



Article Optimized Integer Aperture Bootstrapping for High-Integrity CDGNSS Applications

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Abstract: Integer Aperture Bootstrapping (IAB) is a crucial method for testing ambiguity acceptance in carrier-phase differential global navigation satellite system (CDGNSS) positioning. It has the advantage that integrity parameters, such as the failure rate, can be analytically calculated, which is essential in safety-of-life applications. Although the IAB methods have been extensively studied, their threshold-determining method is still not well explained, theoretically. In this study, a new method, named Analytical Integer Aperture Bootstrapping (AIAB), is theoretically derived to determine the optimal IAB threshold. AIAB is novel in that: (1) a precise and easy-to-compute expression has been developed to describe the relationship between the IAB threshold and the failure rate, (2) an analytical function model has been derived from the expression to determine the IAB threshold; moreover, the function model is simplified, and (3) a data-constraint approach has been proposed to reduce the complexity of IAB. In the global CDGNSS simulations, AIAB is shown to outperform the existing IAB methods under both strong and weak models, particularly at low fix rates, which are 23% to 40% higher than the basic IAB method. The Monte Carlo simulation results show that AIAB can obtain almost theoretically the same performance as Optimal Integer Aperture (OIA).

Keywords: Integer Aperture Bootstrapping; ambiguity acceptance test; integrity; CDGNSS

1. Introduction

Provided that the correct integer ambiguities are fixed, CDGNSS can achieve decimeterto-centimeter-level positioning accuracy, which is demanded by precision approaches and (shipboard) landing of aircraft [1], intelligent transportation systems of land vehicles [2], rail traffic management systems of trains [3], the port approach of shipboards [4], and other safety-of-life (SoL) applications. In addition to high accuracy, SoL applications demand extremely high liability and reliability, as measured by integrity, which is achieved by employing the alert limit (AL), integrity risk (IR), and time to alert (TTA). IR, or the probability of integrity failures in which the position error exceeds the AL without alert within TTA, must be strictly satisfied in SoL applications. However, the incorrect integer fix may introduce uncontrollable positioning errors in CDGNSS. Therefore, the failure rate, also known as the probability of the incorrect integer fix, must comply with the allocated IR requirement. For example, as IR is 10^{-7} for landing, an acceptable failure rate is allocated to be in the order of 10^{-8} or even smaller [5]. In summary, the integrity monitoring (IM) of ambiguity resolution is a significant and challenging aspect of SoL in CDGNSS.



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). The IM of ambiguity resolution aims to enable the failure rate to meet the demandingly allocated IR. The GERAFS [6] and the EPIC [5,7] were proposed to determine the integrity risk based on the CDGNSS underlying model and the integer estimator [8]. Unfortunately, these methods can only assess the prior failure rate, not reduce it. When the CDGNSS model is not strong enough, the availability of these methods is severely limited. To enhance the availability, the integer aperture (IA) was used to control the failure rate by the ambiguity acceptance test [9]. Given a specific IA estimator, the failure rate can be controlled by the test threshold (also known as the aperture parameter). Therefore, the method for determining the aperture parameter is crucial for ensuring integrity monitoring. This can be classified into five categories: empirical, Monte Carlo, look-up table, function, and analytical approaches.

The empirical approach determines a constant aperture parameter depending on the particular scenario [10]. The approach has been widely used in practical applications due to its simplicity. However, it cannot be applied to SoL applications due to its lack of theoretical basis for integrity.

The integer least-squares (ILS) method has the highest success rate [11], and as a result, many ILS-based IA estimators have been proposed. However, most of them, e.g., the ratio test [12] and the difference test [13,14], do not have an analytical relationship between the aperture parameter and the failure rate because of the irregular regions of these IA estimators. Therefore, the Monte Carlo approach is used to determine the aperture parameter based on the failure rate by simulation statistics [15,16]. However, this approach is computationally complex and does not meet the real-time requirements of the SoL applications.

To decrease the computational complexity of the Monte Carlo method, two alternative approaches have been developed to express the aperture parameter as an approximate function of the failure rate and the feature parameters of the CDGNSS model. These are the look-up table [17] and function approach [18,19], which fit the Monte Carlo simulation samples in advance. However, it is important to note that these methods do not guarantee that the allocated IR is always satisfied for any satellite geometry.

Unlike the above approaches, the analytical approach can meet the allocated IR based on a strict analytical relationship between the aperture parameter and the failure rate. In most cases, this approach is based on an IA estimator method, named Integer Aperture Bootstrapping (IAB), which has a suboptimal success rate and an analytical failure rate function of the aperture parameter [20–22]. Additionally, the analytical approach can be based on an IA estimator named Ellipsoidal IA [23]. However, the success rate of Ellipsoidal IA is usually lower than that of IAB due to the possible overlap of the pull-in region, which is determined by the aperture parameter. Under the IAB framework, the Generalized IAB (GIAB) has been presented to satisfy the stringent integrity requirements of SoL [24–26]. The key problem of the analytical approach is the computational complexity of the inverse operation of the failure rate function. To address this issue, GIAB assigns an overall failure rate to every ambiguity and sets the aperture parameter as a simple analytical function of the allocated failure rate. The performance of GIAB is directly influenced by the allocation weighting function, which is chosen using heuristics rather than theoretical derivation. The performance of GIAB is directly influenced by the allocation weighting function, which is chosen using heuristics rather than theoretical derivation. Therefore, GIAB can only provide near-optimal performance. A more effective method is the Integrity Monitoring Ratio Test (IM-RT), which uses protection levels to minimize false alarms and missed detections [27].

This paper aims to develop a real-time analytical approach that performs with high integrity under the IAB framework. To achieve this, three problems must be addressed. Firstly, an analytical failure rate function of the aperture parameter must be found, which strictly meets the demandingly allocated IR. Secondly, the optimal aperture parameter relationship must be derived theoretically, which determines the shape of the pull region. The third step is to calculate the aperture parameter by combining the inverse of the failure

rate function from the first step with the relationship described in the second step. This relationship determines the size of the pull region, but it can be computationally challenging due to the use of the inverse function.

As noted above, the IAB has solved the first problem because its failure rate can be accurately calculated. Although GIAB has provided an analytical approach to solve the second and third problems, the approach has not been proven optimal theoretically. In response, a new analytical approach based on the IAB, named Analytical Integer Aperture Bootstrapping (AIAB), is developed here to set the aperture parameter theoretically with low computational complexity. The main contributions of this paper are as follows: Firstly, we briefly describe the previously existing IAB framework. Secondly, a theoretical derivation for a simplified analytical upper bound on the failure rate of the aperture parameter is probabilistically formulated. Finally, based on the upper bound on the failure rate, a constraint function is theoretically derived to describe the optimal IAB aperture parameter relationship and is further simplified to meet the practical applications. Furthermore, a new approach based on data constraint is proposed to avoid the computational complexity problem.

2. IAB Overview

This section briefly introduces IAB approaches from [20–22], with some amplifications for clarity and notational consistency. Conceptually, IAB approaches can be divided into four steps.

2.1. Float Solution Estimation

All the linearized GNSS measurement models can be given as:

$$y = Aa + Bb + v \tag{1}$$

where *y* is the m-vector of both code and carrier phase measurements, *a* is the *n*-vector of unknown integer parameters, *b* is the *q*-vector of unknown real-valued parameters, and *v* is the m-vector of measurement noise, which is usually assumed following the normal distribution with the variance–covariance matrix denoted as Q_{yy} . *A* and *B* are the design matrices of *a* and *b*, respectively.

Applying the weighted least-squares estimation to obtain float solutions \hat{a} and \hat{b} with the variance–covariance matrix denoted as $Q_{\hat{a}}$ and $Q_{\hat{b}}$, respectively, yields:

$$\begin{bmatrix} Q_{\hat{a}} & Q_{\hat{a}\hat{b}} \\ Q_{\hat{b}\hat{a}} & Q_{\hat{b}} \end{bmatrix} = \left(H^T W H \right)^{-1},$$
(2b)

where H = [A B] and $W = Q_{yy}^{-1}$.

2.2. Integer Ambiguity Resolution by Integer Bootstrapping

Integer ambiguity resolution can transform the float ambiguity into a corresponding integer ambiguity. Integer ambiguity resolution is related to float ambiguity, mapping, and the variance–covariance matrix. The process is described in [21] as:

$$\check{a} = S_{IB}(\hat{a}, Q_{\hat{a}}) \tag{3a}$$

$$S_{IB}: \mathbb{R}^m \to \mathbb{Z}^n$$
, (3b)

where \check{a} is the *n*-vector of the resolved integer ambiguity, called fixed ambiguity, and S_{IB} is the Integer Bootstrapping (IB) mapping.

The strong correlation of ambiguity can lead to low performance of the IB estimation, so the ambiguities are decorrelated by the Z-Transform [28,29] in the IB. The Z-

$$\hat{z} = Z^T \hat{a} \tag{4a}$$

$$Q_{\hat{z}} = Z^T Q_{\hat{a}} Z \tag{4b}$$

where *Z* is the integer-preserving transformation matrix, \hat{z} is the vector of decorrelated float ambiguity, and $Q_{\hat{z}}$ is the variance–covariance of the decorrelated float ambiguity.

Applying S_{IB} to \hat{z} and $Q_{\hat{z}}$ produces decorrelated integer ambiguity, as:

$$\check{z} = S_{IB}(\hat{z}, Q_{\hat{z}}) \tag{5}$$

where \check{z} is the vector of decorrelated integer ambiguity.

 S_{IB} is determined by IB, which follows from a sequentially conditional least-squares adjustment. The computation process [21] is as follows.

Firstly, using the triangular factorization to decompose the covariance of the float ambiguities as:

$$Q_{\hat{z}} = LDL^{T} \tag{6a}$$

$$L_{i,j} = \begin{cases} 0 & 1 \le i < j \le n \\ 1 & i = j \\ l_{i,j} & 1 \le j < i \le n \end{cases}$$
(6b)

$$D_{i,j} = \begin{cases} 0 & i \neq j \\ d_i^2 & i = j \end{cases}$$
(6c)

where *L* is a unit lower triangular matrix reflecting the residue correlation of the decorrelated float ambiguity, and *D* is a diagonal matrix denoting the conditional variance. $L_{i,j}$ and $D_{i,j}$ are the elements of the matrix.

Secondly, let \hat{z}_{IB} be the sequential conditional least-squares estimator of \hat{z} , and let \dot{z} be the vector of the correct decorrelated integer ambiguity. Then, \hat{z} and \hat{z}_{IB} are related by L as:

$$\hat{z} - \dot{z} = L(\hat{z}_{IB} - \dot{z}) \tag{7}$$

Finally, all the integer ambiguities are fixed sequentially as:

where [.] denotes the nearest integer rounding, and $\check{z}_{IB,i}$, $\hat{z}_{IB,i}$, and \hat{z}_i are the elements of \check{z}_{IB} , \hat{z}_{IB} , and \hat{z} , respectively, with $1 \le i \le n$.

2.3. Ambiguity Acceptance Test by IA

IAB tests the ambiguity residual by the aperture parameter. Let $\tau = (\tau_1, \tau_2, ..., \tau_n)^T$ be the vector of the ambiguity residual, let $K = (k_1, k_2, ..., k_n)^T$ be the vector of the aperture parameter, and let k_i and τ_i be the elements of K and τ , respectively, where $1 \le i \le n, 0 \le k_i \le 1$, and $-0.5 < \tau_i \le 0.5$. If $|\tau_i| \le \frac{k_i}{2}$, $\check{z}_{IB,i}$ is accepted or rejected. All the residuals are tested sequentially.

It is clearly shown that the aperture parameter determines the performance of the IAB, so "how to determine the aperture parameter" is the key issue in the IAB. There are two existing IAB methods, termed Basic IAB and GIAB, used as the control methods in our study. Basic IAB sets all the elements of *K* to the same value [22]. Meanwhile, GIAB

allocates a failure rate, P_F , to each ambiguity error rate, P_{Ei} , using a weight function, and then computes the k_i by the allocated failure rate, P_{Ei} [24,25], as:

$$P_{Cj} = 2\Phi\left(\frac{k_i}{2d_i}\right) - 1 \tag{9a}$$

$$P_F = P_{E1} + \sum_{i=2}^{n} \left(P_{Ei} \prod_{j=1}^{i-1} P_{Cj} \right)$$
(9b)

$$P_{Ei}(w_i P_F) = \begin{cases} w_1 P_F & i = 1\\ \frac{w_i P_F}{\prod_{i=1}^{i-1} P_{C_i}} & i > 1 \end{cases}$$
(9c)

where Φ denotes the cumulative normal distribution.

2.4. Fixed Solution Resolution

If the fixed ambiguity is accepted by IA, the real-valued parameters \check{a} and \check{b} can be updated with:

$$\check{a} = Z^{-1}\check{z}_{IB} \tag{10a}$$

$$\check{b} = \hat{b} - Q_{\hat{h}\hat{a}} Q_{\hat{a}}^{-1} (\hat{a} - \check{a})$$
 (10b)

3. IAB Event Probabilities Based on an Upper Bound on the Failure Rate

In this section, a simplified failure rate upper bound function of the aperture parameter is derived on the hypothesis of weak correlation of the decorrelated ambiguities. Then, the probabilities of the other events are analyzed based on this simplified function.

3.1. IAB Events

IAB has four mutually exclusive and independent outcome events (success, failure, false alarm, and detection) [30,31]. The success event, H_S , occurs upon acceptance of the correct integer, the failure event, H_F , occurs upon acceptance of any incorrect integers, the false-alarm event, H_E , occurs upon rejection of the correct integer, and the detection event, H_D , occurs upon rejection of any incorrect integer. Let $\epsilon = \hat{z}_{IB} - \dot{z}$ be the vector of the float ambiguity error. The regions corresponding to H_S , H_F , H_E , and H_D events are illustrated in Figure 1.



Figure 1. Regions of the float ambiguity error, mapped by the IAB to success, failure, false-alarm, and detection events for a two-dimensional example model.

6 of 20

3.2. Simplified Function to Compute the Upper Bound of Failure Rate

The failure event probability, termed the failure rate, is an important integrity parameter. IAB has the advantage that its failure rate can be computed and controlled by the aperture parameter, K, as follows.

Let $\Delta z = \check{z}_{IB} - \dot{z}$ be the vector of the integer ambiguity error, and the probability of the acceptance of the ambiguity with integer error, Δz , is given as [22]:

$$P(\Delta z|IAB) = \prod_{i=1}^{n} \left(\Phi\left(\frac{k_i - 2L_i \Delta z}{2d_i}\right) - \Phi\left(\frac{-k_i - 2L_i \Delta z}{2d_i}\right) \right)$$
(11)

where L_i is the i-th row of L.

The failure rate, P_F , is the probability of acceptance of all the incorrect integers [22], as:

$$P_F = P(H_F) = \sum_{\Delta z \neq 0^n \text{ and } \Delta z \in Z^n} P(\Delta z | IAB)$$
$$= \sum_{\Delta z \neq 0^n \Delta z \in Z^n} \prod_{i=1}^n \left(\Phi\left(\frac{k_i - 2L_i \Delta z}{2d_i}\right) - \Phi\left(\frac{-k_i - 2L_i \Delta z}{2d_i}\right) \right)$$
(12)

Since (12) contains an infinite number of items, it is impossible to compute the true value of P_F . However, a precise estimation of P_F can be obtained by calculating only the: $\prod_{i=1}^{n} \left(\Phi\left(\frac{k_i - 2L_i \Delta z}{2d_i}\right) - \Phi\left(\frac{-k_i - 2L_i \Delta z}{2d_i}\right) \right),$ with a high probability.

The computations of (12) may be complex with a weak CDGNSS model. In our study, a probability estimation based on weak correlation is proposed to reduce the computational complexity, as follows.

The P_F can be expressed as:

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$$P_F = \sum_{\Delta z \in \mathbb{Z}^n} P(\Delta z | IAB) - P(0^n | IAB)$$
(13)

Clearly, P_F can be easily obtained as $\sum_{\Delta z \in Z^n} P(\Delta z | IAB)$ is calculated.

On the hypothesis of a weak correlation of decorrelated ambiguities, Δz and Δz_i are related by L_i as:

$$L_i \Delta z \approx \Delta z_i \tag{14}$$

where Δz_i denotes the i-th integer element of Δz .

Then, $\sum_{\Delta z \in \mathbb{Z}^n} P(\Delta z | IAB)$ can be expressed as:

$$\sum_{\Delta z \in \mathbb{Z}^{n}} P(\Delta z \mid IAB) = \sum_{\Delta z \in \mathbb{Z}^{n}} \prod_{i=1}^{n} \left(\Phi\left(\frac{k_{i}-2L_{i}\Delta z}{2d_{i}}\right) - \Phi\left(\frac{-k_{i}-2L_{i}\Delta z}{2d_{i}}\right) \right)$$

$$\approx \sum_{\Delta z \in \mathbb{Z}^{n}} \prod_{i=1}^{n} \left(\Phi\left(\frac{k_{i}-2\Delta z_{i}}{2d_{i}}\right) - \Phi\left(\frac{-k_{i}-2\Delta z_{i}}{2d_{i}}\right) \right)$$

$$= \prod_{i=1}^{n} \sum_{\Delta z_{i} \in \mathbb{Z}^{1}} \left(\Phi\left(\frac{k_{i}-2\Delta z_{i}}{2d_{i}}\right) - \Phi\left(\frac{-k_{i}-2\Delta z_{i}}{2d_{i}}\right) \right)$$

$$= \prod_{i=1}^{n} \sum_{l \in \mathbb{Z}^{1}} \left(\Phi\left(\frac{k_{i}-2l}{2d_{i}}\right) - \Phi\left(\frac{-k_{i}-2l}{2d_{i}}\right) \right)$$
(15)

Let
$$F_i(k_i) = \sum_{l \in \mathbb{Z}^1} \left(\Phi\left(\frac{k_i - 2l}{2d_i}\right) - \Phi\left(\frac{-k_i - 2l}{2d_i}\right) \right)$$
 and $F_{i,j}(k_i) = \Phi\left(\frac{k_i - 2l}{2d_i}\right) - \Phi\left(\frac{-k_i - 2l}{2d_i}\right)$ then:

$$\sum_{\Delta z \in Z^n} P(\Delta z | IAB) = \prod_{i=1}^n F_i(k_i)$$
(16a)

$$P(0^{n}|IAB) = \prod_{i=1}^{n} F_{i,0}(k_{i})$$
(16b)

$$P_F = \prod_{i=1}^{n} F_i(k_i) - \prod_{i=1}^{n} F_{i,0}(k_i)$$
(16c)

The calculation of $F_i(k_i)$ is not possible directly due to its infinite number of items. However, an approximate value can be calculated as follows:

$$F_i(k_i) = \sum_{l \in \mathbb{Z}^1} F_{i,l}(k_i) = \sum_{l \in [-N:N]} F_{i,l}(k_i) + \sum_{l \in [-\infty:-N-1]} F_{i,l}(k_i) + \sum_{l \in [N+1:\infty]} F_{i,l}(k_i)$$
(17)

Thus,

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$$\sum_{l \in [-\infty:n-1]} F_{i,l}(\mathbf{k}_i) = \sum_{l \in [n+1:\infty]} F_{i,l}(\mathbf{k}_i) < \Phi\left(\frac{k_i - 2N + 2}{2d_i}\right)$$
(18a)

$$\sum_{i \in [-N:N]} F_{i,l}(k_i) + 2\Phi\left(\frac{k_i - 2N + 2}{2d_i}\right) \ge F_i(k_i) \ge \sum_{l \in [-N:N]} F_{i,l}(k_i)$$
(18b)

The upper and lower bounds on $F_i(k_i)$ can be accurately estimated according to the formula, and the estimated error range can be determined by $2\Phi\left(\frac{k_i-2N+2}{2d_i}\right)$. Conservatively, an upper bound on the failure rate can be expressed as:

$$P_{F} = \prod_{i=1}^{n} F_{i}(k_{i}) - \prod_{i=1}^{n} F_{i,0}(k_{i})$$

$$= \prod_{i=1}^{n} \sum_{l \in [-N:N]} \left(\Phi\left(\frac{k_{i}-2l}{2d_{i}}\right) - \Phi\left(\frac{-k_{i}-2l}{2d_{i}}\right) \right)$$

$$+ 2\Phi\left(\frac{k_{i}-2N+2}{2d_{i}}\right) - \prod_{i=1}^{n} \left(\Phi\left(\frac{k_{i}}{2d_{i}}\right) - \Phi\left(\frac{-k_{i}}{2d_{i}}\right) \right)$$
(19)

Compared to (12), (19) can drastically reduce the amount of computation by exchanging the order of addition and multiplication.

To validate the simplified function for the failure rate, we compared the true P_F value obtained by (12) with the correlation matrix, L, the conditional-variance matrixes, D, and the aperture parameter, K, in two dimensions, with the approximate P_F values obtained by (19), where $L = \begin{bmatrix} 1 & 0 \\ l_{1,2} & 1 \end{bmatrix}$, $D = \begin{bmatrix} d & 0 \\ 0 & d \end{bmatrix}$, and $K = \begin{bmatrix} k \\ k \end{bmatrix}$. It can be found in Figure 2 that:

- (a) The approximate P_F is always higher than the true P_F , so the simplified function (19) can obtain the upper bound on the failure rate.
- (b) The accuracy of the approximation of the failure rate is proportional to the aperture parameter value and inversely proportional to the conditional variance value and correlation value, with the range of the correlation value being 0 to 0.5.



Figure 2. Cont.



Figure 2. True failure rate value vs. approximate failure rate value. (a) True P_F value vs. approximate P_F value, with a weak correlation value of $l_{1,2} = 0.1$. (b) True P_F value vs. approximate P_F value, with a middle correlation value of $l_{1,2} = 0.3$. (c) True P_F value vs. approximate P_F value, with a strong correlation value of $l_{1,2} = 0.5$.

3.3. Probabilities of the Other IAB Events

The probability of a success event, H_S , denoted as P_S , can be expressed as:

$$P_S = P(H_S) = P(0^n | IAB) = \prod_{i=1}^n \left(\Phi\left(\frac{k_i}{2d_i}\right) - \Phi\left(\frac{-k_i}{2d_i}\right) \right)$$
(20)

The probability of a false-alarm event, H_E , denoted as P_E , can be expressed as:

$$P_E = P(H_E) = P(0^n | IB) - P(0^n | IAB)$$

=
$$\prod_{i=1}^n \left(\Phi\left(\frac{1}{2d_i}\right) - \Phi\left(\frac{-1}{2d_i}\right) \right) - \prod_{i=1}^n \left(\Phi\left(\frac{k_i}{2d_i}\right) - \Phi\left(\frac{-k_i}{2d_i}\right) \right)$$
(21)

where $P(0^n | IB)$ is the probability of fixing the correct integer ambiguity in *IB*.

As P_S , P_E , and P_F can be computed, the probability of detection event, H_D , denoted as P_D , can be expressed as:

$$P_D = P(H_D) = 1 - P_S - P_E - P_F$$
(22)

The fix rate, denoted as P_A , is the probability of the fix event occurring upon acceptance of any integer. P_A can be expressed as:

$$P_A = P_S + P_E \tag{23}$$

In addition to the above parameters, the following two conditional probabilities are usually used in integrity:

(a) The missing detection rate, P_{MD} , is the conditional probability of a failure event given the event that occurs upon acceptance of any integer:

$$P_{MD} = P(H_F | (H_F + H_S)) = \frac{P_F}{P_S + P_F}$$
(24)

(b) The false-detection rate, *P_{FD}*, is the conditional probability of a false-alarm event given the event that occurs upon rejection of any integer:

$$P_{FD} = P(H_E | (H_E + H_D)) = \frac{P_E}{P_E + P_D}$$
(25)

4. AIAB Optimal Aperture Shape Based on the Upper Bound on the Failure Rate

This section derives a constraint function to describe the optimized aperture relationship that determines the AIAB aperture shape. The constraint function is then simplified to reduce computational complexity.

4.1. The AIAB Constraint Function

IAB is an integrity-monitoring method that aims to reduce the integrity risk by increasing the availability risk. Figure 3 shows that although the false-alarm rate increased, the failure rate decreased in IAB.





The optimal IAB aperture parameter should provide the lowest false-detection rate for a given missed detection rate, $P_{MD,alloc}$, as:

S

$$arg min[P_{FD}]$$

$$t.P_{MD} = P_{MD,alloc}$$
(26)

where
$$P_{FD} = \frac{\prod_{i=1}^{n} F_{0,i}(1) - \prod_{i=1}^{n} F_{0,i}(k_i)}{\prod_{i=1}^{n} F_{0,i}(1)} = 1 - \frac{\prod_{i=1}^{n} F_{0,i}(k_i)}{\prod_{i=1}^{n} F_{0,i}(1)}$$
 and $P_{MD} = \frac{\prod_{i=1}^{n} F_{i}(k_i) - \prod_{i=1}^{n} F_{0,i}(k_i)}{\prod_{i=1}^{n} F_{i}(k_i)}$
 $1 - \frac{\prod_{i=1}^{n} F_{0,i}(k_i)}{\prod_{i=1}^{n} F_{i}(k_i)}$.
Equation (26) can be equated as:

$$arg \max[\prod_{i=1}^{n} F_{0,i}(k_i)]$$

s.t.
$$\frac{\prod_{i=1}^{n} F_{0,i}(k_i)}{\prod_{i=1}^{n} F_i(k_i)} = 1 - P_{md,alloc}$$
 (27)

The Lagrange multiplier calculator is used to locate the maxima of the function $\prod_{i=1}^{n} F_{0,i}(k_i)$ that is subject to $\frac{\prod_{i=1}^{n} F_{0,i}(k_i)}{\prod_{i=1}^{n} F_i(k_i)} = 1 - P_{md,alloc}$, as follows. The formula of the Lagrange multiplier is:

 $L(k_1, \dots, k_n, \lambda) = \prod_{i=1}^n F_{0,i}(k_i) + \lambda \left(\frac{\prod_{i=1}^n F_{0,i}(k_i)}{\prod_{i=1}^n F_i(k_i)} - 1 + P_{md,alloc}\right)$ (28)

Set the gradient of $L(k_1, ..., k_n, \lambda)$ equal to the zero vector as:

$$\frac{\frac{\partial L(k_1,...,k_n,\lambda)}{\partial k_j}}{F_{0,j}(k_j)} = \frac{f_{0,i}(k_j)}{F_{0,j}(k_j)} \prod_{i=1}^n F_{0,i}(k_i) + \lambda \frac{\frac{f_{0,i}(k_j)}{F_{0,j}(k_j)} \prod_{i=1}^n F_{0,i}(k_i) - \frac{f_j(k_j)}{F_j(k_j)} \prod_{i=1}^n F_{0,i}(k_i)}{\prod_{i=1}^n F_i(k_i)} = 0$$
(29)

Equation (29) can be simplified as:

$$\frac{1}{\lambda} \prod_{i=1}^{n} F_i(k_i) - 1 = \frac{f_{j,0}(k_j) / f_j(k_j)}{F_{j,0}(k_j) / F_j(k_j)}$$
(30)

Finally, the optimal IAB aperture parameter relationship can be obtained as:

$$\frac{F_{i,0}(k_i)/F_i(k_i)}{f_{i,0}(k_i)/f_i(k_i)} = \frac{F_{j,0}(k_j)/F_j(k_j)}{f_{i,0}(k_j)/f_j(k_j)}$$
(31)

where *i* and *j* denote the subscripts corresponding to the integer ambiguities.

Similarly, it can be proven that Equation (31) also satisfies the following:

- (a) Subject to a given fix rate or a given success rate, locate the minimum of the false-alarm rate, false-detection rate, missed detection rate, and failure rate.
- (b) Subject to a given false-alarm rate or a given false-detection rate, locate the minimum of the missed detection rate and failure rate and the maximum of the fix rate and success rate.
- (c) Subject to a given missed detection or a given failure rate, locate the minimum of the false-alarm rate and failure rate, and the maximum of the fix rate and success rate.

It can be seen that (31) provides the optimal aperture shape under weak correlation assumptions of the integer ambiguities.

Therefore, the AIAB constraint function can be defined as:

$$R_{basic}(k_i, d_i) = \frac{F_{i,0}(k_i) / F_i(k_i)}{f_{i,0}(k_i) / f_i(k_i)}$$
(32)

The function is also called the basic R-value function. Let the (32) function value be the R-value. As can be seen from Figure 4, for a given value of *d*, the R-value is monotonically increasing with the aperture parameter, which implies that there is a one-to-one correspondence between the R-value and the aperture parameter. The range of the R-value is 1 to $\frac{F_{i,0}(1_i)/F_i(1)}{f_{i,0}(1)/f_i(1)}$, where $\frac{F_{i,0}(1_i)/F_i(1)}{f_{i,0}(1)/f_i(1)} < 2$ and $\frac{F_{i,0}(1_i)/F_i(1)}{f_{i,0}(1)/f_i(1)}$ is inversely proportional to *d*. The key of AIAB is to let the R-value of different integer ambiguities be the same,

The key of AIAB is to let the R-value of different integer ambiguities be the same, but it needs to take into account the range of the R-value. When the R-value exceeds its maximum value range, the corresponding aperture parameter is set to 1.



Figure 4. R-value with different aperture parameter values and *d* values.

4.2. The Simplified AIAB Constraint Function

The calculation and inversion of the R-value function (32) is very complex and can be considered to simplify it. As $F_{i,0}(k_i)$ and $F_i(k_i)$ are less sensitive than $f_{i,0}(k_i)$ and $f_i(k_i)$ to the aperture parameter with $F_{i,0}(k_i)/F_i(k_i) \approx 1$, the simplified R-value function can be expressed as:

$$R_{f/f0}(k_i, d_i) = \frac{1}{f_{i,0}(k_i)/f_i(k_i)} = f_i(k_i)/f_{i,0}(k_i)$$
(33a)

The simplified R-value function is compared with other simplified functions, as follows:

$$R_{F0/F}(k_i, d_i) = F_{i,0}(k_i) / F_i(k_i)$$
(33b)

$$R_{F0/f0}(k_i, d_i) = F_{i,0}(k_i) / f_{i,0}(k_i)$$
(33c)

Similarly, the R-value function of the Basic IAB can be defined as:

$$R_{BasicIAB}(k_i, d_i) = k_i \tag{33d}$$

The above R-values were normalized by R_{basic} to compare the similarity with the AIAB basic constraint function in Figure 5a,b. It is shown that the similarity between the $R_{f/f0}$ and R_{basic} was the highest in both strong and weak CDGNSS models. However, the similarity slightly decreased in the weak GNSS model. Additionally, $R_{BasicIAB}$ exhibited the lowest similarity to R_{basic} .



Figure 5. The similarity of simplified functions to the basic AIAB constraint function in the strong CDGNSS model, with d = 0.25(cycle) and d = 1.0(cycle). (**a**) d = 0.25(cycle) and (**b**) d = 1.0(cycle).

The $R_{f/f0}$ function (33a) can be further simplified as follows:

(a) $f_{i,0}(k_i)$ can be expressed as:

$$f_{i,0}(k_i) = \frac{pdf_{norm}\left(\frac{0.5k_i}{d_i}\right) + pdf_{norm}\left(-\frac{0.5k_i}{d_i}\right)}{2} = \frac{1}{\sqrt{2\pi}d_i}exp\left(-\frac{1}{2}\left(\frac{k_i}{2d_i}\right)^2\right)$$
(34)

where pdf_{norm} denotes the normal probability density function formula. (b) $f_i(k_i)$ can be expressed as:

$$f_{i}(k_{i}) = \sum_{l \in \mathbb{Z}^{1}} f_{i,l}(k_{i}) \approx f_{i,0}(k_{i}) + f_{i,-1}(k_{i}) + f_{i,1}(k_{i})$$

$$= \frac{1}{\sqrt{2\pi}d_{i}} exp\left(-\frac{1}{2}\left(\frac{k_{i}}{2d_{i}}\right)^{2}\right) + \frac{1}{\sqrt{2\pi}d_{i}} exp\left(-\frac{1}{2}\left(\frac{2-k_{i}}{2d_{i}}\right)^{2}\right)$$

$$+ \frac{1}{\sqrt{2\pi}d_{i}} exp\left(-\frac{1}{2}\left(\frac{2+k_{i}}{2d_{i}}\right)^{2}\right)$$
(35)

As
$$\frac{1}{\sqrt{2\pi}d_i}exp\left(-\frac{1}{2}\left(\frac{2+k_i}{2d_i}\right)^2\right) \ll \frac{1}{\sqrt{2\pi}d_i}exp\left(-\frac{1}{2}\left(\frac{2-k_i}{2d_i}\right)^2\right)$$
, $f_i(k_i)$ can be simplified as:

$$f_i(k_i) \approx exp\left(-\frac{1}{2}\left(\frac{k_i}{2d_i}\right)^2\right) + exp\left(-\frac{1}{2}\left(\frac{2-k_i}{2d_i}\right)^2\right) \tag{36}$$

(c) $R_{f/f0}$ can be simplified as:

$$\frac{f_{i,0}(k_i)}{f_i(k_i)} \approx \frac{exp\left(-\frac{1}{2}\left(\frac{k_i}{2d_i}\right)^2\right)}{exp\left(-\frac{1}{2}\left(\frac{k_i}{2d_i}\right)^2\right) + exp\left(-\frac{1}{2}\left(\frac{2-k_i}{2d_i}\right)^2\right)} = \frac{1}{1 + exp\left(-\frac{1}{2}\left(\frac{2-k_i}{2d_i}\right)^2 + \frac{1}{2}\left(\frac{k_i}{2d_i}\right)^2\right)}$$
(37)

The constraint function becomes $-\left(\frac{2-k_i}{2d_i}\right)^2 + \left(\frac{k_i}{2d_i}\right)^2 = \frac{k_j-1}{d_j^2}$. Let the simplified $R_{f/f0}$ be R_{dd} , as:

$$R_{dd}(k_i, d_i) = \frac{k_i - 1}{d_i^2}$$
(38)

Compared to the complexity of solving and inverting the R_{basic} function, the computational complexity of solving and inverting R_{dd} was greatly reduced. Therefore, this constraint function can be called the AIAB-DD constraint function, while the original basic AIAB constraint function is called the AIAB-Basic constraint function.

5. Setting AIAB Aperture Size with Data Constraint

This section provides a detailed description of a new IAB approach aimed at avoiding the computational complexity associated with using the fixed failure rate (FF) approach.

5.1. AIAB Approach with Performance Constraint

Currently, the aperture parameter is determined using the FF approach. This approach is essentially a method of performance constraint that determines the aperture parameters based on performance requirements, such as the failure rate, and then compares the ambiguity residuals with the aperture parameters to decide whether the performance requirement can be met. The AIAB approach with the performance constraint can be performed by the Monte Carlo method or the following steps, as:

- (a) As the relationship between R_{dd} and the failure rate can be obtained from (12), (19), and (38), R_{dd} can be estimated by a dichotomy search or other methods for a given failure rate.
- (b) If R_{dd} is known, the aperture parameter can be solved by (38).

Clearly, the computational complexity of the AIAB approach with the performance constraint is extremely high due to the search of R_{dd} .

5.2. AIAB Approach with Data Constraint

Unlike the approach with the performance constraint, the AIAB approach with the data constraint determines the aperture parameter by the AIAB-DD constraint function based on the ambiguity residuals and then calculates the performance parameter, such as the failure rate, and compares the calculated performance parameter with the allocated performance parameter to determine whether the performance requirement is met. Taking the failure rate as an example of the performance parameter, the AIAB approach with the data constraint is shown in Figure 6. The failure rate was firstly computed by the simplified function (21) to reduce computational complexity, and secondly computed (if needed) by (14) to avoid the performance losses. In most cases, the failure rate only needs to be calculated once. It should be noted that the input parameter can be the missed detection rate, the false-alarm rate, etc. This is another advantage over the approach with the performance constraint.



Figure 6. The flowchart of the AIAB approach with the data constraint for a given failure rate, $P_{F,allocated}$.

It can be seen that the greatest computational complexity in AIAB lies in the possible second failure rate calculation. Further, the Simplified AIAB has been proposed by removing the second failure rate calculation in Figure 6 to meet the requirements of practical engineering applications.

In summary, AIAB can be implemented by either a performance-constraint-based class FF approach or a data-constraint-based approach. Compared to the FF-like AIAB method, the data-constrained AIAB method has a lower computational complexity. To verify this speculation, we conducted a comparison of the two computational complexities based on a MATLAB program on a Lenovo XI laptop with an i7-10510U CPU and 16 G of RAM for a total of 286 tests. The results showed that the average processing time of the data-constrained AIAB approach was 18.8 ms, and that of the performance-constrained FF-like AIAB approach was 291.3 ms. It can be seen that the running time of the data-

constrained AIAB method was significantly lower than that of the FF-like method, and it can meet the requirements of engineering applications. Of course, the FF-like performance constraint approach also has certain advantages, which can provide clear thresholds and help to comprehensively analyze the performance. The data-constrained approach can only judge whether the current data meet a single performance requirement.

6. Simulations and Discussion

Simulations were conducted to verify the performance of AIAB and compare it with that of different IAB methods in two aspects: the global CDGNSS service performance simulation and the Monte Carlo simulation based on certain epochs.

6.1. The Global CDGNSS Service Performance Simulation

6.1.1. The Simulation Strategy

To demonstrate the projected AIAB performance in general, we conducted a series of simulations to compare AIAB with existing IAB methods, i.e., Basic IAB and GIAB. A simulated GPS constellation with 24 MEO was used to simulate and implement global L1C/A-based CDGNSS in the future Ground-Based Augmentation System (GBAS) for 24 h with a sampling interval of 3600 s, and the CDGNSS positioning was implemented worldwide, uniformly, with a 15-degree interval in both longitude and latitude. A total of eight parameter configurations in Table 1 were used to simulate as many different application scenarios as possible. Since GIAB determines the aperture parameter by the failure rate, the failure rate was chosen to compare the different methods. The required integrity risk was set as 2×10^{-7} in the landing of aircraft and autonomous driving of land vehicles, and the corresponding required failure rate was allocated as 10^{-8} . Therefore, the failure rate was configured to 10^{-8} and 10^{-4} for high-integrity and middle-integrity applications, respectively. The undifferentiated observation noise of a single differential code between the base station and the rover was simulated to follow a normal distribution, with $\sigma_{\Delta\rho}$ of 0.1 m, 0.25 m, 0.5 m, and 1.0 m, respectively, so as to represent different CDGNSS models, and the undifferentiated observation noise of a single differential carrier phase at the base station and the rover was simulated to follow a normal distribution, with $\sigma_{\Delta \alpha}$ of 2 mm. The number of fixed ambiguities was set to 4 to fairly compare the different methods. Therefore, a total of 507,264 scenarios with different failure rates and model strengths were simulated to evaluate the performance of the AIAB as comprehensively as possible. When using the Monte Carlo method to validate performance, each scenario needs to be tested at least an order of magnitude higher than the inverse of the failure rate, and for a failure rate of 10^{-4} , each scenario needs to be simulated 10^5 times, which is much longer than the computational power of our simulation equipment. As mentioned in Section 5, the FF-like approach can be used for the full performance evaluation, so we adopted the FF-like approach, as described in Section 5.1, to reduce the computational effort of the simulation by determining the threshold value based on the failure rate and then calculating other parameters, such as the fix rate. It should be noted that this is only for the purpose of comparing the performance, and the data-constrained AIAB method is still recommended for real applications.

Table 1. The simulation strategy with a wide range of CDGNSS model paramet

Scheme	P_F	$\sigma_{\Delta ho}$ (m)		
A1	10^{-4}	0.1		
A2	10^{-4}	0.25		
A3	10^{-4}	0.5		
A4	10^{-4}	1.0		
A5	10^{-8}	0.1		
A6	10^{-8}	0.25		
A7	10^{-8}	0.5		
A8	10^{-8}	1.0		

6.1.2. The Comparison of Actual Failure Rates of Different Methods

The failure rate can be calculated by the GIAB failure rate function (9), the simplified function (19), and the basic function (20). Function (20) yields the true value of the failure rate, while functions (9) and (19) can only estimate its approximate upper bound value. Therefore, we can evaluate the accuracy of functions (9) and (19) by function (20).

First, it was verified that the simplified function (19) proposed in this paper can calculate an upper bound on the failure rate with the simplified AIAB aperture parameter from Scheme A1 to A8. The approximation function failure rate estimation accuracy has already been analyzed in Section 3.2 in relation to the aperture parameters and correlation coefficients. This section will focus on analyzing the estimation accuracy for different schemes. Let the simplified function be P_{FS} and the true failure rate value of the basic function be P_{F} , and the results are shown in Table 2. It can be seen that the P_F was always less than P_{FS} , implying that the failure rate of the simplified function can bound the true failure rate value and will not cause the integrity risk. Furthermore, the P_F/P_{FS} values for schemes A1, A2, A3, and A4 with a demanding failure rate of 10^{-4} were 0.91, 0.8, 0.73, and 0.66, respectively, showing that the weaker the model strength, the worse the estimation accuracy. Meanwhile, the P_F/P_{FS} values for schemes A1 and A5 were 0.91 and 0.81, respectively, showing that the lower the failure rate requirement, the better the estimation accuracy.

Scheme	Maximum (P _F /P _{FS})	Mean (P _F /P _{FS})	Minimum (P _F /P _{FS})
A1	1.00	0.91	0.27
A2	1.00	0.80	0.22
A3	1.00	0.73	0.19
A4	1.00	0.66	0.21
A5	1.00	0.81	0.07
A6	1.00	0.65	0.07
A7	1.00	0.55	0.06
A8	1.00	0.47	0.07

Table 2. The accuracy of the simplified failure rate function with different simulation schemes.

Second, the accuracy of the failure rate estimation was compared between the GIAB function (9) and the function (19) proposed in this paper. We examined the actual failure rates at various fix rates to compare the two failure rate approximation estimate functions, since the fix rate, to some extent, reflects the demanding failure rate and model strength. As shown in Figure 7, the true failure rates of the two methods did not exceed the configured failure rate, and the proposed function (19) provided a closer approximation to the true failure rate estimation significantly deteriorated at low fix rates and the performance of the IAB was mainly determined by the shape of the IAB and the failure rate, the performance of the GIAB decreased at low fix rates, as will be verified in the following.



Figure 7. The accuracy of the simplified failure rate function (PF_GIAB and PF_AIAB denote the true failure rate estimated by the GIAB function (9) and the proposed function (19), with the demanding failure rate being configured as PF).

6.1.3. The comparison of AIAB, GIAB, and the Basic IAB

Since the IAB method aims to obtain a higher fix rate with a set fixed failure rate, the fix rate was chosen as an indicator for comparing the performance of AIAB, Simplified AIAB, GIAB, and Basic IAB, as shown in Figure 8 and Table 3. The fix rates of AIAB, Simplified AIAB, GIAB, and Basic IAB are denoted as P_{A_AIAB} , P_{A_SAIAB} , P_{A_CIAB} , and P_{A_BIAB} , respectively. According to the P_{A_BIAB} , the results were divided into four categories: low, medium, high, and very high, corresponding to the range of P_{A_BIAB} equal to [0.2–0.6), [0.6–0.9), [0.9–0.95), and [0.95–1], respectively. AIAB had the highest fix rate, and Simplified AIAB was second only to AIAB. In the case of the very high fix rate, the fix rates of the four methods were almost the same and were not listed in Table 3. In the case of the high fix rate, the fix rates of GIAB and Simplified AIAB was significantly higher than that of GIAB and Basic IAB.



Figure 8. Comparison of the fix rate with Scheme A1 to A8. The points in the figure represent the epochs of the scheme, and the horizontal coordinates are the Basic IAB fix rate, \Box represents the AIAB fix rate, \bigcirc represents the simplified AIAB fix rate, and ***** represents the GIAB fix rate. (a) The comparison of fix rate with Scheme A1. (b) The comparison of fix rate with Scheme A2. (c) The comparison of fix rate with Scheme A3. (d) The comparison of fix rate with Scheme A4. (e) The comparison of fix rate with Scheme A5. (f) The comparison of fix rate with Scheme A6. (g) The comparison of fix rate with Scheme A7. (h) The comparison of fix rate with Scheme A8.

P _{A_BIAB}	Low (0.2 to 0.6)			Medium (0.6 to 0.9)		High (0.9 to 0.95)			
Scheme	$\frac{P_{A_AIAB}}{P_{A_BIAB}}$	$\frac{P_{A_SAIAB}}{P_{A_BIAB}}$	P _{A_GIAB} P _{A_BIAB}	$\frac{P_{A_AIAB}}{P_{A_BIAB}}$	$\frac{P_{A_SAIAB}}{P_{A_BIAB}}$	$\frac{P_{A_GIAB}}{P_{A_BIAB}}$	$\frac{P_{A_AIAB}}{P_{A_BIAB}}$	$\frac{P_{A_SAIAB}}{P_{A_BIAB}}$	$\frac{P_{A_GIAB}}{P_{A_BIAB}}$
A1	1.28	1.15	0.95	1.10	1.05	1.01	1.01	1.00	1.00
A2	1.29	1.12	0.88	1.10	1.03	1.00	1.01	1.00	1.00
A3	1.23	1.10	0.96	1.09	1.03	1.00	1.02	1.01	1.00
A4	1.26	1.07	0.86	1.08	1.02	1.00	1.02	1.01	1.00
A5	1.37	1.32	1.26	1.09	1.06	1.06	1.03	1.01	1.01
A6	1.38	1.24	1.15	1.12	1.06	1.04	1.03	1.01	1.01
A7	1.37	1.19	1.09	1.12	1.06	1.04	1.03	1.01	1.01
A8	1.40	1.17	1.02	1.17	1.05	1.03	1.03	1.01	1.00

Table 3. The comparison of fix rate with different simulation schemes.

The fix rate of the IAB is jointly affected by the model strength, the IAB threshold parameter relationship, and the failure rate. The model strengths of the four methods in the simulation were similar with the same simulation schemes. When the model strength was sufficient, the fix rates of the four methods were almost the same. As the model strength became weaker, the difference in fix rates between the four methods became larger due to the larger role of the other two factors in the fix rate of IAB. The failure rate was estimated by the basic function (20) in AIAB, by the proposed function (19) in Simplified AIAB and Basic IAB, and by the GIAB function (9) in GIAB. It is clear that AIAB had the highest fix rate due to its estimable, almost true failure rate and its more rational assignment of threshold parameters. Although Simplified AIAB and IAB use the same failure rate estimation function, the lower fix rate in IAB than in Simplified AIAB is due to the oversimplification of setting the threshold in IAB to the same value. GIAB virtually always beats basic IAB in fix rate, but the plots in Figure 8 and Table 3 show that GIAB was frequently worse than IAB in the case of a high fix rate. Although GIAB had a more reasonable constraint relationship for the aperture parameters than IAB, the accuracy of the failure rate calculation of GIAB by (9) was lower than that of IAB by (19), which is the main reason why GIAB will perform worse than IAB in the case of a low fix rate.

6.2. The Monte Carlo Simulation

It is well known that the state-of-the-art Optimal Integer Aperture (OIA) [16] is the theoretically best IA method, but its threshold value can only be determined accurately by Monte Carlo methods. To further demonstrate the performance of AIAB, a Monte Carlo test was implemented to compare the performance of AIAB with OIA. It has been shown in Section 6.1 that there is a difference in the effectiveness of different IA methods in the case of insufficient model strength. Therefore, the ambiguity covariance matrix, Q_a , which is [6.2900, 5.9780, 0.5440; 5.9780, 6.2920, 2.3400; 0.5440, 2.3400, 6.2880], in ambiguity success rate evaluation software, Ps-lambda [32], was chosen to be multiplied by a factor of 0.0095 so that its fix rate without IA is equal to 0.9 in order to make the model strength suitable for comparing the failure rate of AIAB with OIA at the same fix rate. As shown in Figure 9a, the failure rate of AIAB was almost the same as that of OIA. Meanwhile, the simulation epoch in Section 6.1 was randomly selected to compare the difference in failure rates between OIA and AIAB using the same methodology, and as shown in Figure 9b. The failure rate for AIAB was slightly higher than OIA by less than 20% to 40%, with the difference controlled within reasonable limits. The results show that AIAB can yield almost theoretically the best IA performance.



Figure 9. The comparison of OIA and AIAB failure rates. (a) The comparison with $Q_a = 0.0095 \times [6.29, 5.98, 0.54; 5.98, 6.29, 2.34; 0.54, 2.34, 6.29]$. (b) The comparison with the global simulation in Section 6.1.

7. Conclusions

In order to solve the problem of the ambiguity fixation error, this paper has investigated the IAB issue, which provides resolved failure rates, in the ambiguity acceptance testing problem, and proposed a new method called AIAB, aiming to provide near-optimal IA aperture parameters. Unlike existing heuristic-based methods, the AIAB method is derived based on the optimization theory of IA and provides the highest success rate at a fixed failure rate, with an easy-to-compute function of the failure rate. Another advantage of AIAB is its ability to determine whether the current failure rate meets the requirements based on real-time data, rather than determining the threshold value based on the failure rate, which is computationally complex.

The performance of AIAB was tested by global CDGNSS simulations with different model strengths. The experimental results showed that the performance of different IABs was mainly determined by the strength of the model, the accuracy of the failure rate estimation, and the relationship between the thresholds of the IAB methods. When the model was not strong enough, AIAB had a higher fixation rate than the basic IAB method of GIAB due to its ability to estimate the actual failure rate and the fact that its threshold relationship is derived from the theoretical optimum. Furthermore, the performance advantage of AIAB became more apparent as the model strength decreased.

After verifying that the AIAB method is the optimal method of all the IABs, the theoretically optimal IA method, i.e., the OIA, was used to compare with the AIAB method via Monte Carlo simulation. The results showed that for the same fix rate, the true failure rate of the AIAB method was comparable to or slightly lower than that of OIA by 20% to 40%, proving that it has a performance close to the theoretical optimum.

In summary, AIAB has been proposed to provide superior performance of ambiguity acceptance tests than existing IAB methods with low computational complexity. However, similar to other IA methods, the performance of the AIAB method heavily depends on the accuracy of the underlying model used for the GNSS data. If the underlying model for AIAB does not match the characteristics of the real data, it may result in the AIAB failure rate exceeding the allocated value or the performance of AIAB being comparable to that of other IAB methods. For example, although difference testing has been shown to outperform ratio testing, in theory [33], ratio testing is even more robust to underlying model errors and, therefore, outperforms difference testing in real experiments [34]. The AIAB method, similar to most other IA methods, is limited to theoretical analyses and simulation validation due to the need for a large amount of historical data related to the application scenario to obtain accurate underlying models for real-world data. In the future, we will conduct research to construct the underlying model using historical data and correct it by combining observation residuals. This will allow us to carry out further methodological research and validation work of AIAB using real data. Finally, the AIAB needs to be developed for calculating position domain integrity risk to improve the availability of positioning services.

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