Supporting Information

Bimetallic Pt-Co catalysts for the liquid-phase WGS

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Figure S1. Nitrogen isotherms (A) and pore size distribution (B) of the calcined (solid lines) and reduced (dashed lines) samples.





Figure S2. EDX spectrum of reduced samples (A) CoAl (B) 0.3Pt/CoAl (C) 1PtCoAl and (D) 0.3Pt/Al.



Figure S3. XPS spectra corresponding to Pt 4d_{5/2}.



Figure S4. Outlet molar concentration of products during WGS reaction in the absence of hydrogen (H₂/CO = 0). Reaction conditions: 260 °C/50 bar; W_{cat} (0.2 g), water flow (0.04mL/min), CO flow (3.5 mL/min, STP).



Figure S5. Outlet molar concentration of products during WGS experiments at different H₂/CO ratio. Reaction conditions: 260 °C/50 bar; W_{cat} (0.2 g), water flow (0.04mL/min), CO flow (3.5 mL/min, STP); H₂/CO=4/3 (0-10 h), H₂/CO =7/3 (11-20 h) and H₂/CO=4 (21-30 h).



Figure S6. Outlet molar concentration of products during WGS experiments at different temperature and pressure over Pt/CoAl. Reaction conditions: W_{cat} (0.2 g), water flow (0.04mL/min), CO flow (3.5 mL/min, STP), H₂ flow (14 mL/min, STP). Upper part: temperature variation (220, 235, 245, 260 °C) and 50 bar. Lower part: pressure variation (25, 35, 40, 50 bar) and 220 °C.

Table 1S. List of apparent activation energies reported in this work and in the literature for Pt catalysts.

Catalysts	Ea (kJ/mol)	Operating conditions	Reference	
0.3%Pt/CoAl	51.5	220-260 °C, liquid-phase	This work	
C03O4	91.0	180-280 °C, gas-phase		
0.2%Pt/Co ₃ O ₄	50.1	50.1 150-200 °C, gas-phase		
0.2%Pt/Co ₃ O ₄	24.8	300-350 °C, gas-phase		
1%Pt/Al ₂ O ₃	68	285 °C, gas-phase	[2]	
0.9% Pt/CeO ₂ /Al ₂ O ₃	70			
1.5% Pt/ZrO ₂	58			
2% Pt/CeO ₂	65	250-350 °C, gas-phase	[3]	
1.9% Pt/TiO ₂	23			
1.5% Pt/Fe ₂ O ₃	44			

Table 2S. Liquid holdup (EL), vapor composition and liquid/vapor distribution of CO and H2.

exp #	H2/CO	T (°C)	P (bar)	£L (%)	Р _{н20} (bar)	Pco (bar)	Р _{н2} (bar) -	Liquid/vapor	
								distribution (mol/mol)	
								СО	H_2
1	0	260	50	16.4	47.36	2.64	0	$1.05 \cdot 10^{-04}$	0
2	4/3	260	50	16.2	47.36	1.13	1.51	$4.49 \cdot 10^{-05}$	$1.13 \cdot 10^{-04}$
3	7/3	260	50	16.1	47.36	0.79	1.85	$3.14 \cdot 10^{-05}$	$7.88 \cdot 10^{-05}$
4	12/3	260	50	15.8	47.36	0.53	2.11	2.11.10-05	5.29.10-05
5	12/3	245	50	18.8	36.78	2.64	10.58	$1.13 \cdot 10^{-04}$	$2.71 \cdot 10^{-04}$
6	12/3	235	50	15.8	30.78	3.84	15.38	$1.72 \cdot 10^{-04}$	$4.03 \cdot 10^{-04}$
7	12/3	220	50	15.8	23.2	5.36	21.44	2.60.10-04	$5.80 \cdot 10^{-04}$
8	12/3	220	40	15.3	23.2	3.36	13.44	$1.63 \cdot 10^{-04}$	$3.64 \cdot 10^{-04}$
9	12/3	220	35	15.1	23.2	2.36	9.44	$1.14 \cdot 10^{-04}$	$2.55 \cdot 10^{-04}$
10	12/3	220	25	14.4	23.2	0.36	1.44	$1.74 \cdot 10^{-05}$	3.89.10-05

Liquid holdup (EL) was estimated according to reference [4].

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