and 6 from Area 3.

Area Code No.		Retention Time (min)	Compounds	Standard Curve	
	1	3.743	Pentane	y = 6443x	
	2	4.499	Acetone	y = 34,348x	
	4	5.807	n-Hexane	y = 32,620x	
	5	5.924	Methacrolein	y = 43,341x	
	8	7.451	3-methyl-hexane	y = 57,274x	
1	9	7.632	Benzene	y = 116,197x	
1	10	7.958	Heptane	y = 82,427x	
	11	9.326	2-methyl-heptane	y = 58,003x	
	13	9.854	Toluene	y = 137,374x	
	14	10.006	Octane	y = 160,012x	
	16	11.680	m-Xylene	y = 74,470x	
	17	11.825	p-Xylene	y = 137,036x	
	3	5.143	2-methyl-pentane	y = 41,944x	
	7	6.453	Butanal	y = 33,394x	
2	19	14.016	Mesitylene	y = 138,233x	
	21	15.115	Undecane	y = 124,317x	
	22	17.369	Naphthalene	y = 466,879x	
	6	6.288	2-methyl-furan	y = 58,003x	
	12	9.656	Methyl Isobutyl Ketone	y = 146,885x	
2	15	10.974	4-ethenyl-cyclohexene	y = 70,311x	
3	18	12.331	Styrene	y = 92,293x	
	20	14.367	D-Limonene	y = 121,411x	
	23	18.080	Benzothiazole	y = 24,376x	

Table 3. The 23 VOCs fingerprint compounds from 3 areas and their standard curves for the GC-MS.

The external method was used to obtain the standard curve of the fingerprint compound. First, a standard solution was prepared by mixing 23 fingerprint compounds in the ethanol solvent. Each compound had 5, 10, 25, 50, and 100 ppm concentrations. For other non-fingerprint compounds, the standard curve of toluene was used [9]. After the GC-MS test, the standard curve describing the relationship between the peak area and mass of each compound was obtained as follows:

$$n_i = \frac{S_i}{k_i} \tag{1}$$

where, m_i is the mass of fingerprint compounds, ng, S_i is the peak area of fingerprint compounds, and k_i is the slope of the standard curve for fingerprint compounds, ng⁻¹.

The total amount of bitumen VOCs emission was calculated as follows:

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$$\mathbf{m} = \sum_{i=1}^{n} m_i + \frac{S_t - \sum S_i}{k_{tol}}$$
(2)

where, m is the total amount of bitumen VOCs emission, ng, n is the number of fingerprint compounds, S_t is the total peak of all VOCs, and k_{tol} is the slope of the standard curve measured by the standard toluene solution prepared in this study, ng⁻¹.

Figure 6 shows the VOCs emission amount of each fingerprint compound. The total base binder VOCs amount was 1306 ng/g. However, this amount for the CRMB binder VOCs was 4180 ng/g, three times that of the base binder. It was indicated that the addition of CR significantly increased the total emission of bitumen VOCs. Two lightweight compounds (No. 1 pentane and No. 4 n-hexane) in the CRMB binder VOCs had a lower emission amount, decreasing by 57.47% and 31.79%, respectively. The reason was that the CR powder absorbed part of the lightweight compounds in the base bitumen, thereby reducing their emissions. However, most fingerprint compounds had an increased emission. The emission amount of benzene, toluene, m-xylene, p-xylene, and mesitylene in the CRMB binder VOCs increased by 34, 11, 20, 15, and 9 times, respectively. It indicated that the CR powder significantly influenced the ARHs emission.

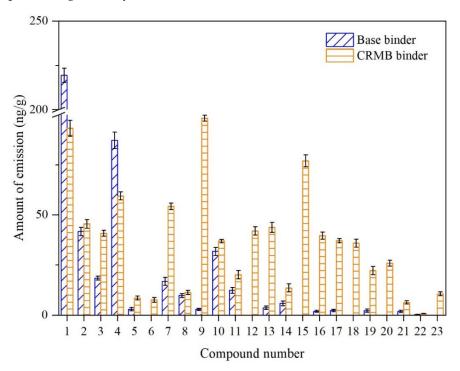


Figure 6. Emission comparison of each VOC fingerprint compound between the base and CRMB binders.

3.2. Inhibition Effect of Mt on the VOCs Emission of CRMB Binder

Figure 7 shows the VOCs GC-MS chromatograms of the CRMB and Mt-CRMB binders. The results indicated that Mt-CRMB VOCs had 108 compounds, 25% less than the CRMB VOCs, which had 144 compounds. It can be easily observed that most fingerprint com-

pounds of the Mt-CRMB VOCs had a smaller peak than that of the CRMB VOCs. Calculated by Equation (2), the total emission of the Mt-CRMB binder was 2901 ng/g, 30.6% less than that of the CRMB binder.

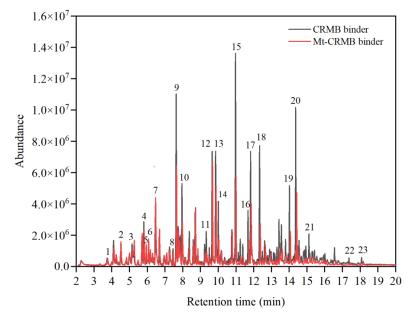


Figure 7. VOCs GC-MS chromatograms of CRMB and Mt-CRMB binders.

Figure 8 compares the emission amount of each VOC fingerprint compound between CRMB and Mt-CRMB binders. Due to the addition of Mt, 19 compounds had a decreased emission. Among them, the emission of compounds Nos. 3, 9, 10, 11, 14, 15, 16, 17, 18, 19, 20, 21, 22, and 23 was significantly reduced by more than 30%. These compounds belonged to the ALK, OLE, and ARH. However, the inhibition effect of Mt on the compounds of No. 2 (acetone), No. 5 (methacrolein), No. 6 (2-methyl-furan), and No. 7 (butanal) was not good.

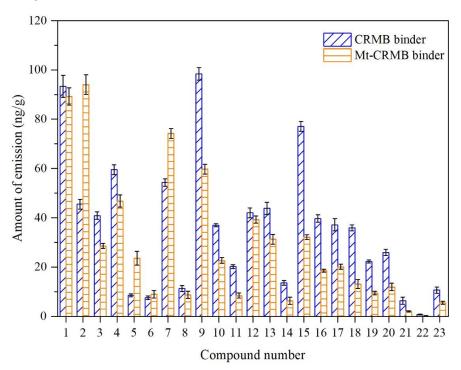


Figure 8. Emission amount comparison of each VOC fingerprint compound between CRMB and Mt-CRMB binders.

Figure 9 shows the VOCs GC-MS chromatograms of the CRMB and Mt-CRMB binders at different retention times, following sampling Method 2 (see Figure 2). The characteristic peak abundance of the CRMB and Mt-CRMB VOCs changed with the extension of the heating time. At Time 2 (i.e., 30 min), the peak abundance reached the maximum. It meant that the CRMB and Mt-CRMB binders at 180 °C had the most VOCs emission after heating for half an hour.

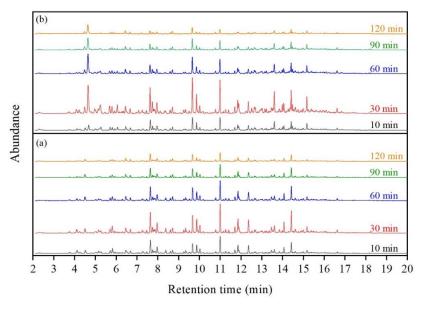


Figure 9. VOCs GC-MS chromatograms of (a) CRMB and (b) Mt-CRMB binders at different times.

Figure 10 shows the species numbers of CRMB and Mt-CRMB VOCs as a function of the heating time. As indicated, the species number for both binders had a similar change trend. At the same time, the Mt-CRMB VOCs had a lower number. Both had a very close maximum number at 30 min. With the extension of the heating time, the species number gradually decreased. At 120 min (i.e., the fifth sampling), the Mt-CRMB binder only had 79 VOCs species, reduced by 39% compared with the maximum value. However, this number for the CRMB binder only decreased by 27%. It indicated that adding Mt could effectively reduce the number of the VOCs of the CRMB binder.

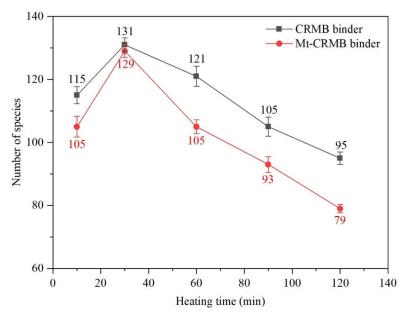


Figure 10. VOCs species number comparison between CRMB and Mt-CRMB binders at different times.

Figure 11 shows the structural change of Mt in the CRMB binder at different times. For the time at 0 min, there were two diffraction peaks. According to the Bragg equation, the basal spacing of Mt was 1.32 nm at 6.62° and 5.25 nm at 1.68°. It meant that parts of Mt remained the original structure, but some showed an intercalated structure with a basal spacing increased by almost three times. The reason was that some small bituminous molecules entered the interlayer of the Mt, forming an intercalation structure [40]. The structure limited the release of bitumen VOCs and reduced their escape paths.

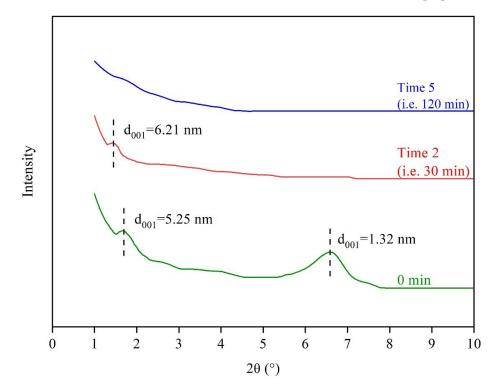


Figure 11. XRD spectrum of Mt-CRMB binder at different times.

For the time at 30 min, there was only one diffraction peak at 1.42°. The peak for the original Mt at 6.62° disappeared, probably due to the continuous stirring of the magnetic rotor improving the exfoliated nanoclay. According to the Bragg equation, the basal spacing of Mt increased from 5.25 nm to 6.21 nm. For the time at 120 min, there was no prominent diffraction peak. The reason was that most Mt layers were exfoliated due to the stirring function. This exfoliation structure improved the inhibition effect on the VOCs emission, with the smallest species number at 120 min.

3.3. VOCs Emission Model of Bitumen

3.3.1. Establishment of Model

Figure 12 shows the schematic diagram of VOCs emission from bitumen. Generally, the VOCs emission consists of internal molecular diffusion in the material, partition on the air-material interface, and external convective mass transfer in the ambient air [41]. Five assumptions were established in the model establishment: the initial concentration of VOCs was uniformly distributed, there was no chemical reaction during the VOCs diffusion, the concentration gradient of VOCs was considered to be the only mass transfer force, the equilibrium condition existed between the material surface and the air boundary layer, and the partition on the material-air interface can be ignored. Under the above assumptions, the bitumen VOCs emission can be regarded as one-dimensional, and its emission rate measured in the experiment equaled that at the upper surface of bitumen.

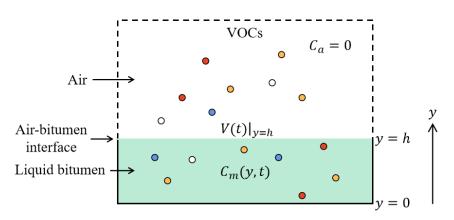


Figure 12. Schematic diagram of VOCs emission from bitumen into the air.

The VOCs diffusion in bitumen follows Fick's second law and can be described by the unsteady diffusion equation:

$$\frac{\partial C_m}{\partial t} = \frac{\partial}{\partial y} \left(D_m \frac{\partial C_m}{\partial y} \right), \ 0 \le y \le h$$
(3)

where, C_m is the concentration of each VOC in bitumen, $\mu g/m^3$, D_m is the diffusion coefficient of each VOC in bitumen, m^2/s , and *h* is the thickness of the bitumen sample, m. The initial condition of VOCs is given as:

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$$C_m|_{t=0} = C_0, \ 0 \le y \le h \tag{4}$$

where, C_0 is the initial concentration of each VOC inside the bitumen, $\mu g/m^3$, and *t* is the heating time, s.

Since the bitumen samples will not penetrate the glass substrate, the concentration gradient is $0 \mu g/m^4$ (i.e., no mass flux) on the bottom boundary. It means that:

$$\left. \frac{\partial C_m}{\partial y} \right|_{y=0} = 0 \tag{5}$$

Since the operation process shown in Figure 2 was designed to simulate the open environment in the process of bitumen preparation, transportation, and spreading in the actual situation, the spread of VOCs emitted from bitumen to the external environment is infinite. Therefore, the assumption of zero concentration on the upper surface of the sample is valid in this case, as follows:

$$C_m|_{y=h} = 0 \tag{6}$$

When the time, *t*, is long enough, the model for the instantaneous emission rate of VOCs based on the Laplace transform can be expressed as [41]:

$$V(t) = \frac{2D_m C_0}{h} e^{\frac{-D_m \pi^2}{4h^2}t}$$
(7)

Equation (7) can also be expressed as:

$$lnV(t) = ln\left(\frac{2D_mC_0}{h}\right) - \frac{D_m\pi^2}{4h^2}t$$
(8)

V(t) can be obtained from the experiment and calculated by the following Equation:

$$V(t) = \frac{m_e}{St_c} \tag{9}$$

where, m_e is the mass of each compound measured in the experiment, μg , S is the area of the upper surface of the sample, m², and t_c is the closed time before each sampling, min.

Two parameters, C_0 and D_m , can be obtained through the linear curve fitting based on Equation (8).

Figure 13 shows the total VOCs emission rates of CRMB and Mt-CRMB binders, and both total emission rates of the two binders sharply increased before 30 min and then gradually decreased. The VOCs emission rates of CRMB and Mt-CRMB binders were close at 30 min. However, with the extension of the heating time, their VOCs emission rates were significantly different. At 120 min, this value of the Mt-CRMB binder decreased by 41% compared with CRMB. For the VOCs collection device, a hysteresis of heat transfer existed at the initial state, leading to the uneven distribution of the VOCs concentration inside the binder. Therefore, there was an emission peak at 30 min. After this time, the internal concentration tended to be uniform, and the emission of bitumen VOCs met Fick's law. Therefore, the emission rates at 30, 60, 90, and 120 min were used to fit the model of Equation (7).

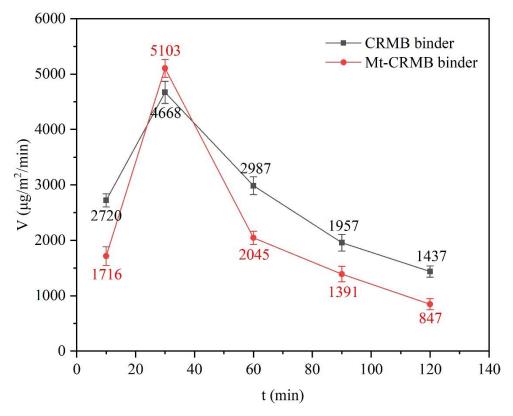


Figure 13. Total VOCs emission rates of CRMB and Mt-CRMB binders.

Table 4 presents the VOCs emission rate of each fingerprint compound. In comparison, the emission rates for all fingerprint compounds of the Mt-CRMB binder decreased at the same heating time, except for No. 12 and No. 21 compounds. It indicated that adding Mt significantly reduced the emission rate of most VOCs in the bitumen.

Table 5 presents the initial concentration, C_0 , and the diffusion coefficient, D_m , in the emission model for 23 fingerprint compounds of CRMB and Mt-CRMB binders. As indicated, C_0 for most compounds after the Mt modification decreased, except for undecane. The acetone had the highest C_0 of $2.033 \times 10^6 \,\mu\text{g/m}^3$, and this value decreased by 27% in the Mt-CRMB binder. Meanwhile, C_0 of 2-methyl-furan, 2-methyl-heptane, octane, and mesitylene decreased by 53%, 58%, 51%, and 51%, respectively. For most compounds, D_m was relatively stable after the Mt modification.

No.	Emission Rate (µg/m²/min)									
	Sampling Time for CRMB Binder					Sampling Time for Mt-CRMB Binder				
	1	2	3	4	5	1	2	3	4	5
1	117.00	160.73	99.80	63.50	45.32	46.52	111.93	44.42	35.73	33.12
2	92.65	142.55	129.52	111.15	72.33	53.28	139.05	88.20	75.12	53.47
3	33.50	44.68	27.95	17.85	12.03	13.85	43.35	15.48	8.27	5.10
4	54.98	79.20	45.92	29.37	21.05	20.52	52.52	21.47	15.63	11.23
5	12.22	18.32	15.58	12.38	10.80	8.72	16.17	10.40	8.68	7.23
6	4.78	9.32	8.23	6.72	5.93	3.08	8.73	4.68	4.05	2.95
7	26.68	46.28	38.48	29.18	27.80	21.62	44.07	26.00	20.27	19.37
8	8.75	14.13	8.77	5.78	4.12	3.85	11.00	4.37	3.02	1.70
9	64.10	98.18	64.57	45.12	35.60	34.90	83.05	28.52	19.17	10.42
10	28.97	39.13	23.53	15.65	12.27	13.60	28.93	12.50	9.17	6.93
11	13.32	23.43	14.48	9.28	6.30	4.52	13.05	5.32	3.40	1.88
12	29.72	52.68	38.22	27.48	21.58	26.30	72.45	33.83	23.50	14.33
13	26.67	43.55	27.17	16.47	10.82	16.42	39.88	15.24	8.85	4.08
14	7.73	13.32	8.43	5.48	3.93	3.28	8.88	3.92	2.72	1.83
15	48.85	83.82	56.92	37.22	25.50	24.37	64.00	27.27	17.98	8.83
16	22.37	37.70	24.22	14.97	9.92	10.92	26.78	10.33	6.83	3.35
17	21.93	37.07	24.28	15.47	10.50	9.48	22.83	9.25	6.32	3.27
18	18.38	30.13	18.88	11.17	7.05	8.00	18.42	6.93	4.47	2.08
19	13.30	23.73	15.60	10.08	6.88	6.08	13.60	6.32	4.52	2.52
20	14.37	29.52	18.43	12.68	8.70	7.38	19.47	9.02	6.47	3.52
21	5.28	10.48	6.65	4.23	2.97	7.60	18.62	8.65	6.03	3.18
22	0.37	0.67	0.48	0.30	0.22	0.25	0.50	0.30	0.23	0.15
23	5.77	9.18	6.60	4.50	3.47	2.07	3.65	3.28	3.53	2.07
Fotal SD	121.53	198.75	162.88	155.47	99.21	171.54	160.15	122.34	142.78	104.12

Table 4. Emission rate, V(t), of 23 fingerprint compounds for CRMB and Mt-CRMB binders at different times.

Table 5. The initial concentration, C_0 , and the diffusion coefficient, D_m , in the emission model for 23 fingerprint compounds of CRMB and Mt-CRMB binders.

No.	CRMB Binder			Mt-CRMB Binder			
	C ₀ (μg/m ³)	D _m (m ² /s)	R ²	C ₀ (μg/m ³)	D _m (m ² /s)	R ²	
1	1.355×10^{6}	$2.163 imes 10^{-8}$	0.9914	1.001×10^{6}	7.439×10^{-9}	0.6893	
2	$2.033 imes 10^6$	$1.607 imes10^{-8}$	0.8316	$1.479 imes10^6$	$1.086 imes10^{-8}$	0.9538	
3	$3.780 imes 10^5$	$3.182 imes10^{-8}$	0.9978	$2.135 imes 10^5$	2.229×10^{-8}	0.9540	
4	$6.198 imes 10^5$	$2.266 imes 10^{-8}$	0.9829	$3.144 imes 10^5$	$1.673 imes 10^{-8}$	0.8896	
5	$3.058 imes 10^5$	$1.302 imes 10^{-8}$	0.9865	$1.801 imes 10^5$	$8.930 imes 10^{-9}$	0.9151	
6	$1.734 imes 10^5$	$1.592 imes10^{-8}$	0.9849	$8.160 imes10^4$	7.839×10^{-9}	0.8928	
7	$7.445 imes 10^5$	$1.247 imes10^{-8}$	0.9155	$4.265 imes 10^5$	$9.344 imes10^{-9}$	0.7946	
8	$1.198 imes 10^5$	$2.919 imes10^{-8}$	0.9917	$7.308 imes 10^4$	$2.089 imes 10^{-8}$	0.9513	
9	$9.257 imes 10^5$	$2.718 imes10^{-8}$	0.9784	$4.840 imes10^5$	$3.094 imes10^{-8}$	0.9399	
10	3.250×10^5	$1.974 imes10^{-8}$	0.9657	$1.888 imes 10^5$	$1.490 imes10^{-8}$	0.8808	
11	$1.959 imes10^5$	$2.978 imes10^{-8}$	0.9966	$8.314 imes10^4$	2.230×10^{-8}	0.9693	
12	5.721×10^5	$2.509 imes10^{-8}$	0.9932	$5.173 imes 10^5$	$1.524 imes10^{-8}$	0.9660	
13	$3.651 imes 10^5$	$3.385 imes10^{-8}$	0.9983	2.769×10^{5}	$3.849 imes10^{-8}$	0.9711	
14	$1.144 imes 10^5$	$2.194 imes10^{-8}$	0.9925	$5.576 imes 10^4$	$2.024 imes 10^{-8}$	0.9378	
15	7.753×10^5	$3.009 imes10^{-8}$	0.9993	$4.629 imes10^5$	$3.344 imes10^{-8}$	0.9767	
16	3.260×10^5	$3.513 imes10^{-8}$	0.9988	1.906×10^5	2.255×10^{-8}	0.9672	
17	$3.305 imes 10^5$	$3.288 imes 10^{-8}$	0.9988	$1.661 imes 10^5$	2.125×10^{-8}	0.9648	
18	$2.492 imes 10^5$	$3.679 imes10^{-8}$	0.9991	$1.293 imes10^5$	$2.453 imes10^{-8}$	0.9708	
19	$2.125 imes 10^5$	$2.848 imes10^{-8}$	0.9990	$1.047 imes10^5$	$2.114 imes 10^{-8}$	0.9680	
20	2.579×10^{5}	$2.888 imes 10^{-8}$	0.9950	$1.489 imes10^5$	$1.946 imes10^{-8}$	0.9687	
21	$9.030 imes10^4$	$2.148 imes10^{-8}$	0.9949	1.406×10^5	$2.981 imes 10^{-8}$	0.9746	
22	$6.363 imes 10^3$	$2.087 imes10^{-8}$	0.9948	$4.483 imes10^3$	$1.874 imes10^{-8}$	0.9700	
23	$9.552 imes 10^4$	$1.669 imes10^{-8}$	0.9929	5.750×10^4	9.606×10^{-9}	0.4464	

3.3.2. The Model Validation

For validating the emission model of Equation (8), the Concentration Field of the PDEtoolbox in MATLAB software was used to construct the finite element model (FEM) for four typical components (toluene, styrene, benzothiazole, and methyl isobutyl ketone) in the CRMB and Mt-CRMB binders. In this FE model, a rectangle was selected as the model's shape and gridded. The boundary (left, right, and bottom) conditions were set with the diffusion concentration gradient equal to $0 \ \mu g/m^4$. The parameters of C_0 and D_m in Table 5 were input into the software to obtain the diffusion model of VOCs inside bitumen. Figure 14 shows the two-dimensional cloud image of benzothiazole diffusion in the Surface gradually increased. As the volatilization time increased, the diffusion flux at the upper interface gradually decreased.

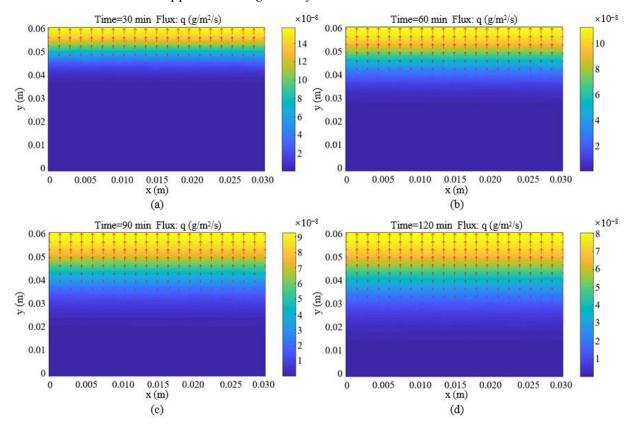


Figure 14. Two-dimensional cloud images of benzothiazole diffusion in CRMB binder at (**a**) 30 min, (**b**) 60 min, (**c**) 90 min, and (**d**) 120 min.

Figure 15 shows the emission rate of four typical compounds at the upper interface based on the FEM and the experiment. As indicated, the emission rate gradually decreased with the increase in the heating time. The emission curve of these compounds in the CRMB and Mt-CRMB binders agreed well with the experimental data. In comparison, the CRMB binder better fit the model and the experiment than the Mt-CRMB. It was observed that the data at 90 min and 120 min differed more from the curve than at 30 min and 60 min. The reason could be that the bitumen gradually aged, hindering the VOCs emission. Although only four fingerprint compounds were used for the verification, it was still proven that the analytical solutions derived from Equations (3)–(6) were reasonable and can be used to describe the emission behavior of bitumen very well. This model can provide a concise and efficient understanding of bitumen VOCs emission behavior and lays a solid foundation for further deepening the model (considering more influencing factors) in future studies.

120

100

80

60

40

20

0

120

100

80

60

40

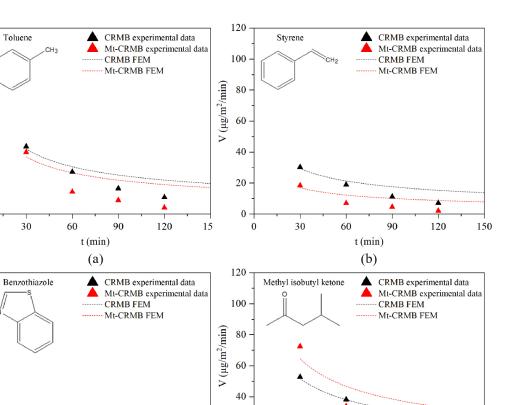
20

0

 $V (\mu g/m^2/min)$

0

V (µg/m²/min)



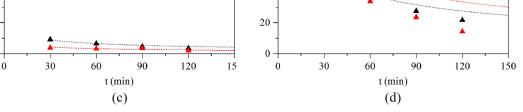


Figure 15. Emission rate of four typical compounds of (**a**) toluene, (**b**) styrene, (**c**) benzothiazole, and (**d**) methyl isobutyl ketone at the upper interface based on the FEM and the experiment.

4. Conclusions

The VOCs emission characteristics of base and CRMB binders during heating were characterized and the inhibiting effect of Mt on the VOCs emission of CRMB was investigated in this research. A VOCs emission model of bitumen was established to compare the VOCs emission behaviors of CRMB and Mt-CRMB. Based on the results and discussion, the following conclusions can be drawn:

(1) The addition of crumb rubber increased the VOCs species number from 123 to 144. The VOCs emission of the CRMB binder was 3.2 times larger than that of the base binder. Furthermore, the addition of crumb rubber significantly increased the ARHs of the base binder, and the emission of some ARHs such as benzene, toluene, m-xylene, and p-xylene emissions increased by more than 10 times. However, the emission of some lightweight compounds such as alkanes was reduced since they were absorbed by the rubber.

(2) Due to its special intercalated structure, the VOCs of Mt-CRMB included 108 compounds, 25% less than that of CRMB, and the Mt nanoclay can reduce the VOCs emission of CRMB binder by about 30%. Especially, its inhibition effects on alkanes, olefins, and aromatic hydrocarbons were more significant, and 14 fingerprint compounds belonging to the above types were reduced by more than 30%. With the extension of the heating time, the VOCs species number of CRMB and Mt-CRMB binders gradually decreased. At 120 min, the Mt-CRMB binder only emitted 79 species of VOCs, reduced by 39% compared with the maximum value.

(3) The VOCs emission rates of CRMB and Mt-CRMB binders were close at 30 min. However, with the extension of the heating time, their VOCs emission rates were significantly different. The emission rate of the Mt-CRMB binder decreased by 41% compared with the CRMB binder at 120 min. Furthermore, the addition of Mt significantly reduced the emission rate of most VOCs in the bitumen. By calculation, the C_0 for most compounds after the Mt modification decreased, except for undecane, and for most compounds, the D_m was relatively stable after the Mt modification. Based on Fick's second law, the emission behavior of CRMB and Mt-CRMB binders can be well-described by the established model.

Overall, the Mt nanoclay can be used as an effective modifier to inhibit the VOCs emission of the CRMB binder, which is widely used in asphalt pavement.

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