

## **SUPPLEMENTARY INFORMATION**

# **Natural Rubber Composites Using Hydrothermally Carbonized Hardwood Waste Biomass as a Partial Reinforcing Filler- Part I: Structure, Morphology, and Rheological Effects during Vulcanization**

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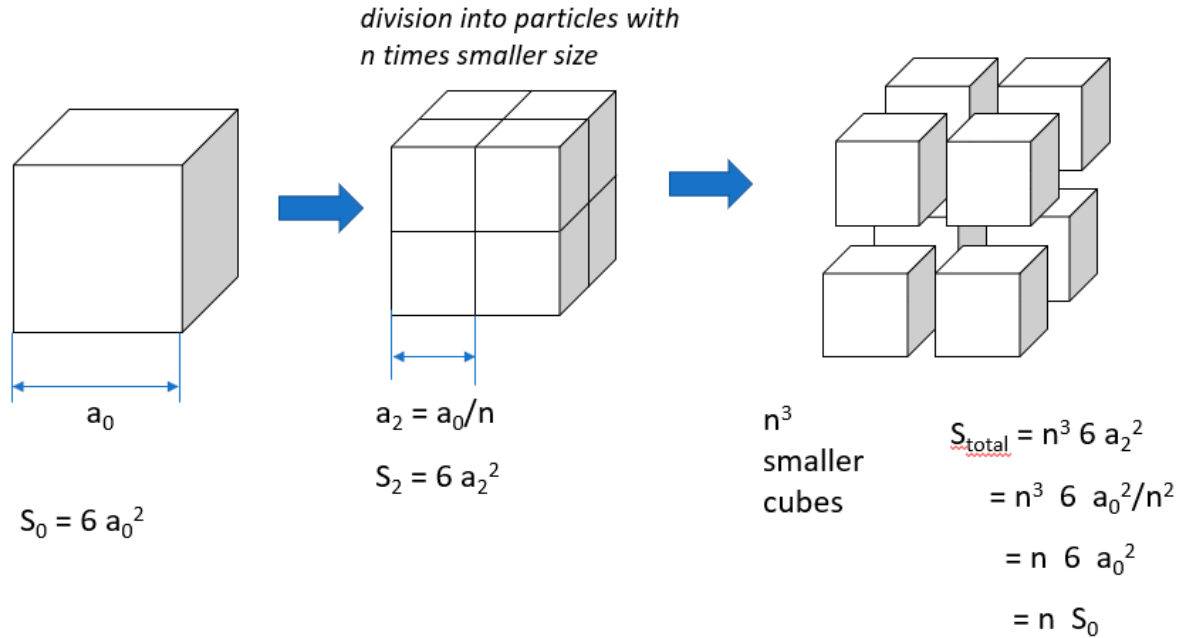
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## 1 Estimation of specific surface from particle size

A simple estimation of the specific surfaces of materials as function of particle size can be done using the model of a cube being divided into smaller cubes (**Scheme** ).



**Scheme S1:** Division of a cube with edge length  $a_0$  into smaller ones with  $n$  times shorter edge length.

It can be seen from Scheme S1 that if a cube of the edge length  $a_0$  is divided into smaller ones, whose edge length is  $n$  times shorter, then the total surface area of the resulting small cubes is  $n$  times larger than the surface area  $S_0$  of the precursor cube. (The total volume  $V_0 = a_0^3$  does not change).

Hence, if the density and filler amount are constant,  $n$  times smaller particles mean  $n$  times higher surface area of the smaller filler.

If both the sizes and densities ( $\rho$ ) of the particles are different, then the size ( $a_{0i}$ ) of the original (precursor) piece (monolithic cube) of a given filler amount (e.g.  $m_{0i} = 1$  g) is different for every filler. It holds:

$$V_{0i} = a_{0i}^3$$

$$S_{0i} = 6 a_{0i}^2$$

$$\rho_i = m_{0i} / a_{0i}^3$$

hence

$$a_{0i} = (m_{0i} / \rho_i)^{1/3}$$

$$S_{0i} = 6 (m_{0i} / \rho_i)^{2/3}$$

and

$$a_{02} / a_{01} = (m_{02} / \rho_2)^{1/3} / (m_{01} / \rho_1)^{1/3} = (\rho_1 / \rho_2)^{1/3}$$

$$S_{02} / S_{01} = 6 (m_{02} / \rho_2)^{2/3} / 6 (m_{01} / \rho_1)^{2/3} = (\rho_1 / \rho_2)^{2/3}$$

A less dense filler (e.g. filler “2” with  $\rho_2$ ,  $a_{02}$ , and  $S_{02}$ ) has to be added in a larger volume than the denser filler “1”, if the same wt.% (or phr) have to be achieved.

If both filler 1 and filler 2 are added in the same amount (in g) and are divided into the same number of particles, than the particles of filler 2 are larger, and their total surface area also is larger than in case of filler 1, as given by the above equations for the ratios  $a_{02} / a_{01}$  and  $S_{02} / S_{01}$ .

For the fillers CB and HC, it can be calculated

with  $m_{0CB} = m_{0HC} = 1 \text{ g}$  and

with

$\rho_{CB} = 2969 \text{ kg/m}^3$  (as determined experimentally in this work) and

$\rho_{HC} = 1407 \text{ kg/m}^3$  (as determined experimentally in this work):

for CB:

$a_{0CB}(1\text{g cube}) = 0.00696 \text{ m} (= 6.96 \text{ mm})$

$S_{0i}(1\text{g cube}) = 0.0002904 \text{ m}^2 (= 2.904 \text{ cm}^2)$

particle size ( $a_{2CB}$ ) found by TEM: 30–60 nm

size factor ( $a_{0CB}/a_{2CB}$ ):  $1.16 \cdot 10^5 - 2.32 \cdot 10^5$

theoretical specific surface area:  $33.7 - 67.4 \text{ m}^2/\text{g}$

difference from experimental ( $77.8 \text{ m}^2$ ): factor 1.15–2.31 (average: 1.73)

for HC:

$a_{0CB}(1\text{g cube}) = 0.00892 \text{ m} (= 8.92 \text{ mm})$

$S_{0i}(1\text{g cube}) = 0.000478 \text{ m}^2 (= 4.78 \text{ cm}^2)$

particle size ( $a_{2HC}$ ) found by TEM: 0.5–3  $\mu\text{m}$

size factor ( $a_{0HC}/a_{2HC}$ ): 2 975 – 17 800

theoretical specific surface area:  $1.42 - 8.53 \text{ m}^2/\text{g}$

difference from experimental ( $21.4 \text{ m}^2$ ): factor 2.51–15.1 (average: 8.79)

HC vs. CB:

the density factor:  $S_{0HC} / S_{0CB} = 1.64$

size ratio (from TEM):  $a_{0HC} / a_{0CB} = \text{ca. } 17\text{--}50$

theoretical specific surface area ratio if densities of CB and HC were the same: 17–50

theoretical specific surface area ratio, corrected by density factor: 27–82

experimentally found (BET) ratio of specific surfaces:

$77.8 \text{ m}^2\text{g}^{-1} / 21.4 \text{ m}^2\text{g}^{-1} = 3.63$

difference from theory: factor 7.5–22.6

## 2 Fillers: Specific surface analysis

### 2.1 sample "CB"

#### Summary Report

##### Surface Area

Single point surface area at  $P/P_o = 0.300303893$ : 76.2684 m<sup>2</sup>/g

BET Surface Area: 77.8403 m<sup>2</sup>/g

#### Options Report

##### Analysis Conditions

##### Preparation

Evacuation rate: 100.0 mmHg/min

Evacuation time: 15.00 min

##### Free Space

Free-space type: Measured

##### Po and Temperature

Po and T type: Most recent measured Po value. Entered temperature value.

Temperature: 77.150 K

##### Analysis Method

Analysis Mode: Equilibration

Equilibration time: 15 s

##### Degas Conditions

Sample Prep: Stage	Temperature (°)	Ramp Rate (°/min)	Time (min)
1	90	10	0

##### Adsorptive Properties

Adsorptive: Nitrogen

Maximum manifold pressure: 1050.00 mmHg

Non-ideality factor: 0.0000620

Density conversion factor: 0.0015468

Molecular cross-sectional area: 0.162 nm<sup>2</sup>

##### Experiment

Started: 11.12.2022 9:43:06odp.

Completed:

Report Time: 11.12.2022 13:58:53odp.

Free Space Diff.: -0.2489 cm<sup>3</sup> Sample

Free Space Type: Measured

Evac. Rate: 100.0 mmHg/min

Gemini VII 2390 V1.01 (V1.01 a)

Analysis Adsorptive: N2

Equilibration Time: 15 s

Sat. Pressure: 735.844 mmHg

Mass: 0.0518 g

Sample Density: 2.969 g/cm<sup>3</sup>

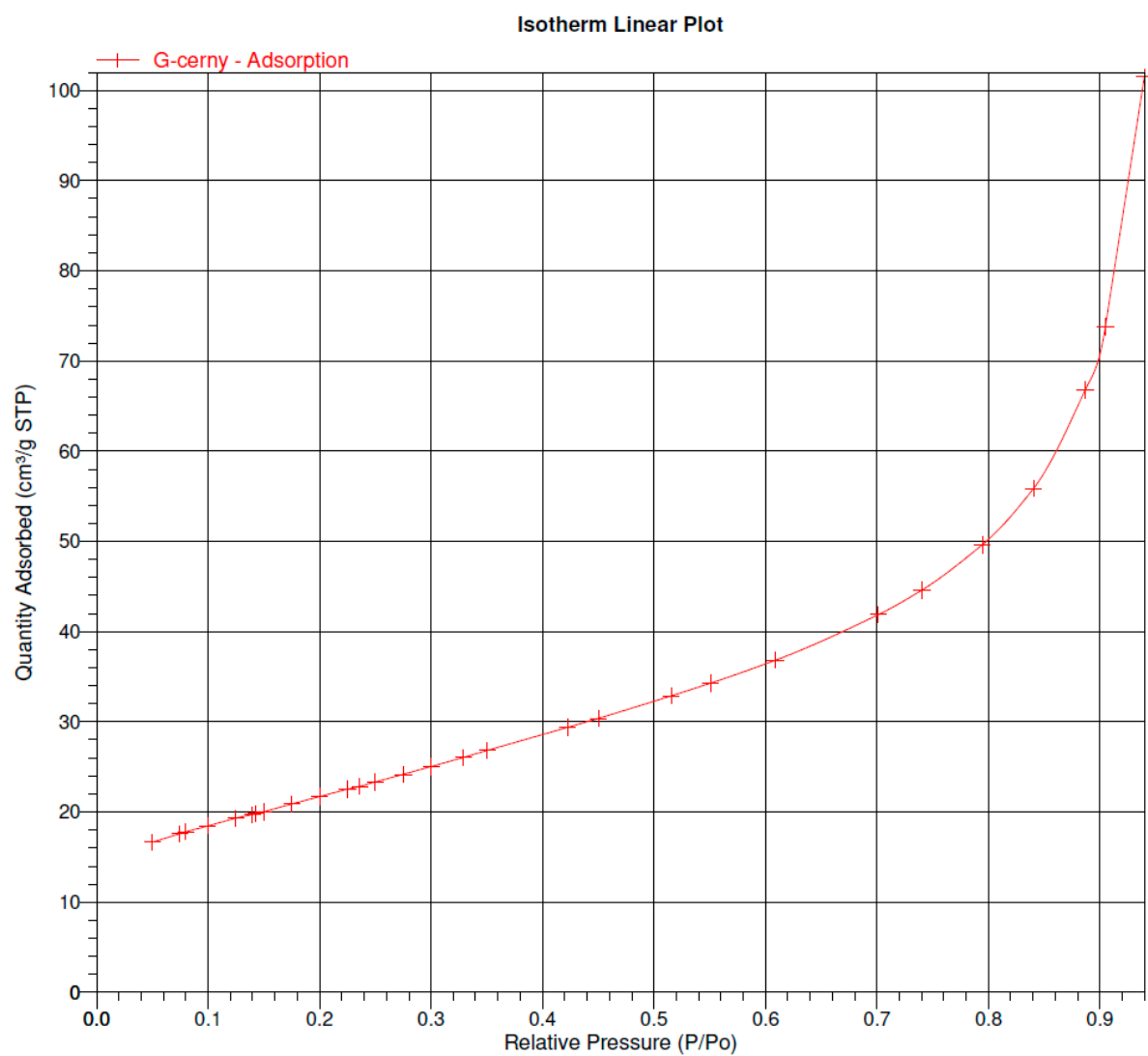
Micromeritics Instrument Corporation

**Isotherm Tabular Data: sample "CB"**

Saturation Pressure (mmHg)

735.843811

Relative Pressure (P/P <sub>0</sub> ) ( )	Absolute Pressure (mmHg)	Quantity Adsorbed (cm <sup>3</sup> /g STP)	Elapsed Time (h:min)
0.049898117	36.71722	16.6576	1:02
0.07472054	54.98265	17.5963	1:07
0.079783256	58.70802	17.7969	1:11
0.099543311	73.24833	18.4357	1:16
0.124927246	91.92694	19.3207	1:21
0.139744301	102.83	19.7229	1:26
0.142832311	105.1023	19.8242	1:31
0.149716719	110.1681	20.0235	1:35
0.174945411	128.7325	20.884	1:40
0.199839583	147.0507	21.7011	1:45
0.225042997	165.5965	22.525	1:50
0.235945476	173.619	22.834	1:55
0.249926054	183.9065	23.3253	2:00
0.275288475	202.5693	24.1804	2:05
0.300303893	220.9768	25.0395	2:09
0.329161111	242.2112	26.0502	2:14
0.350476254	257.8958	26.8253	2:19
0.422393335	310.8155	29.3764	2:24
0.450421095	331.4396	30.3889	2:29
0.515674517	379.4559	32.8786	2:34
0.550580227	405.1411	34.2731	2:39
0.608902988	448.0575	36.8241	2:45
0.701359689	516.0912	41.8803	2:51
0.740250322	544.7086	44.5928	2:57
0.794441802	584.5851	49.6104	3:04
0.840416919	618.4156	55.8577	3:11
0.886894356	652.6157	66.7701	3:22
0.904951076	665.9026	73.7827	3:33
0.939989623	691.6855	101.5176	3:58



**Figure S1.** Adsorption isotherm (of nitrogen) on the sample "CB".

**BET Surface Area Data: sample "CB"**BET Surface Area:  $77.8403 \pm 0.1566 \text{ m}^2/\text{g}$ Slope:  $0.055478 \pm 0.000111 \text{ g}/\text{cm}^3 \text{ STP}$ Y-Intercept:  $0.000447 \pm 0.000020 \text{ g}/\text{cm}^3 \text{ STP}$ 

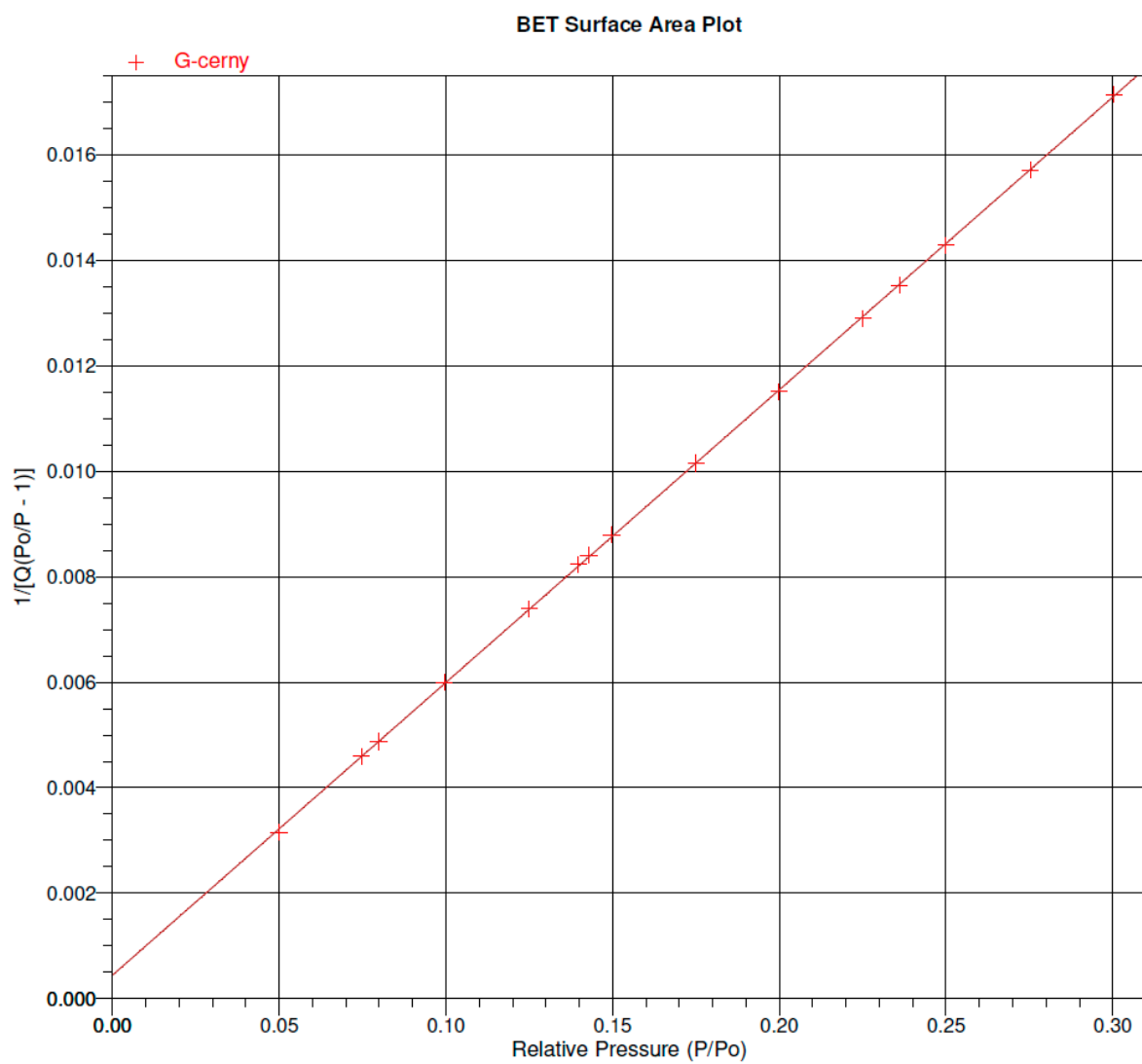
C: 125.055284

Qm:  $17.8812 \text{ cm}^3/\text{g STP}$ 

Correlation Coefficient: 0.9999741

Molecular Cross-Sectional Area:  $0.1620 \text{ nm}^2$ 

Relative Pressure (P/P <sub>0</sub> )	Quantity Adsorbed (cm <sup>3</sup> /g STP)	1 / [Q(P/P <sub>0</sub> - 1)] ( )
0.049898117	16.6576	0.003153
0.07472054	17.5963	0.004589
0.079783256	17.7969	0.004872
0.099543311	18.4357	0.005996
0.124927246	19.3207	0.007389
0.139744301	19.7229	0.008236
0.142832311	19.8242	0.008406
0.149716719	20.0235	0.008794
0.174945411	20.884	0.010153
0.199839583	21.7011	0.011509
0.225042997	22.525	0.012892
0.235945476	22.834	0.013524
0.249926054	23.3253	0.014285
0.275288475	24.1804	0.015709
0.300303893	25.0395	0.017141



**Figure S2.** BET-plot of the adsorption isotherm (of nitrogen) on the sample “CB”.



## 2.2 sample "HC"

### Summary Report

#### Surface Area

Single point surface area at  $P/P_0 = 0.300333577$ : 16.1976 m<sup>2</sup>/g

BET Surface Area: **21.3628 m<sup>2</sup>/g**

### Options Report

#### Analysis Conditions

##### Preparation

Evacuation rate: 100.0 mmHg/min

Evacuation time: 15.00 min

##### Free Space

Free-space type: Measured

##### P<sub>0</sub> and Temperature

P<sub>0</sub> and T type: Most recent measured P<sub>0</sub> value. Entered temperature value.

Temperature: 77.150 K

##### Analysis Method

Analysis Mode: Equilibration

Equilibration time: 15 s

#### Degas Conditions

Sample Prep: Stage	Temperature (°)	Ramp Rate (°/min)	Time (min)
1	90	10	0

#### Adsorptive Properties

Adsorptive: Nitrogen

Maximum manifold pressure: 1050.00 mmHg

Non-ideality factor: 0.0000620

Density conversion factor: 0.0015468

Molecular cross-sectional area: 0.162 nm<sup>2</sup>

#### Experiment

Started: 12.12.2022 7:12:35pm

Completed: 12.12.2022 10:53:53pm

Report Time: 12.12.2022 10:53:54pm

Free Space Diff.: -0.1764 cm<sup>3</sup>

Free Space Type: Measured

Evac. Rate: 100.0 mmHg/min

Gemini VII 2390 V1.01 (V1.01 a)

Analysis Adsorptive: N2

Equilibration Time: 15 s

Sat. Pressure: 737.604 mmHg

Sample Mass: 0.0067 g

Sample Density: 1.407 g/cm<sup>3</sup>

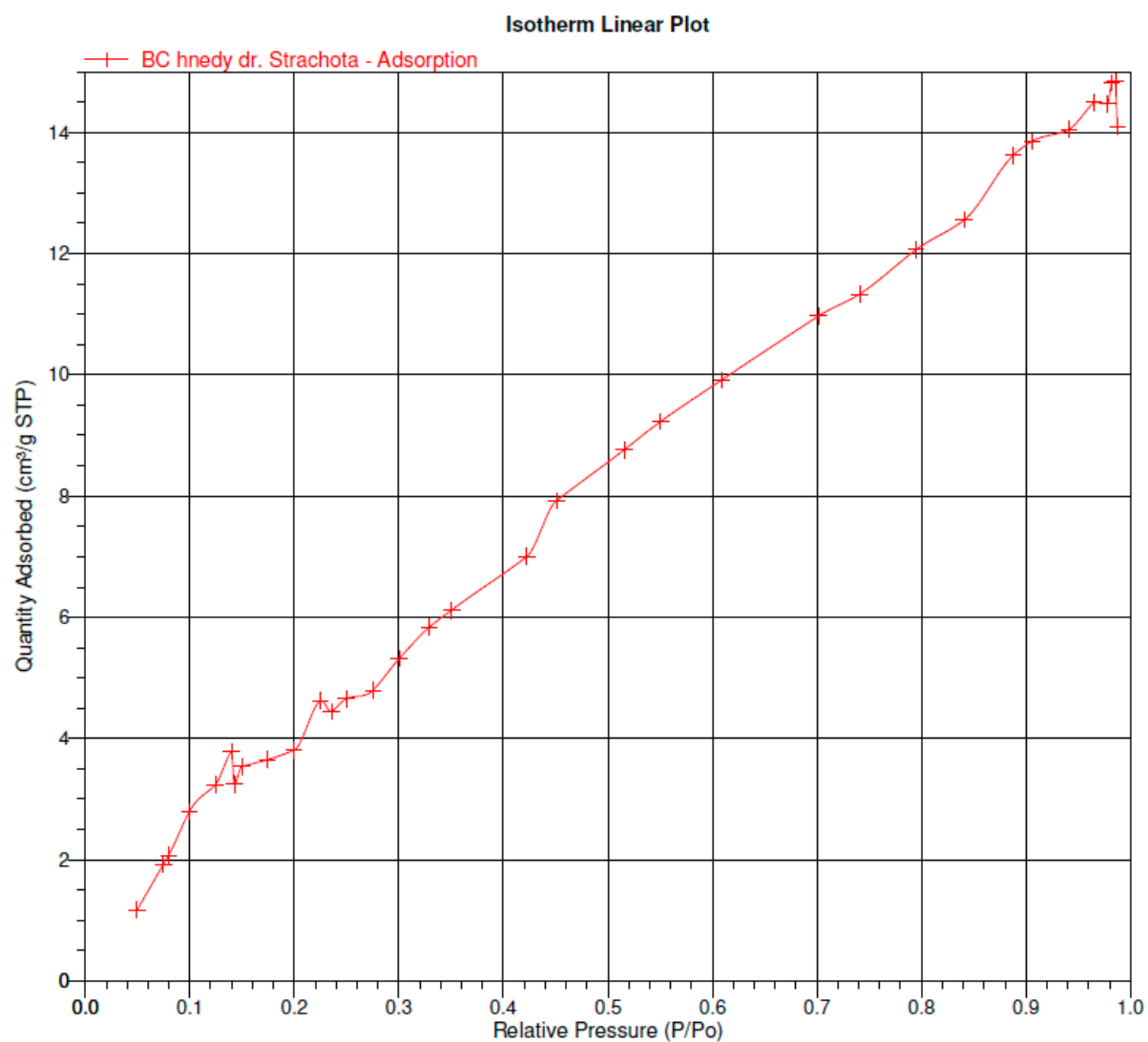
Micromeritics Instrument Corporation

**Isotherm Tabular Data: sample "HC"**

Saturation Pressure (mmHg)

737.603760

Relative Pressure (P/P <sub>0</sub> ) ( )	Absolute Pressure (mmHg)	Quantity Adsorbed (cm <sup>3</sup> /g STP)	Elapsed Time (h:min)
0.049548202	36.54694	1.1705	1:02
0.074690135	55.09172	1.9263	1:06
0.079673647	58.76758	2.0759	1:11
0.099589798	73.45781	2.7953	1:16
0.124712823	91.98865	3.2422	1:21
0.139911925	103.1996	3.7847	1:26
0.142721506	105.2719	3.2455	1:31
0.149936357	110.5936	3.5417	1:37
0.174458312	128.6811	3.6504	1:42
0.199597349	147.2238	3.8079	1:46
0.224892283	165.8814	4.6242	1:51
0.235823424	173.9442	4.451	1:55
0.24984764	184.2886	4.657	2:00
0.275206808	202.9936	4.7967	2:04
0.300333577	221.5272	5.318	2:09
0.329279038	242.8775	5.8377	2:13
0.350309394	258.3895	6.1167	2:18
0.422373954	311.5446	7.0002	2:23
0.450678326	332.422	7.9227	2:28
0.515632773	380.3327	8.7645	2:32
0.550645309	406.1581	9.2317	2:37
0.608948688	449.1628	9.9155	2:41
0.701460252	517.3997	10.9698	2:46
0.740700709	546.3436	11.329	2:50
0.794822547	586.2641	12.0648	2:55
0.84085884	620.2206	12.5536	2:59
0.887693403	654.766	13.6197	3:03
0.905954787	668.2357	13.8525	3:08
0.94085702	693.9797	14.0482	3:13
0.96489429	711.7097	14.4939	3:17
0.977974001	721.3573	14.4711	3:22
0.981893355	724.2482	14.8229	3:28
0.985918046	727.2169	14.8436	3:34
0.987254425	728.2026	14.0991	3:40



**Figure S3.** Adsorption isotherm (of nitrogen) on the sample “HC”.

**BET Surface Area Data: sample "HC"**BET Surface Area:  $21.3628 \pm 1.6445 \text{ m}^2/\text{g}$ Slope:  $0.177420 \pm 0.015428 \text{ g}/\text{cm}^3 \text{ STP}$ Y-Intercept:  $0.026355 \pm 0.002837 \text{ g}/\text{cm}^3 \text{ STP}$ 

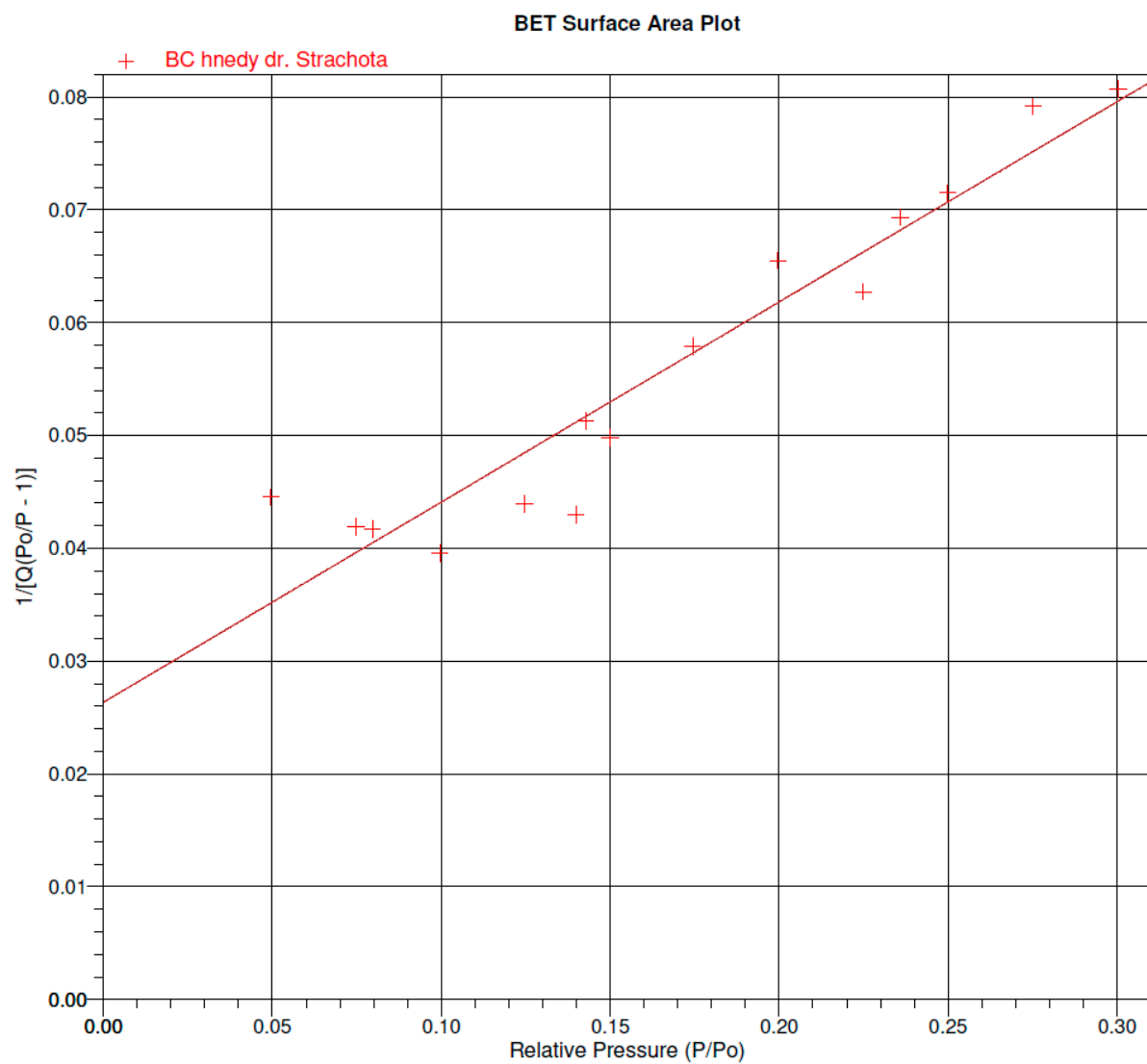
C: 7.731971

Qm:  $4.9074 \text{ cm}^3/\text{g STP}$ 

Correlation Coefficient: 0.9542024

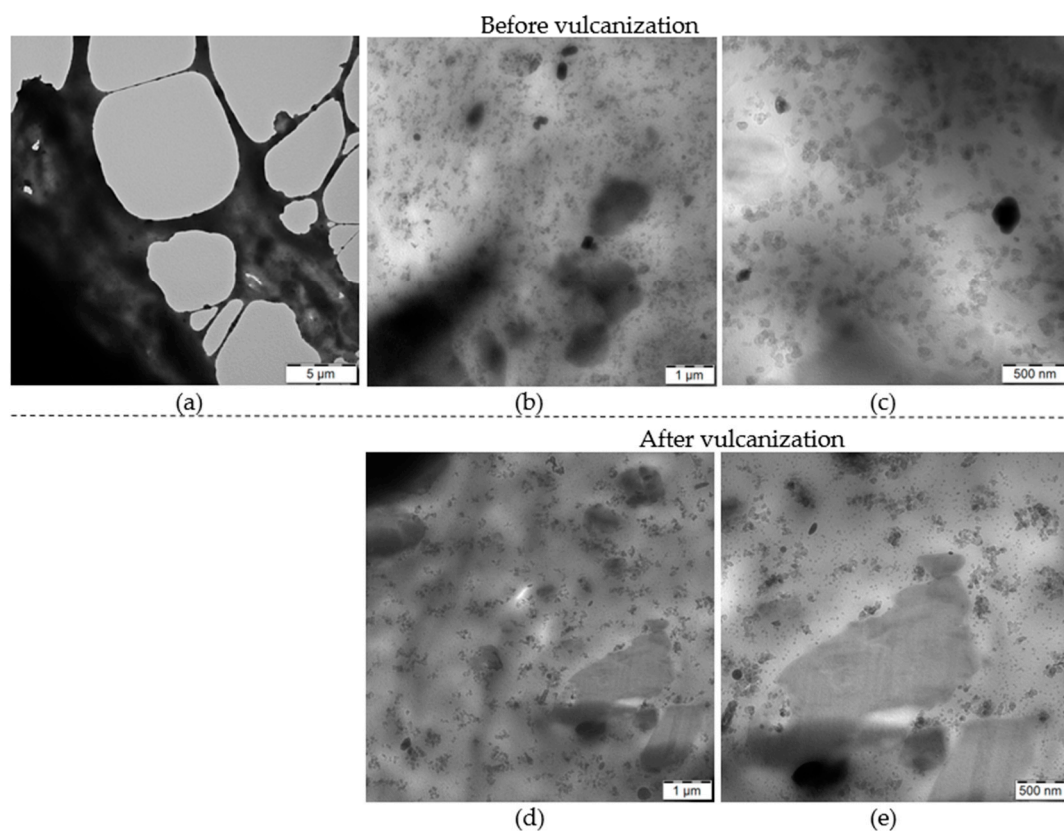
Molecular Cross-Sectional Area:  $0.1620 \text{ nm}^2$ 

Relative Pressure (P/P <sub>0</sub> )	Quantity Adsorbed (cm <sup>3</sup> /g STP)	1 / [Q(P/P <sub>0</sub> - 1)] ( )
0.049548202	1.1705	0.044538
0.074690135	1.9263	0.041903
0.079673647	2.0759	0.041703
0.099589798	2.7953	0.039569
0.124712823	3.2422	0.043946
0.139911925	3.7847	0.042982
0.142721506	3.2455	0.051296
0.149936357	3.5417	0.049802
0.174458312	3.6504	0.057891
0.199597349	3.8079	0.065488
0.224892283	4.6242	0.062744
0.235823424	4.451	0.069332
0.24984764	4.657	0.071519
0.275206808	4.7967	0.079159
0.300333577	5.318	0.080716

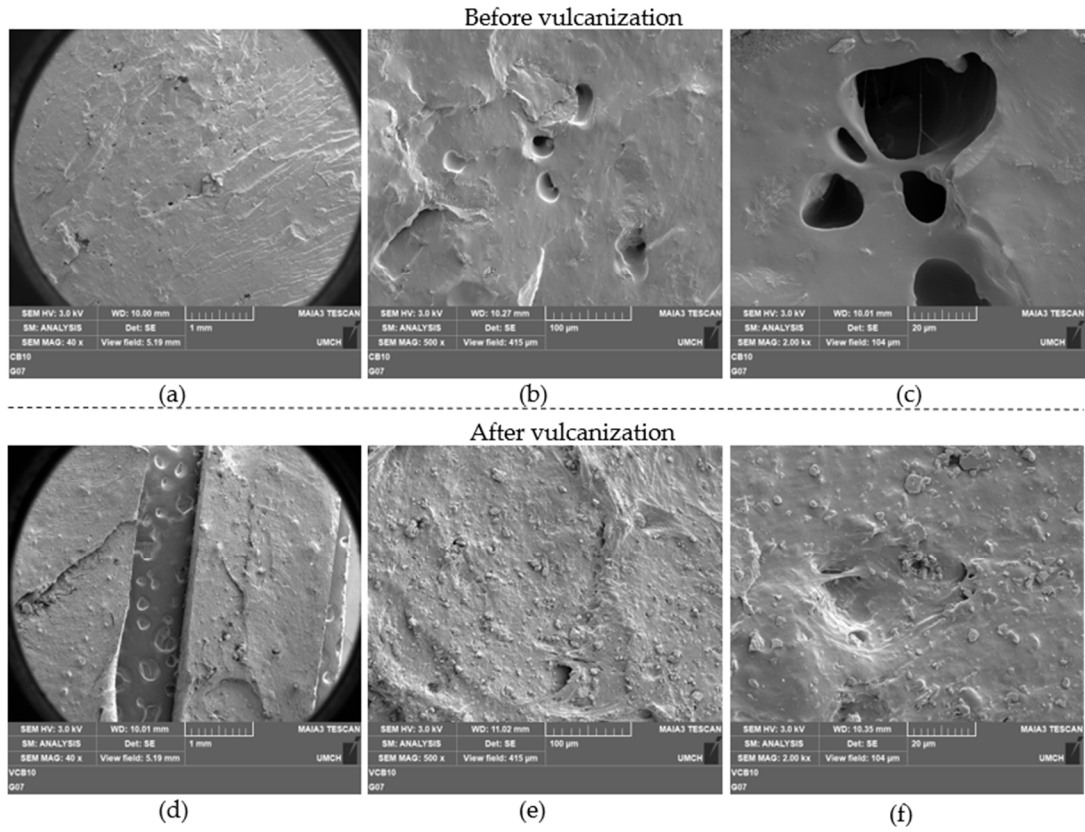


**Figure S4.** BET-plot of the adsorption isotherm (of nitrogen) on the sample "HC".

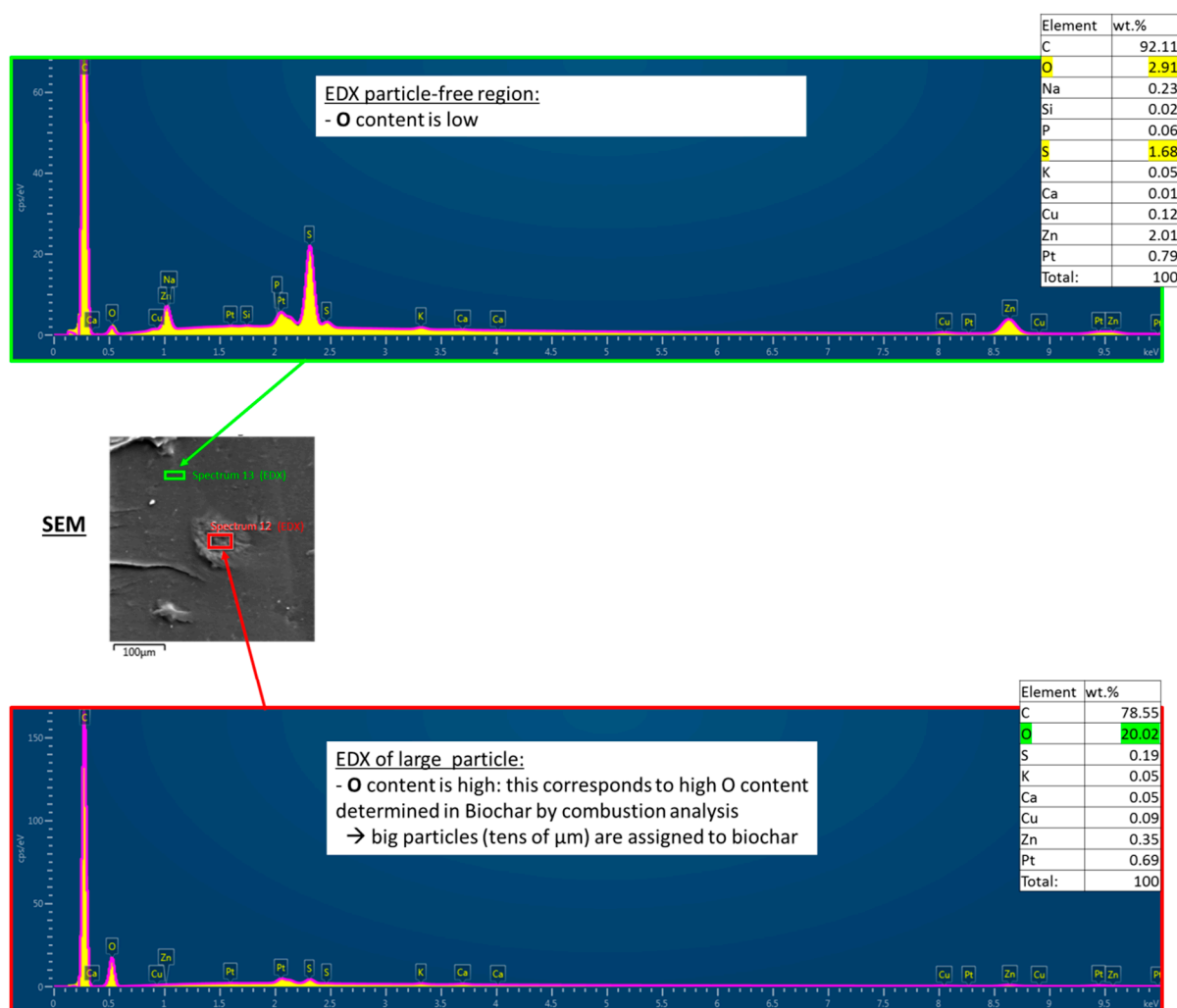
### 3 Nanocomposite Morphology: TEM/SEM



**Figure S5.** TEM images of the sample filled with 40 phr (25.16 wt.%) of hydrochar and 10 phr (6.29 wt.%) of carbon black: (a, b, c) unvulcanized state: sample CB10; (d, e) vulcanized state: sample VCB10; (a): 'global view' – 5  $\mu\text{m}$  scalebar; (b, d): 1  $\mu\text{m}$  scalebar; and (c, e): 500 nm scalebar.



**Figure S6.** SEM images of the sample filled with 40 phr (25.16 wt.%) of hydrochar and 10 phr (6.29 wt.%) of carbon black: (a, b, c) unvulcanized state: sample CB10; (d, e, f) vulcanized state: sample VCB10; (a, d): really global view – 1 mm scalebar; (b, e): 100  $\mu\text{m}$  scalebar; and (c, f): 20  $\mu\text{m}$  scalebar.



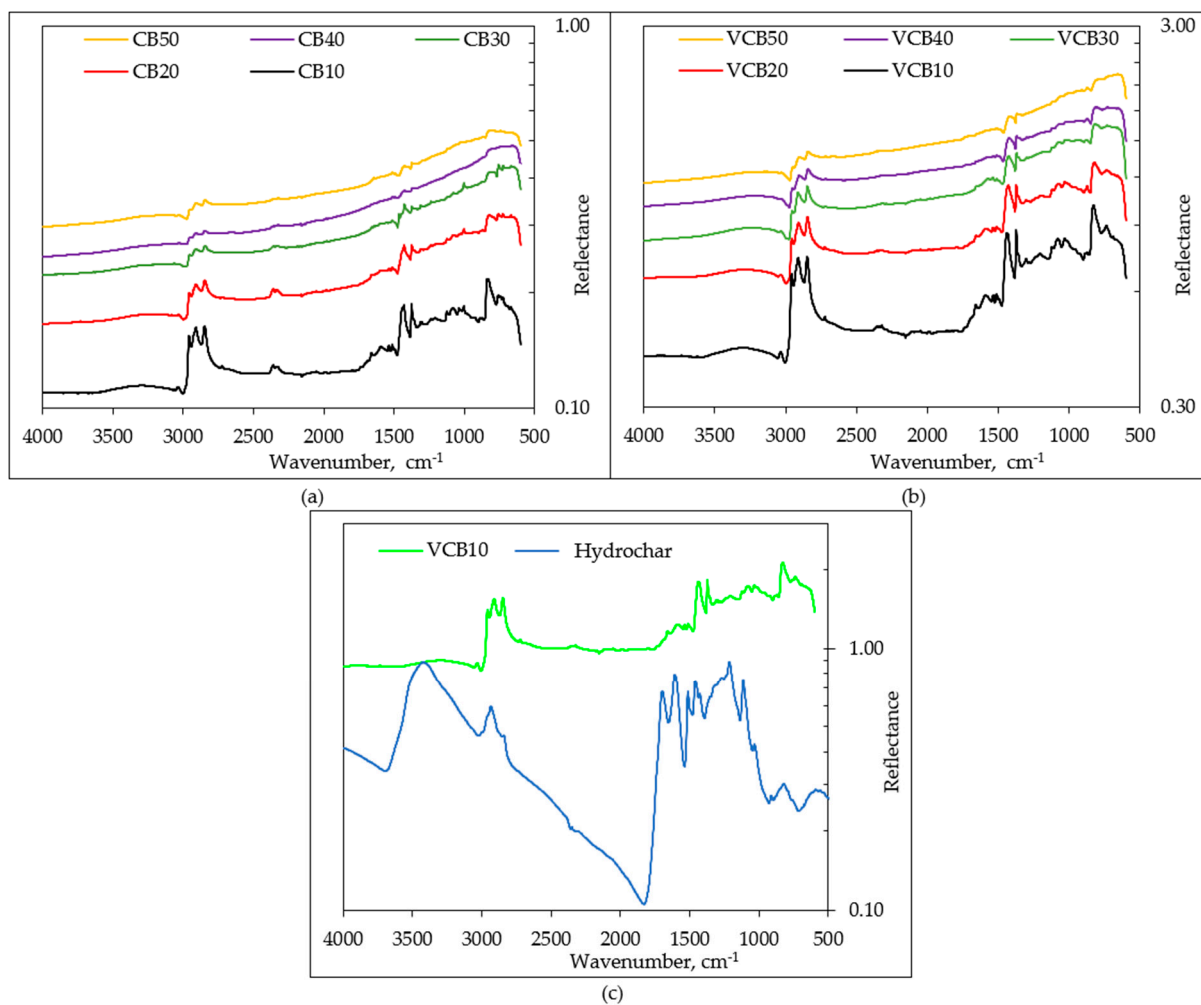
**Figure S7.** EDX elemental analysis from the SEM image of the sample VCB40: top: hydrochar-free domain; bottom: hydrochar grain; in the hydrochar-free matrix (top) sulphur can clearly be detected, following trace elements also are visible: Zr (from ZrO<sub>2</sub> balls in ball mill), Pt (from applied metal coating used in SEM for better sharpness), Cu (from Cu grid on which the SEM sample was placed), Na, Ca, K (minerals from wood which stayed in the hydrochar).



#### 4 FTIR of nanocomposites

Unvulcanized and vulcanized samples were analysed using FTIR spectroscopy and the results are presented in the Figure S8. The unvulcanized and vulcanized samples with the same ratio of the fillers (HC/CB) are showing nearly identical FTIR spectra (see Figure S8a vs. b). On the other hand, the influence of the presence of the graphitic CB filler (which does not display any intense peaks, as shown in the Main Manuscript) on the intensity of the IR peaks of the composites clearly can be seen: All the observable IR peaks which originate mainly from the natural rubber strongly decrease in intensity with increasing CB content, which could be assigned to indiscriminate reflection on the graphitic CB phase. At high contents of hydrochar, its characteristic groups of peaks in the region 1700 down to 1000  $\text{cm}^{-1}$  appear to prominently contribute to the FTIR pattern of the composites (see e.g. the overlay in Figure S8).

The following assignments of the registered peaks can be made (on the example of sample VCB10, see Figure S8b and c): The characteristic vibrational absorption bands of C–H stretching of natural rubber (and also of hydrochar) are found at 2962, 2917 and 2852  $\text{cm}^{-1}$ , assigned to aliphatic groups (a weak signal of unsaturated C-H stretching of rubber and hydrochar also can be seen at 3037  $\text{cm}^{-1}$ ). The small absorption peak at 1656  $\text{cm}^{-1}$  corresponds to C=C stretching in rubber and is overlaid with C=C peaks of HC. The absorption bands, detected at 1442  $\text{cm}^{-1}$  and 1373  $\text{cm}^{-1}$  are related to the C-H bending of the groups  $-\text{CH}_2-$  (rubber and HC) and  $-\text{CH}_3-$  (predominantly from rubber), respectively. In view of the prominent broad peak around 3300  $\text{cm}^{-1}$ , the presence of water in KBr can be noted, while the occasionally observed peak near 2350  $\text{cm}^{-1}$  is caused by carbon-dioxide from the atmosphere.



**Figure S8.** FT-IR spectra of a) unvulcanized, b) vulcanized natural rubber samples, and c) overlay of hydrochar and VCB10 spectra.