pharmaceutics

# Supplementary Materials: A Novel Framework to Aid the Development of Design Space Across Multi-Unit Operation Pharmaceutical Processes-A Case Study of Panax Notoginseng Saponins Immediate Release Tablet 

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Methods-Properties of Input Materials, Granules and Tablets
The bulk density $\left(D_{\mathrm{b}}\right)$ and the tapped density $\left(D_{\mathrm{t}}\right)$ of materials and granules were measured in a 250 mL cylinder according to the USP 39-NF34, and each batch of samples was tested in triplicate.

The Hausner ratio ( $H R$ ) was calculated as Equation (S1).

$$
\begin{equation*}
H R=D_{\mathrm{t}} / D_{\mathrm{b}} \tag{S1}
\end{equation*}
$$

Statistical parameters of the granule size distribution including $D_{10}, D_{50}$, and $D_{90}$ were measured by the laser diffraction instrument (BT 2001; Dandong Bettersize Instrument Ltd., Dandong, People's Republic of China) three times. The width of the granule size distribution (ie, span) was calculated by Equation (S2).

$$
\begin{equation*}
\text { Span }=\left(D_{90}-D_{10}\right) / D_{50} \tag{S2}
\end{equation*}
$$

The angle of repose $(A O R)$ of materials and granules was measured with the powder flow ability tester (Copley BEP2; Copley Scientific Limited, Nottingham, UK). Samples were poured through a vibrating metal funnel onto a platform until a stable and height-fixed heap was formed. The AOR was measured as the angle made by the inclined plane of the heap with the horizontal. Each batch of the sample was tested in triplicate.

The specific surface area (SSA) of materials was measured by applying a 3H-2000 PS1 specific surface \& pore size analysis instrument (Beishide Instrument Technology Co. Ltd., Beijing, R.P China). Samples were weighed and were then poured into the sample tubes with filler rods. Before measurement, samples were degassed at $120^{\circ} \mathrm{C}$ for 2.5 h to keep the surface of samples clean enough. Partial pressure points for nitrogen at 77 K were set between 0.05 and 0.3 Bar, split equally into 6 points and the equilibration time was 10 s . The SAA of materials was determined based on the Brunauer-Emmett-Teller adsorption isotherm analysis.

The moisture content (MC) of granule was tested using the Sartorius MA35 instrument (Sartorius AG, Goettingen, Germany). The sample was placed on the pan and heated to $105{ }^{\circ} \mathrm{C}$. The percentage of moisture content was recorded until the weight was constant. Each batch of samples was tested in triplicate.

The hardness of the tablet was evaluated with the HC 97 instrument (Kraemer Elektronik GmbH, Darmstadt, Germany). The tablet diameter and thickness were measured by the digimatic indicator (ID-C112X/1012X; Mitutoyo Corporation, Kawasaki, Japan). With these obtained data, the tensile strength $(T S)$ of tablets was calculated according to the equation described by Fell and Newton.

$$
\begin{equation*}
T S=2 F / \pi d t \tag{S3}
\end{equation*}
$$

where $F$ refers to the hardness of tablets ( N ), $d$ refers to tablet diameter ( mm ), and $t$ refers to tablet thickness (mm). Each batch of samples was tested 10 times.

The disintegration time was tested according to the USP 39-NF34, and each batch of samples was tested in six times.

The results of properties of input materials, granules and tablets were showed in Table S1 and Table S2.

Table S1. The properties of different batches of PNS materials.

| Lots | $\begin{aligned} & D_{10 \mathrm{~m}} \\ & (\mu \mathrm{~m}) \end{aligned}$ | $\begin{aligned} & D_{50 \mathrm{~m}} \\ & (\mu \mathrm{~m}) \end{aligned}$ | $\begin{aligned} & D_{90 \mathrm{~m}} \\ & (\mu \mathrm{~m}) \end{aligned}$ | Spanm | $S S A\left(\mathrm{~m}^{2} \cdot \mathrm{~g}^{-1}\right)$ | $\begin{gathered} D_{\mathrm{bm}} \\ \left(\mathrm{~g} \cdot \mathrm{~mL}^{-1}\right) \end{gathered}$ | $\begin{gathered} D_{\mathrm{tm}} \\ \left(\mathrm{~g} \cdot \mathrm{~mL}^{-1}\right) \end{gathered}$ | $\overline{A O R_{m}}$ <br> ( ${ }^{\circ}$ ) | HR m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ZL1208 | 3.067 | 20.02 | 83.10 | 3.996 | 0.9152 | 0.477 | 0.744 | 47.3 | 1.56 |
| ZL0120 | 3.829 | 26.51 | 95.51 | 3.457 | 0.6896 | 0.488 | 0.729 | 45.8 | 1.49 |
| ZL0518 | 4.193 | 30.14 | 115.3 | 3.688 | 0.6891 | 0.507 | 0.755 | 45.2 | 1.49 |
| ZL0524 | 3.922 | 28.61 | 102.5 | 3.446 | 0.6368 | 0.511 | 0.751 | 45.5 | 1.47 |
| BCTG | 3.792 | 37.75 | 133.6 | 3.438 | 0.6209 | 0.572 | 0.813 | 48.6 | 1.42 |
| YNSS | 3.448 | 30.03 | 112.1 | 3.619 | 0.9789 | 0.524 | 0.778 | 44.9 | 1.48 |
| SXAS | 2.107 | 8.518 | 23.72 | 2.536 | 1.512 | 0.387 | 0.587 | 51.0 | 1.52 |
| XAHX | 2.927 | 19.85 | 84.82 | 4.125 | 0.9495 | 0.476 | 0.728 | 50.4 | 1.53 |
| WHYC | 3.027 | 18.86 | 76.92 | 3.916 | 0.7675 | 0.318 | 0.506 | 44.7 | 1.59 |
| YNZW | 2.730 | 12.74 | 47.59 | 3.523 | 0.8795 | 0.411 | 0.613 | 44.7 | 1.49 |
| YNYK | 3.447 | 24.33 | 96.34 | 3.819 | 0.7176 | 0.488 | 0.752 | 45.7 | 1.54 |

Table S2. The properties of different batches of granules and tablets.

| Runs | Granule |  |  |  |  |  |  |  |  | Tablet |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} D_{\mathrm{b}} \\ \left(\mathrm{~g} \cdot \mathrm{~mL}^{-1}\right) \end{gathered}$ | $\begin{gathered} D_{\mathrm{t}} \\ \left(\mathrm{~g} \cdot \mathrm{~mL}^{-1}\right) \end{gathered}$ | $\begin{aligned} & \hline M C \\ & (\%) \end{aligned}$ | AOR <br> $\left({ }^{\circ}\right)$ | HR | $\begin{gathered} D_{10} \\ (\mu \mathrm{~m}) \end{gathered}$ | $\begin{gathered} D_{50} \\ (\mu \mathrm{~m}) \end{gathered}$ | $\begin{gathered} D_{90} \\ (\mu \mathrm{~m}) \end{gathered}$ | Span | $\begin{gathered} \hline T S \\ \text { (Мра) } \end{gathered}$ | $\begin{gathered} D T \\ (\mathrm{~min}) \end{gathered}$ |
| 1 | 1.06 | 32.4 | 0.410 | 0.491 | 1.20 | 38.50 | 120.9 | 249.2 | 1.743 | 3.83 | 2.25 |
| 2 | 1.70 | 34.0 | 0.389 | 0.474 | 1.19 | 40.82 | 128.7 | 275.8 | 1.827 | 5.08 | 6.01 |
| 3 | 1.86 | 34.7 | 0.383 | 0.464 | 1.21 | 16.97 | 66.82 | 164.2 | 2.200 | 6.73 | 5.33 |
| 4 | 1.93 | 33.0 | 0.479 | 0.547 | 1.14 | 69.18 | 170.5 | 346.5 | 1.627 | 3.67 | 4.87 |
| 5 | 1.34 | 33.5 | 0.436 | 0.527 | 1.21 | 61.40 | 141.9 | 287.8 | 1.596 | 3.92 | 6.93 |
| 6 | 1.50 | 32.0 | 0.410 | 0.475 | 1.16 | 36.85 | 115.6 | 236.8 | 1.729 | 4.88 | 3.17 |
| 7 | 1.26 | 32.0 | 0.399 | 0.479 | 1.20 | 36.23 | 109.5 | 219.3 | 1.672 | 4.98 | 3.53 |
| 8 | 1.22 | 33.0 | 0.450 | 0.541 | 1.20 | 54.60 | 140.5 | 298.4 | 1.735 | 3.87 | 3.34 |
| 9 | 1.11 | 32.0 | 0.473 | 0.578 | 1.22 | 66.17 | 145.3 | 294.8 | 1.574 | 1.73 | 6.01 |
| 10 | 1.55 | 33.0 | 0.486 | 0.583 | 1.20 | 60.01 | 141.4 | 296.9 | 1.675 | 2.45 | 7.41 |
| 11 | 1.49 | 33.7 | 0.436 | 0.507 | 1.16 | 56.95 | 228.0 | 552.4 | 2.174 | 3.38 | 4.14 |
| 12 | 1.21 | 31.6 | 0.467 | 0.569 | 1.22 | 59.50 | 146.8 | 311.2 | 1.715 | 3.14 | 3.51 |
| 13 | 1.74 | 33.4 | 0.412 | 0.509 | 1.24 | 29.94 | 98.79 | 210.8 | 1.830 | 4.26 | 2.44 |
| 14 | 1.75 | 32.9 | 0.456 | 0.540 | 1.19 | 73.58 | 196.1 | 487.4 | 2.110 | 3.96 | 5.41 |
| 15 | 1.83 | 33.5 | 0.414 | 0.496 | 1.20 | 44.00 | 171.8 | 460.9 | 2.430 | 5.74 | 5.25 |
| 16 | 1.92 | 33.2 | 0.491 | 0.561 | 1.14 | 48.91 | 197.4 | 493.6 | 2.253 | 1.94 | 3.81 |
| 17 | 1.68 | 33.5 | 0.491 | 0.550 | 1.12 | 61.80 | 222.6 | 538.5 | 2.14 | 2.73 | 7.42 |
| 18 | 1.87 | 34.3 | 0.409 | 0.467 | 1.14 | 44.19 | 135.1 | 304.4 | 1.927 | 4.98 | 3.94 |
| 19 | 1.61 | 32.7 | 0.431 | 0.535 | 1.24 | 72.75 | 236.2 | 549.9 | 2.042 | 3.68 | 4.51 |
| 20 | 1.07 | 33.3 | 0.453 | 0.557 | 1.23 | 56.69 | 141.7 | 310.6 | 1.792 | 2.85 | 6.54 |
| 21 | 1.76 | 33.5 | 0.451 | 0.531 | 1.18 | 57.83 | 141.6 | 299.4 | 1.706 | 2.81 | 3.67 |
| 22 | 2.04 | 32.6 | 0.472 | 0.540 | 1.14 | 62.24 | 155.3 | 336.9 | 1.77 | 3.45 | 4.80 |
| 23 | 1.76 | 32.2 | 0.445 | 0.511 | 1.15 | 46.24 | 134.8 | 292.9 | 1.830 | 4.57 | 3.00 |
| 24 | 1.64 | 33.4 | 0.445 | 0.507 | 1.14 | 53.03 | 145.6 | 315.7 | 1.804 | 5.04 | 5.39 |
| 25 | 1.87 | 34.2 | 0.419 | 0.509 | 1.22 | 22.03 | 81.97 | 210.4 | 2.302 | 4.26 | 3.97 |
| 26 | 1.55 | 33.3 | 0.447 | 0.549 | 1.23 | 58.40 | 144.3 | 315.6 | 1.782 | 1.98 | 3.39 |
| 27 | 1.48 | 34.1 | 0.455 | 0.540 | 1.19 | 67.14 | 155.0 | 322.7 | 1.649 | 3.99 | 5.68 |
| 28 | 1.97 | 33.1 | 0.443 | 0.523 | 1.18 | 52.41 | 142.4 | 309.6 | 1.806 | 4.07 | 2.90 |
| 29 | 1.80 | 33.9 | 0.464 | 0.526 | 1.13 | 53.16 | 143.0 | 310.9 | 1.802 | 4.78 | 4.13 |
| 30 | 1.85 | 33.1 | 0.452 | 0.544 | 1.20 | 57.48 | 142.7 | 301.7 | 1.712 | 3.64 | 4.82 |
| 31 | 1.77 | 33.7 | 0.461 | 0.570 | 1.24 | 68.6 | 155.9 | 322.8 | 1.631 | 2.11 | 4.26 |
| 32 | 1.88 | 33.8 | 0.436 | 0.543 | 1.25 | 59.78 | 147.3 | 311.9 | 1.712 | 4.22 | 5.87 |
| 33 | 1.75 | 33.2 | 0.442 | 0.515 | 1.16 | 31.99 | 108.1 | 238.1 | 1.906 | 4.14 | 3.47 |
| 34 | 1.71 | 32.2 | 0.487 | 0.558 | 1.15 | 73.59 | 167.0 | 339.4 | 1.592 | 2.94 | 5.81 |
| 35 | 1.29 | 34.3 | 0.436 | 0.522 | 1.20 | 55.02 | 138.1 | 294.6 | 1.735 | 3.56 | 3.40 |
| 36 | 1.47 | 33.6 | 0.427 | 0.535 | 1.25 | 58.44 | 145.3 | 307.8 | 1.716 | 3.09 | 3.20 |
| 37 | 1.87 | 34.3 | 0.440 | 0.501 | 1.14 | 65.49 | 171.5 | 400.7 | 1.953 | 5.50 | 6.20 |
| 38 | 1.63 | 33.8 | 0.392 | 0.487 | 1.24 | 47.48 | 133.0 | 291.2 | 1.833 | 4.73 | 3.03 |
| 39 | 1.63 | 32.1 | 0.428 | 0.502 | 1.17 | 48.39 | 138.0 | 306.8 | 1.872 | 4.37 | 3.11 |
| 40 | 1.86 | 33.1 | 0.425 | 0.496 | 1.17 | 42.33 | 129.2 | 289.2 | 1.910 | 3.93 | 2.11 |
| 41 | 1.67 | 34.1 | 0.408 | 0.484 | 1.19 | 35.93 | 113.6 | 254.4 | 1.922 | 5.48 | 3.78 |
| 42 | 1.64 | 33.1 | 0.406 | 0.506 | 1.25 | 46.91 | 125.9 | 274.9 | 1.811 | 5.18 | 3.71 |
| 43 | 1.52 | 34.4 | 0.447 | 0.531 | 1.19 | 65.02 | 160.1 | 333.1 | 1.674 | 3.60 | 5.37 |
| 44 | 2.10 | 34.0 | 0.416 | 0.480 | 1.15 | 38.43 | 117.4 | 264.3 | 1.924 | 5.22 | 2.40 |
| 45 | 1.49 | 33.1 | 0.441 | 0.529 | 1.20 | 54.73 | 147.3 | 319.2 | 1.796 | 3.78 | 2.78 |
| 46 | 1.27 | 33.0 | 0.442 | 0.539 | 1.22 | 54.84 | 148.4 | 319.8 | 1.786 | 4.67 | 3.52 |
| 47 | 1.70 | 33.2 | 0.477 | 0.554 | 1.16 | 64.85 | 163.7 | 335.8 | 1.655 | 2.96 | 4.62 |
| 48 | 1.55 | 34.1 | 0.442 | 0.533 | 1.21 | 69.01 | 153.3 | 314.4 | 1.601 | 3.12 | 4.65 |
| 49 | 1.54 | 33.1 | 0.430 | 0.504 | 1.17 | 41.10 | 134.0 | 310.0 | 2.077 | 6.07 | 7.06 |
| 50 | 1.22 | 33.5 | 0.456 | 0.538 | 1.18 | 61.51 | 150.1 | 316.0 | 1.695 | 3.28 | 7.66 |
| 51 | 1.65 | 32.4 | 0.469 | 0.535 | 1.14 | 74.40 | 211.4 | 516.4 | 2.094 | 4.09 | 7.77 |
| 52 | 1.64 | 34.1 | 0.394 | 0.466 | 1.18 | 35.90 | 122.1 | 291.3 | 2.092 | 3.90 | 2.76 |

