

Article



A Bifunctional Pt/CeO₂-Cu₁/CeO₂ Catalyst System for Isooctane Oxidation under Fully Simulated Engine-Exhaust Condition: Eliminating the Inhibition by CO

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Abstract: Pt-based catalysts, because of their outstanding activity for hydrocarbon oxidation, are widely used in the engine-exhaust aftertreatment system to remove hydrocarbon emissions. However, the CO and NO_x present in real engine exhausts compete with hydrocarbons for active Pt sites, and thus inhibit hydrocarbon oxidation. In this work, we evaluated the inhibition effects of CO and NO on isooctane oxidation over a Pt/CeO₂ catalyst under the simulated condition of the US DRIVE test protocol (S-GDI, stoichiometric gasoline direct injection). We also leveraged a low-cost single-atom Cu₁/CeO₂ catalyst, which is highly active for low-temperature CO oxidation, to eliminate the inhibition effect of CO. Specifically, by physically mixing Cu₁/CeO₂ and Pt/CeO₂, all the CO is completely converted below 200 °C under simulated exhaust condition, which helps lower the isooctane oxidation temperature. However, the unconverted NO still strongly suppresses HC oxidation. Possible strategies to address the NO inhibitor were proposed.

Keywords: emission control; hydrocarbon oxidation; Pt/CeO2; Cu single-atom catalyst



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1. Introduction

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Unburned hydrocarbon fuels are one of the major pollutants in the exhaust of internal combustion engines [1,2]. Although hydrocarbon emissions can be addressed by the three-way catalysts (TWCs) or the diesel oxidation catalysts (DOCs), the low-temperature hydrocarbon oxidation during the "cold start" period is still a challenging task for the engine aftertreatment system [3], due to stable C-H bonds, especially for the saturated alkane molecules [4]. Thus, low-temperature hydrocarbon oxidation catalysts are needed.

So far, the expensive platinum group metals (PGM), such as Pt and Pd, are still the most efficient catalysts for low-temperature hydrocarbon oxidation, due to their ability to activate C-H bonds of hydrocarbon molecules [5]. However, under real exhaust conditions, the catalytic reaction of hydrocarbons on PGMs can be inhibited by other components, including CO, NO_x, and H₂O, due to the competitive adsorption [6–12]. For instance, CH₄ oxidation on Pd catalysts is strongly inhibited by H₂O, associated with the formation of OH species in the active PdO phase [10–12]. In contrast, for the Pt-based catalyst, the inhibition effect of H₂O is weaker, with CO and NO, and HC itself as the major inhibitor. A typical empirical kinetic model for hydrocarbon (HC) oxidation on Pt-based catalysts is given in the form of [6]:

$$_{\rm HC} = \frac{kY_{\rm HC}Y_{\rm O_2}}{T^n (1 + K_{\rm CO}Y_{\rm CO} + K_{\rm HC}Y_{\rm HC} + K_{\rm NO}Y_{\rm NO})^2}$$
(1)

where r_{HC} denotes the rate of hydrocarbon oxidation; *T* is the temperature; *k* is the rate constant; Y_i represents the concentration of component *i* (*i* = HC, O₂, CO, or NO); and K_i represents the inhibition factor of the component *i* (*i* = HC, CO, or NO). The inhibition

factor, K_i , is essentially associated with the strength of molecule adsorption on the metal catalyst. Among the hydrocarbon molecules, the saturated alkanes were adsorbed more weakly on metal catalysts than the unsaturated alkenes or aromatics, and thus the oxidation of alkanes is more easily inhibited by other components [9].

In a previous work [13], we synthesized a Pt/CeO₂ catalyst (Table 1), which showed improved hydrocarbon-oxidation activity, by using a CeO₂ support pre-calcined at 800 °C. Loading Pt on this high-temperature pretreated CeO₂ formed two-dimensional Pt rafts, which can be turned into three-dimensional Pt nanoparticles (1–1.5 nm) upon reduction treatment (by CO at 250 °C). On one hand, the Pt rafts or nanoparticles are responsible for activating HC molecules. On the other hand, the high-temperature pretreatment decreased the surface defects on the CeO_2 and thus enhanced the mobility of the surface lattice oxygen and promoted the redox activity of the catalyst, regardless of the Pt cluster morphology. This improved redox activity promoted the catalytic activity of Pt/CeO_2 for HC oxidation, for both weakly adsorbed alkanes and strongly adsorbed aromatics and alkenes, under both lean and stoichiometric conditions. However, the fully simulated exhaust can dramatically decrease the reactivity of hydrocarbon molecules, due to the competitive adsorption of CO and NO_x, especially for the weakly adsorbed alkanes. For instance, T_{50} (temperature for 50% conversion) for isooctane oxidation on this Pt/CeO_2 catalyst was as low as 161 and 194 °C under rich (0.74% O_2) and lean (10% O_2) conditions (WHSV = 200L h⁻¹ g⁻¹), respectively. However, under fully simulated conditions (S-GDI and LTC-G), the presence of CO, NO_x, and H₂O significantly inhibited isooctane oxidation, increasing the T_{50} to 257 and 238 °C, respectively. Therefore, in addition to improving the intrinsic activity of the oxidation catalysts, eliminating the inhibition effects of other exhaust components is also a key to achieving low-temperature hydrocarbon oxidation reactivity under real exhaust conditions.

Table 1. Properties of Pt/CeO₂ and Cu₁/CeO₂ catalysts.

Pt/CeO ₂ [13]	Cu ₁ /CeO ₂ [14]	
1.66 wt.% Pt ^a	2 wt.% Cu ^b	
30	46	
	Pt/CeO₂ [13] 1.66 wt.% Pt ^a 30	

^a measured by ICP, ^b nominal loading.

Introducing catalytic sites which are specifically active for CO or NO conversion at lower temperatures (lower than the onset temperature for hydrocarbon oxidation) is a strategy to eliminate their inhibition effects for hydrocarbon oxidation. In our previous work [14], a low cost Cu_1/CeO_2 single-atom catalyst was developed for low-temperature CO oxidation. The Cu₁/CeO₂ with 2 wt.% Cu loading (Table 1) was synthesized via the atom trapping method (800 °C calcination) [15]. The Cu single-atom active sites trapped at step defects, with the Cu–O–Ce being the primary active oxygen species, can activate either lattice or adatom oxygen atoms for CO oxidation, accessing additional reaction channels as the catalyst environment changes. This Cu_1/CeO_2 catalyst is specifically active for CO oxidation, with low activity for HC oxidation. The complete CO conversion was achieved below 150 °C on this Cu_1/CeO_2 catalyst under the condition of 1% CO/8% O_2 with a GHSV of 300,000 h^{-1} [14]. Even under the fully simulated condition of the CDC (clean diesel combustion)-test protocol (12%O₂, 6% H₂O, 6% CO₂, 500 ppm CO, 100 ppm H₂, 200 ppm NO, 500 ppm C₃H₆, 300 ppm C₃H₆, 100 ppm C₃H₈) [16], this catalyst showed a low T₉₀ of 180 °C for CO conversion. In addition, strong anchoring of Cu to step defects effectively halts sintering and deactivation.

In this work, we systematically analyzed the inhibition effects of CO, NO, and H₂O on the isooctane oxidation over Pt/CeO₂ catalysts under the stoichiometric condition. We also leveraged the low-cost Cu₁/CeO₂ catalyst with high CO oxidation activity to eliminate the CO inhibition effect. It was found that CO and NO are the major inhibitors for isooctane oxidation under fully simulated exhaust conditions. Although the CO inhibitor was successfully addressed by Cu₁/CeO₂, the isooctane oxidation on Pt/CeO₂ was still strongly

inhibited by NO in the exhaust. We also proposed possible strategies for eliminating the inhibition effect of NO to further improve hydrocarbon oxidation reactivity under real exhaust conditions.

2. Results

2.1. Inhibition of HC Oxidation over Pt/CeO₂ Catalysts by CO and NO

We first evaluated the respective inhibition effect of CO, NO, and H_2O on the oxidation of isooctane (C_8H_{18}) under stoichiometric conditions. The test conditions are summarized in Table 2. The simulated exhaust conditions are based on the U.S. DRIVE protocol S-GDI (stoichiometric gasoline direct injection) [16]. The concentrations of CO, NO, and H_2 were adjusted from the original S-GDI protocol, due to the limitation of the available gas-mixture source (5000 ppm CO/2000 ppm NO/1000 ppm H_2).

Table 2. Gas composition of the fully simulated S-GDI and simplified conditions for catalyst tests #.

Gas Composition	O ₂	$O_2 + H_2O$	O ₂ + NO	O ₂ + CO	S-GDI
O2	0.74%	0.74%	0.74%	0.74%	0.74%
H_2O	0	13%	0	0	13%
CO ₂	0	0	0	0	13%
CO	0	0	0	3500 ppm	3500 ppm
NO	0	0	1400 ppm	0	1400 ppm
H_2	0	0	0	0	700 ppm
Isooctane	3000 C ₁				

[#] Space velocity: 200 L h⁻¹ $g_{Pt/CeO2}^{-1}$.

Figure 1 shows the light-off curves of isooctane oxidation on the Pt/CeO₂ catalyst under stoichiometric conditions. As shown in Figure 1a, under the simplified O₂-only condition (0.74% O₂), the oxidation of isooctane on Pt/CeO₂ was initiated at around 150 °C and the complete conversion was achieved below 200 °C. However, under the fully simulated S-GDI condition, the isooctane light-off temperature was significantly increased, by almost 100 °C. For instance, T_{50} of isooctane increases from 161 °C under the O₂-only condition to 257 °C under the S-GDI condition, as shown in Figure 1d. It seems that the decrease in isooctane oxidation reactivity is due to the inhibition effects of other components in the fully simulated exhaust condition.

CO, NO, and H₂O are all known to be potential inhibitors for hydrocarbon oxidation on noble metal catalysts. Therefore, we evaluated the inhibition effect of these three components by testing the light-off of isooctane oxidation in the O₂ + H₂O, O₂ + CO, and O₂ + NO conditions (composition listed in Table 2), separately. As shown in Figure 1a, H₂O only slightly increased the temperature of isooctane oxidation ($T_{50} = 177$ °C, Figure 1d), whereas CO and NO both significantly retarded the light-off of isooctane ($T_{50} = 237-238$ °C), close to the case of the S-GDI condition. These results suggest that CO and NO play a major role in inhibiting isooctane oxidation on the Pt/CeO₂ catalysts.

In contrast to isooctane, the oxidation reactivities of NO and CO on Pt/CeO₂ were not significantly affected by the presence of other components (e.g., CO, NO, and H₂O), as shown by the light-off curves of NO (Figure 1b) and CO (Figure 1c) under different conditions. As shown in Figure 1c, CO oxidation was initiated at a temperature as low as 150 °C, and reached 50% conversion at 217–231 °C. These T_{50} values of CO conversion are slightly lower than the temperature for the initiation of isooctane light-off under O₂ + CO and S-GID conditions (225–245 °C), as shown in Figure 1a. The sequential conversions of CO and isooctane suggest that the onset of isooctane oxidation requires the removal of the inhibitor CO.

On the other hand, Pt/CeO_2 has a relatively low activity for NO conversion. As shown in Figure 1b, the onset for NO conversion was at around 225 °C, and reached a maximum of about 30–40% at around 275 °C. While NO was converted into NO₂ and N₂O, a portion of NO_x (NO, NO₂ and N₂O) also underwent deNOx reactions (forming N₂), as indicated by the total-NO_x (NO, NO₂ and N₂O) conversion curve. Therefore, the NO inhibitor cannot be completely removed throughout the isooctane light-off test, due to the low NO conversion.

Given that CO and NO are the major inhibitors for isooctane oxidation on Pt/CeO_2 in the fully simulated exhaust, we proposed to introduce additional catalyst components which can remove these inhibitors at a lower temperature, so that the isooctane oxidation temperature on Pt/CeO_2 can be significantly reduced, ideally to the level of the $O_2 + H_2O$ condition.



Figure 1. Light-off curves of isooctane (**a**), NO (**b**), and CO (**c**) during isooctane oxidation on Pt/CeO₂ catalysts under fully simulated stoichiometric condition (S-GDI) and various simplified exhaust conditions (space velocity: $200L h^{-1} g_{Pt/CeO2}^{-1}$); (**d**) summary of T_{50} and T_{90} for isooctane conversion.

2.2. Eliminating the CO-Inhibition Effect Using Cu1/CeO2 Single-Atom Catalyst

In recent work by our group [14], a CeO₂-supported Cu single-atom catalyst Cu₁/CeO₂, as a low-cost non-PGM catalyst, was found to be a highly active and stable catalyst for low-temperature CO oxidation. Therefore, we introduced the Cu₁/CeO₂ to eliminate the inhibitor CO at low temperature by physically mixing Cu₁/CeO₂ with Pt/CeO₂. Figure 2 shows the performance of the Pt/CeO₂-Cu₁/CeO₂ bifunctional catalyst system, evaluated under a Pt-based space velocity of 200L h⁻¹ g_{Pt/CeO2}⁻¹, similar to the Pt/CeO₂ catalyst test of Figure 1.



Figure 2. Light-off curves of isooctane (**a**), NO (**b**), and CO (**c**) on Pt/CeO₂ + Cu₁/CeO₂ catalyst mixture (1:1 weight ratio) under fully simulated stoichiometric condition (S-GDI) and various simplified exhaust conditions (space velocity: 200L h⁻¹ $g_{Pt/CeO2}^{-1}$); (**d**) summary of T_{50} and T_{90} for isooctane conversion.

The isooctane light-off curves are shown in Figure 2a. In the O₂-only condition, the isooctane oxidation reactivity on the Cu_1/CeO_2 -Pt/CeO₂ mixture is essentially the same as on Pt/CeO_2 (Figure 1a), because the Cu_1/CeO_2 single-atom catalyst has very low activity for hydrocarbon oxidation. For instance, no isooctane oxidation was observed on Cu₁/CeO₂ below 300 $^{\circ}$ C in the S-GDI condition. The Introduction of 13% of H₂O $(O_2 + H_2O \text{ condition})$ has very weak inhibition effect on isooctane oxidation (Figure 2a), which is also similar to the Pt/CeO₂ catalyst. In the O_2 + CO condition, the Cu₁/CeO₂-Pt/CeO₂ mixture shows improved isooctane-oxidation activity in comparison to Pt/CeO₂, with T_{50} decreasing significantly, from 238 °C to 182 °C, because Cu₁/CeO₂ completely converts CO below 170 °C (Figure 2c) to eliminate the inhibition effect of CO. However, in the O_2 + NO condition, the Cu_1/CeO_2 -Pt/CeO₂ mixture does not improve the isooctane oxidation activity, as Cu₁/CeO₂ is not active for NO conversion (Figure 2b). Consequently, in the fully simulated S-GDI condition, the Cu_1/CeO_2 -Pt/CeO₂ mixture has only limited improvement for isooctane oxidation in comparison to Pt/CeO_2 , with T_{50} decreasing slightly, from 257 °C to 238 °C. This small improvement is likely ascribed to the elimination of the CO inhibitor below 200 °C.

It is noted that the CO oxidation activity of the Cu₁/CeO₂-Pt/CeO₂ mixture is lower under S-GDI than the O₂ + CO conditions (Figure 2c). This is likely because NO or H₂O has some inhibition effect on CO oxidation over Cu₁/CeO₂ [14]. The comparison of performance under the O₂ + NO + CO (0.75% O₂ + 1400 ppm NO + 3500 ppm CO) and S-GDI conditions (Figure S1) indicates that H_2O decreases both the CO oxidation activity and NO conversion activity of the Pt/CeO₂ + Cu₁/CeO₂ mixture, but barely affects its isooctane oxidation activity. Nevertheless, Cu₁/CeO₂ is capable of completely converting CO below 200 °C under the S-GDI condition.

On the other hand, for the PGM catalysts, not only does CO inhibit the oxidation of HCs, but HCs can also inhibit the oxidation of CO [6–9]. In contrast, on the Cu₁/CeO₂ catalyst, we noted that the presence of isooctane did not significantly change the CO oxidation activity. T_{50} and T_{90} for CO oxidation on Cu₁/CeO₂-Pt/CeO₂ in the mixture of isooctane (3000 ppm C₁) + CO (3500 ppm) + O₂ (0.74%) are 105 and 128 °C, respectively (Figure 2c), close to those reported for Cu₁/CeO₂ in the feed of CO (1%) + O₂ (4%) (T_{50} = 96 and T_{90} = 135 °C, Figure 3). This suggests that the Cu₁/CeO₂ single-atom catalyst also overcomes the inhibition effect of HCs on the CO oxidation reaction, because the H-C group of the HC molecules adsorbed more weakly on the Cu-O-Ce sites in comparison to the PMG sites [17]. This feature makes Cu₁/CeO₂ an attractive catalyst and specifically active for CO oxidation.



Figure 3. Light-off curves of CO oxidation on the pristine and reduced Cu₁/CeO₂ and Pt₁/CeO₂ catalysts ("-r" denotes reduced catalysts; "-LO1" and "-LO2" denote 1st and 2nd light-off test, respectively; light-off test condition: 1%CO/4%O₂/Ar balance, 20 mg of catalysts, 500 mg of inert SiC and 3 °C/min at 300 L (g_{cat} h)⁻¹; reduction-treatment condition: 1% CO/Ar, 275 °C).

2.3. Stability of Cu₁/CeO₂ Single-Atom Catalyst

Another advantage of the Cu_1/CeO_2 catalyst is its outstanding stability in comparison with the Pt-based catalysts. It is known that the noble metal single-atom catalysts (e.g., Pt_1/CeO_2 and Pd_1/CeO_2) easily undergo metal aggregation under reduction conditions [18]. In contrast, Cu single-atom sites on CeO_2 are highly resistant to reduction conditions with CO [14]. Figure 3 compares the CO oxidation activities of the pristine and reduced Cu_1/CeO_2 and Pt_1/CeO_2 catalysts, both of which were synthesized by the atomictrapping method. The pristine Pt_1/CeO_2 has relatively low activity for CO oxidation under 1% CO and 4% O₂ conditions, with a high T_{50} of 290 °C. Upon reduction treatment by 1% CO at 275 °C, Pt single-atom sites on the Pt_1/CeO_2 -reduced sample aggregated to form metallic Pt nanoparticles (Pt_{NP}). These metallic Pt_{NP} sites are in fact very active for CO oxidation, and show a T_{50} as low as 102 °C. However, the metallic Pt sites on Pt_{NP} are not stable. After one cycle of light-off tests to >300 °C, due to the surface oxidation or Pt-atom redispersion, the activity of the Pt₁/CeO₂-reduced sample was degraded in the second light-off. In contrast, the pristine and reduced Cu_1/CeO_2 present the same high activity for CO oxidation ($T_{50} = 100-102$ °C), indicating that the reduction atmosphere did not cause any change on the Cu single-atom sites.

3. Materials and Methods

The CeO₂-supported Pt catalysts (Pt/CeO₂), with improved hydrocarbon oxidation activity, were prepared by the incipient-wetness-impregnation method, as described in our previous work [13]. A commercial CeO₂ (99.99%, 10 nm, US Research Nanomaterials, Inc., Houston, TX, USA) pre-calcined at 800 °C for 10 h was used as the support. Aqueous solution of [Pt(NH₃)₄](NO₃)₂ (99.995%, Sigma Aldrich, St. Louis, MO, USA) was impregnated on the CeO₂ support to achieve a nominal 2 wt.% Pt loading. The Pt-loaded CeO₂ was dried at 70 °C for 4 h and then calcined at 500 °C for 4 h in flowing air to obtain the Pt/CeO₂ catalysts. The actual Pt content was determined by ICP (inductively coupled plasma) analysis. The detailed characterization results of the Pt/CeO₂ catalyst are available in [13].

The CeO₂-supported Cu single-atom catalyst (Cu₁/CeO₂) with 2wt.% Cu loading was prepared by the incipient-wetness-impregnation method and high-temperature calcination, as described in [14]. The CeO₂ support was prepared by thermal decomposition of Ce(NO)₃·6H₂O (99%, from Sigma-Aldrich) in air at 350 °C for 2 h. After loading Cu(NO₃)₂·2.5H₂O (Sigma-Aldrich) on the CeO₂ support by incipient wetness impregnation, the catalyst was dried in air at 150 °C for 1 h, followed by 800 °C calcination for 10 h. The detailed characterization results of this Cu₁/CeO₂ catalyst are available in [14]. A Pt₁/CeO₂ single-atom catalyst (with 1 wt.% Pt loading), as a control catalyst for Cu₁/CeO₂, was synthesized with the same method, using [Pt(NH₃)₄](NO₃)₂ as the Pt precursor. The Pt/CeO₂-Cu₁/CeO₂ catalyst mixture (1:1 mass ratio) was prepared by grinding the two catalysts together using a mortar and pestle.

The catalyst performance for isooctane oxidation was evaluated by temperatureprogramed reaction using a plug flow micro-reactor system, with the reactor effluent composition quantified using an FTIR gas analyzer (MKS, Multigas 2030). The catalyst powders were pressed, crushed, and sieved (180–250 μ m) for the tests. A total 150 mg of the Pt/CeO₂ catalyst (or 300 mg of the Pt/CeO₂-Cu/CeO₂ catalyst mixture) was mixed with 400 mg of SiC diluent and loaded in a quartz reactor (inner diameter ~10 mm) above a porous frit. The catalysts were tested with different gas compositions to evaluate the inhibition effects of different exhaust components (CO, NO, H₂O). The specific test conditions are listed in Table 2. The fully simulated exhaust conditions are based on the U.S. DRIVE protocols S-GDI (stoichiometric gasoline direct injection) [16]. The concentrations of CO, NO, and H₂ were adjusted from the original protocols based on the available gas-mixture source (5000 ppm CO/2000 ppm NO/1000 ppm H₂). The liquid isooctane and H₂O were introduced into vaporization zones located at the upstream of the reactor using a syringe infusion pump and an HPLC pump, respectively.

To evaluate and compare the stabilities of the Cu₁/CeO₂ and Pt₁/CeO₂ single-atom catalysts under the reduction condition, the pristine catalyst samples were pretreated in 1%CO/Ar at 275 °C for 30min. The CO-reduced catalysts were denoted as Cu₁/CeO₂-r and Pt₁/CeO₂-r, respectively. The CO-oxidation activities of the pristine and reduced catalysts were test by CO light-off experiments with a simplified condition (1%CO/4%O₂/Ar balance, 3 °C min⁻¹, space velocity 300 L (g_{cat} h)⁻¹), using a mixture of 20 mg catalysts and 500 mg SiC diluent. The catalysts were loaded into a 4.0-mm-i.d. × 40.64-cm-long quartz tube packed in-between inert quartz wool. The reactor effluent was analyzed using z GC2060 gas chromatograph model by Shanghai Ruimin GC Instruments, Inc.

4. Discussion

For the catalytic oxidation of isooctane on the Pt/CeO₂ catalyst under the fully simulated S-GDI condition, CO and NO were identified as the two major inhibitors in lowering the HC oxidation reactivity. These inhibition effects can be addressed by introducing catalytic sites or co-catalysts to preferentially convert CO or NO. The low-cost and stable Cu₁/CeO₂ single-atom catalyst, which is capable of completely converting CO below 200 °C under the fully simulated condition, can be added as a co-catalyst to eliminate the CO inhibitor. It is worth pointing out that the two types of catalytic sites, Cu single-atoms

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sites and Pt clusters, were integrated via physical mixing rather than co-impregnation of two sites on the same CeO₂ support. This is to avoid interactions between these two types of sites, such as the formation of a Pt-Cu alloy or the coverage of Cu single-atom sites by Pt clusters. For instance, a bi-metallic Pt/Cu₁/CeO₂ catalyst, which was prepared by loading Pt clusters on an as-synthesized Cu₁/CeO₂ single-atom catalyst, showed lower isooctane oxidation activity than both the Pt/CeO₂ catalyst and the Pt/CeO₂-Cu₁/CeO₂ mixture, with equivalent Pt loading (Figure S2). However, this bi-functional Pt/CeO₂-Cu₁/CeO₂ catalyst system has low activity for NO conversion, and thus the isooctane oxidation reactivity was not obviously improved in the presence of NO.

Because Pt/CeO_2 is capable of converting isooctane below 200 °C under the " O_2 only" condition (0.75% O_2 , Figure 1d), it would be ideal if NO could be eliminated below 200 °C so that the noble metal Pt/CeO_2 catalyst could be made best use of for HC oxidation. Potential methods for low-temperature NOx abatement include low-temperature HC-SCR (hydrocarbon-selective catalytic reduction), CO-NO reaction, and the use of PNA (passive NOx adsorber).

One potential approach is to incorporate low-temperature HC-SCR catalysts to utilize HCs to reduce NO_x . For instance, Ag/Al₂O₃ were reported to be active HC-SCR catalysts [19–21]. A wide range of HCs, including alkane, alkenes, and oxygenates, can serve as reductants for NO_x reduction on Ag/Al₂O₃. Although the operation temperature windows (>80% NOx conversion) are typically between 350 $^{\circ}$ C and 500 $^{\circ}$ C [20], it was found that the presence of H₂ can significantly improve the activity of Ag/Al₂O₃ and decrease the NO_x conversion temperature [21]. For example, on a 2 wt.%Ag/Al₂O₃ catalyst [19], >95% NO_x conversion was achieved at 200 °C, with octane as the reductant, in exhaust steam with a high H₂/NO ratio (720 ppm NO, 570 ppm C₈H₁₈, 4.3% O₂; 7200 ppm H₂, 7.2% H₂O). The mechanisms for the promotion effect of H_2 on HC-SCR activity are still under debate. Generally, two types of mechanisms were proposed: (1) H_2 reducing the Ag^+ species into the more active $Ag^{\delta+}$ or Ag^0 sites [22] and/or (2) H_2 modifying the nature and quantity of reaction intermediates [21]. However, the real exhaust contains less H_2 (e.g., 1670 ppm H₂ and 1000 ppm NO for the S-GDI condition [16]), and thus an HC-SCR catalyst with high activity under low H_2 concentration is needed for this approach. Alternatively, H_2 sources can be added to the aftertreatment system to provide sufficient H_2 to facilitate low temperature HC-SCR. For instance, a gas fuel reformer can be used to generated H_2 on board [23].

Another possible strategy is to promote a low-temperature (CO + NO) reaction by introducing a Rh_1/CeO_2 single-atom catalyst recently reported by Khivantsev et al. [24]. In this work, a 0.5 wt.% Rh_1/CeO_2 catalyst was reported to complete the NO abatement above 120 °C in a (460 ppm NO + 1750 ppm CO) stream. This single Rh atom was demonstrated to be an economic noble-metal catalyst for low-temperature NO removal, although its performance in the presence of O_2 is yet to be testified. In summary, the low-temperature oxidation of hydrocarbon in real engine exhaust would require the incorporation of multiple catalyst systems, to address the reaction inhibitors.

5. Conclusions

In this work we systematically analyzed the inhibition effects of other components on the catalytic oxidation of isooctane on Pt/CeO_2 catalysts under the fully simulated exhaust condition (S-GDI). It was found that CO and NO are the two major inhibitors for low-temperature isooctane oxidation. The development of catalysts for hydrocarbon abatement should not only focus on promoting the intrinsic activity for hydrocarbon oxidation, but also on addressing the reaction inhibition by other exhaust components.

The introduction of a low-cost Cu_1/CeO_2 single-atom catalyst, which is highly active for low-temperature CO oxidation (<200 °C), even under the fully simulated exhaust condition, successfully eliminates the inhibition effect of CO on the noble metal Pt/CeO₂ catalyst for isooctane oxidation. However, the unconverted NO still strongly inhibits the low-temperature oxidation of isooctane. To further eliminate the inhibition effect of NO, so as to achieve low-temperature hydrocarbon in real engine exhaust, we propose that future work can be focused on exploring catalytic sites for low-temperature NO_x conversion (<200 °C) or the integration of a NO_x removal system into the upstream of the hydrocarbon oxidation catalyst.

Supplementary Materials: The following supporting information can be downloaded at: https: //www.mdpi.com/article/10.3390/catal13030508/s1, Figure S1: Comparison of isooctane oxidation activity of Pt/CeO₂+Cu₁/CeO₂ catalyst mixture under the O₂+NO+CO and S-GDI conditions; Figure S2: Activity of a bi-metallic Pt/Cu₁/CeO₂ catalyst.

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