



Article Economy Mode Setting Device for Wind-Diesel Power Plants

Andrey Dar'enkov, Elena Sosnina *, Andrey Shalukho and Ivan Lipuzhin

Department of Electric Power Engineering, Power Supply and Power Electronics, Nizhny Novgorod State Technical University n.a. R.E. Alekseev, 603950 Nizhny Novgorod, Russia; darenkov@nntu.ru (A.D.); shaluho@nntu.ru (A.S.); lipuzhin@nntu.ru (I.L.)

* Correspondence: sosnyna@yandex.ru

Received: 20 December 2019; Accepted: 5 March 2020; Published: 10 March 2020



Abstract: The article is devoted to the problem of reducing fuel consumption in a diesel generator set (DGS) as a part of a wind-diesel power plant (WDPP). The object of the research is a variable speed DGS. The goal is to develop the WDPP intelligent control system, providing an optimal shaft speed of an internal combustion engine (ICE). The basis of the intelligent control system is an economy mode setting device (EMSD), which controls the fuel supply to the ICE. The functional chart of EMSD has been presented. The main EMSD blocks contain a controller and an associative memory block. The associative memory block is a software model of an artificial neural network that determines the optimal shaft speed of the ICE. An algorithm for the WDPP intelligent control system has been developed and tested using the WDPP Simulink model. The EMSD prototype has been created, and its research has been conducted. Dependences of the change in specific and absolute fuel consumption on the load power have been obtained for two 4 kW DGS: with constant rotation speed and variable rotation speed DGS with EMSD. It has been established that the use of EMSD in the mode of low loads allow one to reduce fuel consumption by almost 30%. The error in determining the optimal engine speed using EMSD prototype is not more than 15%.

Keywords: wind-diesel power plant; intelligent control system; diesel-generator set; internal combustion engine; artificial neural network; fuel economy

1. Introduction

Wind-diesel power plants (WDPP) are widely used for power autonomous consumers all round the world [1]. The main components of the WDPP are a wind turbine and a diesel generator set (DGS). DGS provides guaranteed power supply to consumers, and the wind turbine can reduce fuel consumption and harmful emissions into the environment [2]. However, commercially available WDPP have certain disadvantages like an excessive diesel fuel consumption during DGS operation, low efficiency, an incomplete use of a wind turbine at low wind speeds [3].

The studies aimed at solving these problems can be divided into two main groups:

- Optimization of the WDPP structure
- Controlling WDPP operating modes and ensuring its stability

The first group includes studies devoted to determining an optimal quantity and capacity of the power units in the system of the WDPP. The article [4] proposes a specific methodology for substantiating the parameters, placing and evaluating the WDPP effectiveness based on a multi-level system assessment of the resource potential and climate information. The article [5] considers the influence of the share of the wind turbine generator capacity in the installed capacity in the WDPP and the composition of consumers on the amount of replacement of the DGS energy output. The article [6]

presents an optimal day-ahead scheduling of the WDPP and considers the role of battery storage system in frequency response. The optimal sizing of the PV/Wind/Diesel/Battery storage stand-alone hybrid system has been presented in the article [7] to minimize the cost of energy supplied by the system while increasing the reliability and efficiency of the system presented by the loss of power supply probability. The article [8] proposes a two-stage stochastic optimization framework to determine an optimal size of energy storage devices in a WDPP. The article [9] introduces an optimization method that takes economic and technical indexes into account. The method optimizes the capacity of the battery and DGS under the premise of satisfying the technical indexes, and it also increases the capacity of the wind turbine and photovoltaic array by considering the economic index.

The second group includes studies on improving the WDPP efficiency. The articles [10,11] proposed an additional adaptive voltage compensation controller for static var compensator by using a double sliding-mode optimal strategy to maintain the system bus voltage stability. In the article [12], a composite control strategy has been investigated for a photovoltaic, wind turbine, and DGS-based off-grid power generation system to achieve high performance while supplying unbalanced nonlinear loads. The article [13] introduces a frequency regulation scheme to share the active power, not supplied by the wind power, among DGS with the aim of reducing the total fuel consumption of the DGS. The article [14] presents a wind energy conversion system with a diesel generator. The proposed system regulates the loading of diesel generator to achieve low-specific fuel consumption.

The use of DGS with the variable shaft speed as a part of the WDPP is the most effective solution [15]. As a rule, a change in the shaft speed depending on the load power is stepwise. This allows one to reduce specific fuel consumption by up to 20%. However, fuel economy can be increased by a smooth regulation of the speed based on the multi-parameter characteristic of the internal combustion engine (ICE) as a part of the DGS.

The multi-parameter characteristic is individual for each ICE; it has a nonlinear character and shows the dependence of specific fuel consumption on the shaft speed and pressure on the ICE piston. The multi-parameter characteristic varies depending on the external and internal ICE operating conditions. External working conditions for ICE are temperature, pressure, and humidity of ambient air, etc. Internal conditions are the brand and quality of fuel and the wear of ICE internal parts, etc. WDPP manufacturers do not provide information on such characteristics, as a rule. It is impossible to calculate a multi-parameter characteristic; it can only be obtained experimentally. There are no developments allowing an optimal selection of the ICE speed in the absence of a multi-parameter characteristic.

The aim of the research is the development of an intelligent control system for WDPP, which provides effective operating modes under changing external and internal working conditions.

The economy mode setting device (EMSD) has been proposed to be used as the basis of the intelligent control system. EMSD automatically calculates the value of the optimal speed of the ICE for the current value of the load power under changing external and internal conditions.

Section 2 describes EMSD. Section 3 presents an algorithm of the intelligent control system. Section 4 is devoted to simulation. Section 5 describes the EMSD prototype. Section 6 is devoted to the experimental research and discussion.

2. Economy Mode Setting Device (EMCD)

A functional chart of EMSD is presented in Figure 1.



Figure 1. Functional chart of economy mode setting device (EMSD): (1) learning controller, (2) management controller, (3) associative memory block, (4) data memory block, (5) information bus, (P_{ω}) DGS power, (g_e) ICE fuel consumption, and (ω) ICE shaft speed.

EMSD is an adaptive controller that uses the principle of artificial neural networks. EMSD consists of four main elements: a management controller, a learning controller, an associative memory block, and nonvolatile memory. A common information bus, providing bi-directional exchange of information and expansion of the system in the case of controlling multiple ICEs, combines the elements.

EMSD optimizes the speed of the engine shaft by controlling the ICE fuel supply depending on the internal and external working conditions. The control signal is generated using the associative memory block, which is a software model of an artificial neural network. The optimal ICE shaft rotation speed is determined in real time. The principle of EMSD operation is as follows.

The sensors record the following parameters: DGS power (*P*), ICE fuel consumption (g_e), and ICE shaft speed (ω). These parameters are transferred to the learning controller, where they are compared with similar parameters available in the data memory block.

If the parameters of the current mode match to the parameters of one of the modes stored in the data memory block, the learning controller reads information about the position of the fuel pump rail (value *h*) and transmits it to the management controller. The management controller forms a control signal in the ICE fuel supply system. As a result, the fuel pump rail moves in the right direction by the required number of steps.

If the input data of the learning controller does not match to any mode stored in the data memory block, then the learning controller performs several learning cycles of the memory block. After training, a new optimal position of the fuel pump rail is formed, which is transmitted to the management controller. Additionally, parameters of a new mode are formed from the input (P, g_{e} , and ω) and output (h) parameters, which are stored in the data memory block.

A block scheme of the neural network of the EMSD associative memory block is presented in Figure 2.

The neural network of the associative memory block consists of three layers: input, hidden, and output. The input layer distributes the input data. The hidden layer consists of two neurons whose activation function is hyperbolic tangent. The signals of the neurons of the hidden layer are displayed linearly in the output layer. The output layer sums up the signals of the hidden layer and normalizes them. Neural network learning is implemented according to the algorithm of back error propagation, and it is realized by the learning controller.



Figure 2. The block scheme of the associative memory block: (P_{load}) load power vector, (K_{norm}) normalization coefficient required to bring the load power value to the unit basis of the neural network, (x_{ij}) input *i* of the neuron (*j*) of the layer *n*, (W_{ij}) weight ratio of the corresponding neuron input, (B_i) weight of additional input for the *i*-th neuron initialization, (Y_{ij}) output *i* of the neuron (*j*-1) of the layer *n*, (S_{ij}) calculated function on the *j*-th layer of neurons, and (ω_{opt}) optimal value of the rotation speed at the output of the learning controller.

At the beginning of learning process, the load power vector P_{load} is applied to the inputs of the first layer of the network. At the outputs of the first layer, the following values are calculated:

$$x_{i1} = P_{\text{load}} \cdot K_{\text{norm}}; \tag{1}$$

$$x_{i2} = \text{th}(x_{i1} \cdot W_{i1} + B_i);$$
(2)

$$s_j^{(n)} = \sum_{i=0}^{M} y_i^{(n-1)} \cdot W_{ij}^{(n)};$$
(3)

$$y_j^{(n)} = \operatorname{th}\left(s_j^{(n)}\right), \, \omega_q \equiv P_q, \tag{4}$$

where

 x_{ii}^{n} is the input *i* of the neuron (*j*) of the layer *n*;

 $W_{ii}^{(n)}$ is the weight ratio of the corresponding neuron input;

 K_{norm} is the normalization coefficient required to bring the load power value to the unit basis of the neural network;

B_i is the weight of additional input for the *i*-th neuron initialization;

M is the number of neurons in the layer *n*;

 $y_{i(j-1)}^{n}$ is the output *i* of the neuron (j - 1) of the layer *n*;

 P_q is the component q of the input vector P; and

 ω_q is the component *q* of the output speed array ω .

For the output layer and the hidden layer *n*, the error value (δ) and the weight change (ΔW_{ij}) are calculated:

$$\delta_j^{(n)} = \left(y_j^{(n)} - d_j \right) \frac{\partial y_j}{\partial s_j}; \tag{5}$$

$$\Delta W_{ij}^{(n)} = -\beta \cdot \delta_j^{(n)} y_i^{(n-1)},\tag{6}$$

where d_i is an ideal (desired) state of the neuron and β is the learning coefficient.

Next, the values of the network link weights are corrected:

$$W_{ij}^{(n)}(t) = W_{ij}^{(n-1)}(t-1) + \Delta W_{ij}^{(n)}(t),$$
(7)

where *t* is the number of the learning era of the associative memory block.

The value of the optimal rotation speed (ω_{opt}) is determined in the output:

$$\omega_{\text{opt}} = \left(\sum_{i=1}^{n} W_{i2} x_{i2} + B_i\right) \cdot 1/K_{\text{norm}},\tag{8}$$

where x_{i1} and x_{i2} are the inputs of the *i*-th neurons of layers 1 and 2 of the neural network, respectively, and K_{norm} is the normalization coefficient needed to reduce the load power value *P* to the unit basis of the neural network.

The calculation continues until the network operation error (E_{ω}) becomes less than permissible. Network operation error is determined by:

$$E_{\omega} = \frac{1}{2} \sum_{t=1}^{p} \left(\omega_t - \omega_{\text{opt}} \right)^2, \tag{9}$$

where

 ω_t is an actual value of the rotation speed at the output of the neural network at the era *t*; ω_{opt} is an optimal value of the rotation speed at the output of the learning controller; and *p* is the number of the learning era corresponding to the permissible error.

A necessary condition for the correct learning of the neural network is the presence of a learning set; that is, a set of logical pairs $\omega_{opt} = f(P)$. A table array of speed values $\omega_{opt} = f(P)$ for discrete values of power *P* is stored in a data memory block.

3. Algorithm of the WDPP Intelligent Control System

The WDPP intelligent control system consists of four modules:

- A network learning management module
- A module for determining the minimum fuel consumption of ICE
- A control module for the optimal position of the ICE fuel pump rail
- A module for managing associative memory and data memory of the neural network

A block-chart of the algorithm of the WDPP intelligent control system is shown in Figure 3.



Figure 3. The algorithm block-chart of the wind-diesel power plant (WDPP) intelligent control system.

The input data of the algorithm are an actual value of the DGS power (P_{DGS}), an ICE fuel consumption (g_e), a rotational speed of the ICE shaft (ω_{ICE}), and an actual value of the output power of the wind generator (P_w).

The management controller monitors change in the value of the load power during the WDPP operation. If the load power changes by more than a predetermined value P_{step} , then a new value P_{new} is fixed. Further, the management controller determines that the new power value belongs to the range of values stored in the associative memory block.

Based on the artificial neural network of the associative memory block, the optimal value of the ICE speed is determined. In accordance with the optimal value of the ICE speed, a control signal for the fuel pump rail h is generated. This provides an efficient mode of WDPP operation.

The developed algorithm significantly expands the limits of the efficient operation of the WDPP and makes the intelligent control system adaptive towards to the external and internal operating conditions of the ICE.

4. Simulation

A Simulink model of the WDPP has been created to test the developed algorithm. The Simulink model allows one to study the static and dynamic modes of WDPP taking into account the mutual influence of WDPP units on each other.

The model is built on the basis of differential equations describing the functioning of the main units of the WDPP:

- A wind turbine, consisting of a turbine and a synchronous generator
- DGS, consisting of a diesel engine and a synchronous generator
- Energy storage systems
- Three-phase active-inductive load

The block scheme of the Simulink model is in Figure 4.



Figure 4. The block-scheme of the WDPP Simulink model. DGS: diesel generator set.

Mathematical models have been developed to simulate the operation of each WDPP unit. The models are differential equations that describe the processes of change of physical quantities such as current, voltage, frequency, torque, etc.

So, the operation of a synchronous generator as part of a wind turbine and DGS is described by a system of equations based on the law of electromagnetic induction and Ohm's law [16]:

$$U_{abc} = \frac{d}{dt} \Psi_{abc} + R_{abc} I_{abc} + H_s U_x,$$

$$\frac{d}{dt} \psi_f = e_f - r_f i_f,$$
(10)

where

 U_{abc} is the stator voltage vector;

 Ψ_{abc} is the stator flux distribution vector;

 R_{abc} is the stator windings resistance vector;

 I_{abc} is the stator current vector;

 H_s is the matrix of independent circuits [17];

 U_x is the vector of the voltage across stator clamps;

 ψ_f is the excitation winding flux distribution; e_f is the electromotive force of the excitation winding; r_f is the resistance of the excitation winding; and i_f is the current of the excitation winding.

Differential equations allow one to determine the phase currents and voltages for static and dynamic modes of operation based on the initial parameters for a specific model of a synchronous generator. The detailed descriptions of the mathematical models of WDPP units and their study results are given in [16].

A system of matrix differential equations has been developed to study WDPP operation modes, taking into account the mutual influence of WDPP units on each other:

$$|\frac{a}{dt}Y_D = V_D(Y_D, Y_G),$$

$$|\frac{d}{dt}Y_G = V_G(Y_D, Y_G, Y_W, Y_E),$$

$$|\frac{d}{dt}Y_W = V_W(Y_G, Y_W, Y_E),$$

$$|\frac{d}{dt}Y_E = V_E(Y_G, Y_W, Y_E).$$
(11)

Vectors Y with corresponding indices represent variable values describing the operation of the diesel engine (D), the synchronous generator (G), the wind turbine (W), and the load (E). Vectors Y are determined for each WDPP unit with appropriate mathematical models. So, the variables for the synchronous generator are the stator voltage and current vectors, which are determined by Equations (10). The variables for the diesel engine are the engine speed and the position of the fuel pump rail. The variables for the wind turbine are wind turbine power and torque.

All equations have been compiled in relative units that facilitate their joint integration. The basic values correspond to the nominal passport data of the elements [16].

The algorithm of the WDPP intelligent control system for WDPP consisting of a 4 kW wind turbine and a 4 kW diesel generator has been tested on the Simulink model. Modeling was carried out for relative values of the load power in the range from 0.00 to 1.00 in increments of 0.05. Figure 5 shows the obtained dependence of the ICE rotation speed on the load power *P*.



Figure 5. The dependence of the internal combustion engine (ICE) rotation speed on the load power obtained with the Simulink model: (*P*) load power, (ω_{opt}) optimal value of the ICE speed.

Dots indicate discrete values calculated by using the learning controller. The solid line shows a continuous dependence $\omega_{opt} = f(P)$ obtained with the associative memory block. The difference between the values ω_{opt} , calculated with the associative memory block and the discrete values determined by the learning controller for the corresponding *P* values, does not exceed 0.03% of the nominal value of the ICE speed.

The research has shown that the developed algorithm of the WDPP intelligent control system provides a minimum error in determining the optimal ICE shaft speed.

5. Economy Mode Setting Device (EMSD) Prototype

An EMSD prototype has been developed. In addition to the learning and management controller, associative and data memory blocks (for generating a control signal), the prototype includes a block of parameters from measuring sensors (for obtaining initial data) and a stepper motor control unit (for changing the position of the fuel pump rail).

The appearance of the prototype is shown in Figure 6.



Figure 6. EMSD prototype: (1) programmable control unit, (2) linear stepper motor, and (3) learning and management controller.

Learning and management controllers are combined in one device (3), which is based on the TM4C123GH6 microcontroller. Its memory capacity is 256 kB, which makes it possible to store the control algorithm, process sensor signals, and also store intermediate data during the functioning of the neural network. To control the position of the fuel pump rail, a linear stepper motor (2) is used, which is connected to a programmable control unit (1). The control unit generates control pulses with a frequency of up to 10 kHz and an accuracy of 0.2%.

6. Experimental Studies and Discussion

The appearance of the test bench is shown in Figure 7. The test bench consists of the following parts: (1 and 2) DGS and wind turbine simulators based on an asynchronous variable frequency drive and an alternator, (3) a DGS based on a gasoline ICE and synchronous generator, (4) connecting terminals for connecting a wind turbine, (5) an accumulator battery, (6) a programmable logic controller, (7) an autonomous inverter, (8) measuring equipment, (9) learning and management controller, and (10) programmable control unit.



Figure 7. The test bench. (1 and 2) DGS and wind turbine simulators based on an asynchronous variable frequency drive and an alternator, (3) a DGS based on a gasoline ICE and synchronous generator, (4) connecting terminals for connecting a wind turbine, (5) an accumulator battery, (6) a programmable logic controller, (7) an autonomous inverter, (8) measuring equipment, (9) learning and management controller, and (10) programmable control unit.

Technical parameters of the test bench are shown in Table 1.

Table 1. Technical parameters of the test bench. DGS: diesel gener	ator set
--	----------

Parameter	Value	Units
Wind turbine rated power	4	kW
DGS-rated power	4	kW
Wind speed	changes from 0 to 10	m/s
Active load	changes from 0 to 8 with step 0,1	kW

The programmable logic controller (6) provides an overall control of the test bench. EMSD prototype is designed to control the operation of DGS simulator (1) and DGS with the gasoline ICE (3).

The EMSD prototype is connected to the frequency converter as part of the DGS simulator. Therefore, it is able to adjust the DGS speed. DGS simulator (1) and wind turbine simulator (2) are used for testing and tuning the software of the WDPP intelligent control system.

The main purpose of the EMSD prototype is to control the DGS based on a gasoline ICE and synchronous generator (3). The learning and management controller (9) as part of EMSD prototype receives information from the sensors about the DGS power, the ICE fuel consumption, and the rotation speed of the ICE shaft and determines the optimal value of the ICE speed according to the algorithm (Figure 3). Information is transmitted to a programmable control unit (10), which forms a control signal for a linear stepper motor. The linear stepper motor changes the position of the ICE fuel pump rail according to the optimal engine speed. The placement of the learning and management controller, the programmable control unit, and the linear stepper motor as the part of the EMSD prototype is shown in Figure 8.



Figure 8. Placement of the EMSD prototype blocks on the test bench: (1) learning and management controller, (2) programmable control unit of the stepper motor, (3) ICE, (4) linear stepper motor, and (5) rail of the ICE fuel pump.

Figure 8 shows: (1) the learning and management controller, (2) programmable control unit of the stepper motor, (3) ICE, (4) linear stepper motor, and (5) rail of the ICE fuel pump.

A test bench has been used to study the parameters of the WDPP operation modes with EMSD. Figure 9 shows the dependences of the specific g_e (Figure 9a) and absolute g (Figure 9b) fuel consumption of 4 kW DGS with variable rotation speed. The results were obtained by calculation (using the multi-parameter characteristics of the ICE) and experimentally (using the EMSD prototype).



Figure 9. Dependence of specific (**a**) and absolute (**b**) fuel consumption for DGS with variable rotation speed: (*P*) load power, (g_e) specific fuel consumption, (g) absolute fuel consumption.

In Figure 9, the blue lines show the calculated characteristics, and the red lines show the experimental characteristics. The obtained results show that the error in determining the optimal engine speed using EMSD prototype is not more than 15%.

Figure 10 shows that the dependences of changes in specific (Figure 10a) and absolute (Figure 10b) fuel consumptions on the load power have been studied for two types of 4 kW DGS: with a constant (blue lines) and variable speed when using EMSD (red lines).



Figure 10. Dependence of specific (**a**) and absolute (**b**) fuel consumption for DGS with constant rotation speed (blue lines) and DGS with variable rotation speed with EMSD (red lines): (*P*) load power, (g_e) specific fuel consumption, (g) absolute fuel consumption.

In the figures, one can see that the greatest difference in the fuel consumption corresponds to the mode of low loads. The difference in the fuel consumption is decreasing with an increase in the load power (Figure 10). The fuel economy takes place due to the regulation of the engine rotation using EMSD and is the greatest with a load power of 1 kW and amounts to almost 30%.

Also, the research results have shown that the intelligent management system based on EMSD provides:

- A stabilization of the current value of the output voltage when changing wind speed and load power
- A total harmonic distortion of the output voltage that does not exceed 5%

7. Conclusions

The article is devoted to solving the problem of the low efficiency of WDPPs.

An WDPP intelligent control system has been developed, which provides effective operating modes when changing external and internal conditions. It has been proposed to use the EMSD as the basis of the intelligent control system. The key block of EMSD is an associative memory block, which is a software model of an artificial neural network. Using this unit, the optimal ICE speed for the current load power value is automatically determined. The proposed approach allows one to expand the limits of WDPP effective operation.

The algorithm of the intelligent control system has been tested on the WDPP Simulink model. The simulation results have shown that the error in determining the values of the ICE shaft rotation speed does not exceed 0.03%. This confirms the high accuracy of the algorithm.

An EMSD prototype has been created. Research of the prototype has been conducted on a test bench consisting of simulators of a 4 kW DGS and 4 kW wind turbine. The research results have shown that the use of EMSD can significantly improve the efficiency of the WDPP. The error in determining the optimal engine speed using an EMSD prototype is not more than 15%. Diesel fuel economy in the low-load area was almost 30% for variable-speed ICE with EMSD compared with the constant-speed ICE.

Author Contributions: Conceptualization, A.D. and E.S.; data curation, I.L.; formal analysis, I.L.; funding acquisition, E.S.; investigation, A.D., A.S., and I.L.; methodology, A.D.; project administration, E.S., A.S., and I.L.; resources, A.D.; software, A.D.; supervision, E.S.; validation, A.D., A.S., and I.L.; visualization, A.S.;

writing—original draft, A.S. and I.L.; and writing—review and editing, A.D. and E.S. All authors have read and agree to the published version of the manuscript.

Funding: This research was funded by the Ministry of Science and Higher Education of the Russian Federation (state task $N_{\rm P}$ 13.2078.2017/4.6 on 31 May 2017).

Conflicts of Interest: The authors declare no conflicts of interest. The funders had no role in the design of the study; in the collection, analyses, or interpretation of data; in the writing of the manuscript; or in the decision to publish the results.

Abbreviations

DGS	Diesel generator set
EMSD	Economy mode setting device
ICE	Internal combustion engine
WDPP	Wind-diesel power plant

References

- Ochoa, D.; Martinez, S. Modeling an isolated hybrid wind-diesel power system for performing frequency control studies. A case of study: San Cristobal Island, Galapagos-Ecuador. *IEEE LATAM* 2019, 17, 775–787. [CrossRef]
- Saad, Y.; Nohra, C.; Younes, R.; Abboudi, S.; Ilinca, A.; Ibrahim, H.; Feger, Z. Study of an optimized wind-diesel hybrid system for canadian remote sites. In Proceedings of the 2017 IEEE Electrical Power and Energy Conference (EPEC), Saskatoon, SK, Canada, 22–25 October 2017; pp. 1–6.
- Khvatov, O.S.; Dar'enkov, A.B. Power plant based on a variable-speed diesel generator. *Russ. Electr. Engin.* 2014, *85*, 145–149. [CrossRef]
- 4. Elistratov, V.V.; Bogun, I.V.; Kasina, V.I. Optimization of wind-diesel power plants parameters and placement for power supply of Russia's Northern Regions consumers. In Proceedings of the 2019 16th Conference on Electrical Machines, Drives and Power Systems (ELMA), Varna, Bulgaria, 6–8 June 2019; pp. 1–5.
- Chernov, D.A.; Karpov, N.D.; Tyagunov, M.G. Features of design and operation of wind-diesel complexes. In Proceedings of the 2018 International Ural Conference on Green Energy (UralCon), Chelyabinsk, Russia, 4–6 October 2018; pp. 34–38.
- 6. Nguyen-Hong, N.; Nakanishi, Y. Optimal scheduling of an isolated wind-diesel-battery system considering forecast error and frequency response. In Proceedings of the 2018 7th International Conference on Renewable Energy Research and Applications (ICRERA), Paris, France, 14–17 October 2018; pp. 464–468.
- Zaki Diab, A.A.; Sultan, H.M.; Mohamed, I.S.; Kuznetsov, O.N.; Do, T.D. Application of different optimization algorithms for optimal sizing of PV/wind/diesel/battery storage stand-alone hybrid microgrid. *IEEE Access* 2019, 7, 119223–119245. [CrossRef]
- Nguyen-Hong, N.; Nguyen-Duc, H.; Nakanishi, Y. Optimal sizing of energy storage devices in isolated wind-diesel systems considering load growth uncertainty. *IEEE Trans. Ind. Appl.* 2018, 54, 1983–1991. [CrossRef]
- Zhu, C.; Liu, F.; Hu, S.; Liu, S. Research on capacity optimization of PV-wind-diesel-battery hybrid generation system. In Proceedings of the 2018 International Power Electronics Conference (IPEC-Niigata 2018-ECCE Asia), Niigata, Japan, 20–24 May 2018; pp. 3052–3057.
- Mi, Y.; Ma, C.; Fu, Y.; Wang, C.; Wang, P.; Loh, P.C. The SVC additional adaptive voltage controller of isolated wind-diesel power system based on double sliding-mode optimal strategy. *IEEE Trans. Sustain. Energy* 2018, 9, 24–34. [CrossRef]
- Zargar, M.Y.; Mufti, M.; Lone, S.A. Voltage and frequency control of a hybrid Wind-Diesel system using SVC and predictively controlled SMES. In Proceedings of the 2017 6th International Conference on Computer Applications in Electrical Engineering-Recent Advances (CERA), Roorkee, India, 5–7 October 2017; pp. 25–30.
- Rezkallah, M.; Chandra, A.; Saad, M.; Tremblay, M.; Singh, B.; Singh, S.; Ibrahim, H. Composite control strategy for a PV-wind-diesel based off-grid power generation system supplying unbalanced non-linear loads. In Proceedings of the 2018 IEEE Industry Applications Society Annual Meeting (IAS), Portland, OR, USA, 23–27 September 2018; pp. 1–6.

- 13. Esmaeilian, H.R.; Fadaeinedjad, R. A remedy for mitigating voltage fluctuations in small remote wind-diesel systems using network theory concepts. *IEEE Trans. Smart Grid* **2018**, *9*, 4162–4171. [CrossRef]
- 14. Tiwari, S.K.; Singh, B.; Goel, P.K. Control of wind-diesel hybrid system with BESS for optimal operation. *IEEE Trans. Ind. Appl.* **2019**, *55*, 1863–1872. [CrossRef]
- Dar'enkov, A.B.; Guzev, S.A.; Fedorov, O.V. Autonomous power plant with variable speed based on multi-windings generator. In Proceedings of the 2017 International Conference on Industrial Engineering, Applications and Manufacturing (ICIEAM), St. Petersburg, Russia, 16–19 May 2017; pp. 1–5.
- 16. Baikov, A.I.; Dar'enkov, A.B.; Sosnina, E.N. Simulation modeling of a wind-diesel power plant. *Russ. Electr. Engin.* **2018**, *18*, 161–167. [CrossRef]
- 17. Baikov, A. *Modelirovanie Elektroprivodov s Ventil'nymi Preobrazovatelyami;* LAP LAMBERT Academic Publishing: Saarbrucken, Germany, 2014.



© 2020 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (http://creativecommons.org/licenses/by/4.0/).