

# Supplementary Materials: Investigation of Ternary Mixtures Containing 1-Ethyl-3-methylimidazolium Bis(trifluoromethanesulfonyl)-azanide, Ethylene Carbonate and Lithium Bis(trifluoromethanesulfonyl)azanide

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**Table S1.** Density data of the mixtures with Li-TFSA at pressure  $p = 0.1$  MPa (Standard uncertainties  $u$  are  $u(d) = 0.0005$  g·cm $^{-3}$ ,  $u(p) = 5$  kPa,  $u(T) = 0.01$  K).

| EMIM-TFSA:EC<br>(wt/wt) | Li-TFSA<br>mol·kg $^{-1}$ | $d$ g·cm $^{-3}$<br>20 °C | $d$ g·cm $^{-3}$<br>40 °C | $d$ g·cm $^{-3}$<br>60 °C | $d$ g·cm $^{-3}$<br>80 °C |
|-------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 100:0                   | 0                         | 1.5240                    | 1.5038                    | 1.4838                    | 1.4642                    |
| 80:20                   | 0                         | 1.4858                    | 1.4646                    | 1.4438                    | 1.4232                    |
| 60:40                   | 0                         | 1.4476                    | 1.4259                    | 1.4044                    | 1.3831                    |
| 40:60                   | 0                         | 1.4096                    | 1.3873                    | 1.3653                    | 1.3434                    |
| 20:80                   | 0                         | 1.3765                    | 1.3541                    | 1.3316                    | 1.3092                    |
| 0:100                   | 0                         | —                         | 1.3219                    | 1.2991                    | 1.2763                    |
| 100:0                   | 0.6                       | 1.5848                    | 1.5637                    | 1.5428                    | 1.5222                    |
| 80:20                   | 0.6                       | 1.5480                    | 1.5265                    | 1.5051                    | 1.484                     |
| 60:40                   | 0.6                       | 1.5122                    | 1.4903                    | 1.4684                    | 1.4466                    |
| 40:60                   | 0.6                       | 1.4868                    | 1.4643                    | 1.4422                    | 1.4202                    |
| 20:80                   | 0.6                       | 1.4554                    | 1.4326                    | 1.4101                    | 1.3877                    |
| 0:100                   | 0.6                       | 1.4321                    | 1.4032                    | 1.3816                    | 1.3591                    |
| 100:0                   | 1.2                       | 1.6276                    | 1.6055                    | 1.5837                    | 1.5619                    |
| 80:20                   | 1.2                       | 1.6161                    | 1.5939                    | 1.5720                    | 1.5502                    |
| 60:40                   | 1.2                       | 1.5933                    | 1.5707                    | 1.5485                    | 1.5266                    |
| 40:60                   | 1.2                       | 1.5656                    | 1.5428                    | 1.5203                    | 1.4980                    |
| 20:80                   | 1.2                       | 1.5353                    | 1.5126                    | 1.4899                    | 1.4670                    |
| 0:100                   | 1.2                       | 1.5139                    | 1.4907                    | 1.4677                    | 1.4449                    |

**Table S2a.** Linear fitting ( $ax + b$ ) of density data according to EC mass percentage (density *vs.* EC mass percentage at specified Li-TFSA concentration).

| Li-TFSA | T °C | $a$ 10 $^{-3}$ g·cm $^{-3}$ | $b$ g·cm $^{-3}$ | $R^2$ |
|---------|------|-----------------------------|------------------|-------|
| 0       | 20   | -1.86 ± 0.03                | 1.5229           | 0.999 |
| 0       | 40   | -1.83 ± 0.04                | 1.5010           | 0.998 |
| 0       | 60   | -1.86 ± 0.04                | 1.4808           | 0.998 |
| 0       | 80   | -1.88 ± 0.04                | 1.4610           | 0.997 |
| 0.6     | 20   | -1.52 ± 0.06                | 1.5794           | 0.992 |
| 0.6     | 40   | -1.59 ± 0.05                | 1.5594           | 0.996 |
| 0.6     | 60   | -1.60 ± 0.05                | 1.5382           | 0.995 |
| 0.6     | 80   | -1.62 ± 0.05                | 1.5174           | 0.995 |
| 1.2     | 20   | -1.20 ± 0.07                | 1.6436           | 0.983 |
| 1.2     | 40   | -1.21 ± 0.07                | 1.6215           | 0.983 |
| 1.2     | 60   | -1.22 ± 0.07                | 1.5998           | 0.983 |
| 1.2     | 80   | -1.23 ± 0.07                | 1.5784           | 0.983 |

The average of the slope  $\bar{m}$  at 0 mol·kg $^{-1}$ , 0.6 mol·kg $^{-1}$  and 1.2 mol·kg $^{-1}$  is calculated as  $\bar{m} = \frac{1}{n} \sum_{i=1}^n m_i$ . The error  $\Delta$  of the average value is determined by  $\Delta = \sqrt{\frac{1}{n} \sum_{i=1}^n \Delta_i^2}$ .

**Table S2b.** Second order of polynomial fitting ( $ax^2 + bx + c$ ) of density data according to EC mass percentage (density vs. EC mass percentage at specified Li-TFSA concentration).

| Li-TFSA | T °C | a 10 <sup>-6</sup> g·cm <sup>-3</sup> | b 10 <sup>-3</sup> g·cm <sup>-3</sup> | c g·cm <sup>-3</sup> | R <sup>2</sup> |
|---------|------|---------------------------------------|---------------------------------------|----------------------|----------------|
| 0       | 20   | 1.86 ± 0.77                           | -2.00 ± 0.06                          | 1.5229               | 0.9996         |
| 0       | 40   | 2.56 ± 0.43                           | -2.08 ± 0.04                          | 1.5010               | 0.9998         |
| 0       | 60   | 2.71 ± 0.42                           | -2.13 ± 0.04                          | 1.4808               | 0.9998         |
| 0       | 80   | 2.87 ± 0.42                           | -2.17 ± 0.04                          | 1.4610               | 0.9998         |
| 0.6     | 20   | 3.79 ± 0.89                           | -1.90 ± 0.09                          | 1.5794               | 0.9986         |
| 0.6     | 40   | 2.54 ± 1.04                           | -1.84 ± 0.11                          | 1.5594               | 0.9982         |
| 0.6     | 60   | 2.88 ± 1.00                           | -1.88 ± 0.10                          | 1.5382               | 0.9983         |
| 0.6     | 80   | 3.03 ± 1.02                           | -1.92 ± 0.11                          | 1.5174               | 0.9983         |
| 1.2     | 20   | -3.55 ± 1.92                          | -0.84 ± 0.20                          | 1.6436               | 0.9892         |
| 1.2     | 40   | -3.57 ± 1.88                          | -0.85 ± 0.20                          | 1.6215               | 0.9897         |
| 1.2     | 60   | -3.59 ± 1.91                          | -0.86 ± 0.20                          | 1.5998               | 0.9897         |
| 1.2     | 80   | -3.65 ± 1.98                          | -0.87 ± 0.21                          | 1.5784               | 0.9891         |

**Table S3.** Free VFTH fitting of the viscosity data. For the fitting procedure, the following initial fitting parameters are used:  $\eta_0 = 0.2 \text{ mPa}\cdot\text{s}$ ;  $D = 4$ ;  $T_0 = 160 \text{ K}$ . No additional assumptions were done during the fitting procedure otherwise mentioned (Standard uncertainties  $u$  are  $u(T_g) = 3 \text{ }^\circ\text{C}$ ,  $u(D) = 0.025 \cdot D$ ,  $u(m) = 0.03 \cdot m$ ,  $u(T_0) = 0.015 \cdot T_0$ ,  $u(\eta_0) = 0.05 \cdot \eta_0$ ).

| Ratio<br>EMIM-<br>TFSA:EC<br>(wt/wt) | c(Li-TFSA)<br>mol·kg <sup>-1</sup> | $\eta_0 \cdot 10^{-2}$<br>mPa·s | T <sub>0</sub> /K | D ± (≤0.1) | m       | T <sub>g</sub> /K DSC * | R <sup>2</sup> | $\eta_{20^\circ\text{C}}/\eta_{120^\circ\text{C}}$ |
|--------------------------------------|------------------------------------|---------------------------------|-------------------|------------|---------|-------------------------|----------------|--|
| 100:0                                | 0                                  | 18.3 ± 0.9                      | 172.2 ± 1.5       | 3.8        | 171 ± 4 | 187.85                  | 0.9997         | 11.3   |
| 100:0                                | 0.3                                | 19.9 ± 0.8                      | 181.1 ± 1.1       | 3.6        | 178 ± 4 | 189.55                  | 0.9998         | 16.0   |
| 100:0                                | 0.6                                | 26.3 ± 0.9                      | 195.4 ± 0.7       | 3.1        | 207 ± 3 | 199.25                  | 0.9999         | 22.2   |
| 100:0                                | 0.9                                | 29.3 ± 1.2                      | 200.9 ± 0.7       | 3.1        | 204 ± 3 | 207.05                  | 0.9999         | 34.3   |
| 100:0                                | 1.2                                | 31.1 ± 2.7                      | 190.0 ± 1.4 ***   | 4.1        | 160 ± 5 | 209.25                  | 0.9998         | 45.9   |
| 80:20                                | 0                                  | 11.7 ± 0.8                      | 158.2 ± 2.4       | 4.2        | 157 ± 7 | 181.25                  | 0.9994         | 7.8  |
| 80:20                                | 0.3                                | 18.8 ± 0.7                      | 183.8 ± 1.2       | 3.0        | 215 ± 5 | 187.25                  | 0.9998         | 10.8   |
| 80:20                                | 0.6                                | 21.7 ± 0.8                      | 191.8 ± 0.7       | 2.9        | 220 ± 4 | 193.65                  | 0.9998         | 15.2   |
| 80:20                                | 0.9                                | 25.0 ± 0.9                      | 197.9 ± 0.7       | 2.9        | 220 ± 4 | 200.65                  | 0.9998         | 21.1   |
| 80:20                                | 1.2                                | 27.6 ± 1.2                      | 205.7 ± 0.7       | 2.8        | 223 ± 4 | 207.05                  | 0.9998         | 34.7   |
| 60:40                                | 0                                  | 6.6 ± 0.1                       | 132.9 ± 0.4       | 5.8        | 118 ± 1 | 176.55                  | 0.9999         | 6.1  |
| 60:40                                | 0.3                                | 16.8 ± 0.1                      | 191.2 ± 0.3       | 2.7        | 238 ± 2 | 183.55                  | 0.9998         | 7.8  |
| 60:40                                | 0.6                                | 17.1 ± 0.2                      | 184.7 ± 0.3       | 2.9        | 218 ± 1 | 189.95                  | 0.9998         | 10.7   |
| 60:40                                | 0.9                                | 19.9 ± 0.2                      | 194.1 ± 0.2       | 2.8        | 225 ± 1 | 197.55                  | 0.9999         | 16.2   |
| 60:40                                | 1.2                                | 24.3 ± 0.2                      | 203.3 ± 0.1       | 2.7        | 234 ± 1 | 205.45                  | 0.9999         | 24.4   |
| 40:60                                | 0                                  | 6.0 ± 0.1                       | 129.3 ± 0.5       | 5.6        | 121 ± 1 | -- **                   | 0.9999         | 5.0  |
| 40:60                                | 0.3                                | 13.6 ± 0.1                      | 170.4 ± 0.5       | 2.9        | 216 ± 2 | 182.95                  | 0.9998         | 6.2  |
| 40:60                                | 0.6                                | 16.6 ± 0.2                      | 181.8 ± 0.4       | 2.7        | 235 ± 2 | 187.65                  | 0.9997         | 7.9  |
| 40:60                                | 0.9                                | 18.8 ± 0.2                      | 191.3 ± 0.3       | 2.7        | 237 ± 2 | 194.55                  | 0.9998         | 11.3   |
| 40:60                                | 1.2                                | 21.8 ± 0.2                      | 199.5 ± 0.2       | 2.6        | 237 ± 1 | 204.65                  | 0.9999         | 18.3   |
| 20:80                                | 0                                  | 6.3 ± 0.1                       | 130.8 ± 0.5       | 5.0        | 134 ± 1 | -- **                   | 0.9998         | 6.0  |
| 20:80                                | 0.3                                | 11.2 ± 0.1                      | 162.5 ± 0.6       | 3.2        | 202 ± 2 | 202.45                  | 0.9997         | 5.6  |
| 20:80                                | 0.6                                | 20.3 ± 0.2                      | 185.3 ± 0.5       | 2.3        | 277 ± 3 | 205.55                  | 0.9995         | 6.3  |
| 20:80                                | 0.9                                | 19.0 ± 0.2                      | 189.7 ± 0.4       | 2.4        | 253 ± 2 | 190.35                  | 0.9997         | 9.5  |
| 20:80                                | 1.2                                | 22.0 ± 0.2                      | 199.1 ± 0.3       | 2.4        | 255 ± 1 | 192.15                  | 0.9998         | 14.3   |
| 0:100                                | 0                                  | 3.1 ± 0.1                       | 109.9 ± 0.2       | 7.1        | 99 ± 1  | 187.95                  | 0.9999         | 4.0  |
| 0:100                                | 0.3                                | 7.9 ± 0.1                       | 145.3 ± 0.6       | 4.0        | 162 ± 2 | 217.65                  | 0.9997         | 4.7  |
| 0:100                                | 0.6                                | 11.7 ± 0.1                      | 166.8 ± 0.6       | 3.1        | 207 ± 2 | 212.85                  | 0.9996         | 5.9  |
| 0:100                                | 0.9                                | 15.5 ± 0.2                      | 186.1 ± 0.5       | 2.5        | 249 ± 2 | 215.25                  | 0.9996         | 8.5  |
| 0:100                                | 1.2                                | 16.7 ± 0.2                      | 192.6 ± 0.3       | 2.6        | 238 ± 2 | 200.75                  | 0.9997         | 12.4   |

\* DSC: heating at 10 K/min; \*\* No  $T_g$  could be extracted from the measurement; \*\*\* the lower fitting border of  $T_0$  was set to 190 K.

For the fitting procedure, the following initial fitting parameters are used:  $\eta_0 = 0.2 \text{ mPa}\cdot\text{s}$ ;  $D = 4$ ;  $T_0 = 160 \text{ K}$ . No additional assumptions were done during the fitting procedure otherwise mentioned.

**Table S4.** Data of flow activation energies.

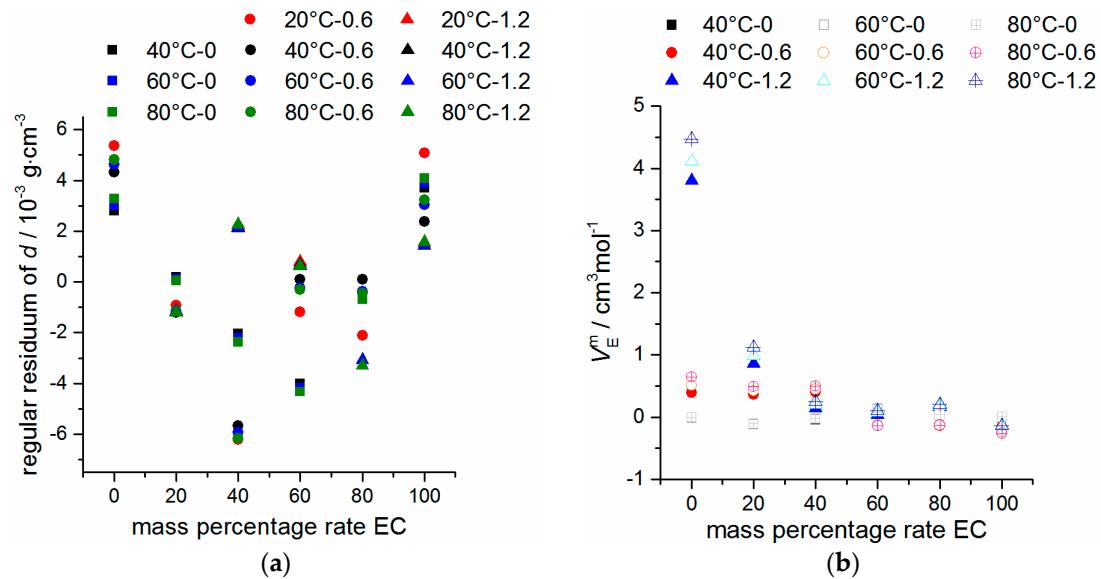
| EMIM-TFSA:EC<br>(wt/wt) | Li-TFSA mol·kg <sup>-1</sup> | E <sub>A</sub> kJ·mol <sup>-1</sup> | R <sup>2</sup> |
|-------------------------|------------------------------|-------------------------------------|----------------|
| 100:0                   | 0                            | 22.4 ± 0.2                          | 0.993          |
| 80:20                   | 0                            | 19.4 ± 0.2                          | 0.991          |
| 60:40                   | 0                            | 17.6 ± 0.2                          | 0.990          |
| 40:60                   | 0                            | 15.8 ± 0.2                          | 0.989          |
| 20:80                   | 0                            | 14.7 ± 0.2                          | 0.986          |
| 0:100                   | 0                            | 14.6 ± 0.3                          | 0.992          |
| 100:0                   | 0.3                          | 25.0 ± 0.3                          | 0.993          |
| 80:20                   | 0.3                          | 21.8 ± 0.3                          | 0.993          |
| 60:40                   | 0.3                          | 18.7 ± 0.2                          | 0.992          |
| 40:60                   | 0.3                          | 17.2 ± 0.2                          | 0.989          |
| 20:80                   | 0.3                          | 16.4 ± .02                          | 0.989          |
| 0:100                   | 0.3                          | 15.6 ± 0.3                          | 0.985          |
| 100:0                   | 0.6                          | 27.3 ± 0.3                          | 0.992          |
| 80:20                   | 0.6                          | 24.2 ± 0.3                          | 0.993          |
| 60:40                   | 0.6                          | 21.8 ± 0.3                          | 0.991          |
| 40:60                   | 0.6                          | 19.3 ± 0.2                          | 0.992          |
| 20:80                   | 0.6                          | 17.4 ± 0.2                          | 0.990          |
| 0:100                   | 0.6                          | 17.0 ± 0.2                          | 0.989          |
| 100:0                   | 0.9                          | 30.9 ± 0.4                          | 0.992          |
| 80:20                   | 0.9                          | 26.9 ± 0.3                          | 0.991          |
| 60:40                   | 0.9                          | 24.7 ± 0.3                          | 0.992          |
| 40:60                   | 0.9                          | 22.3 ± 0.3                          | 0.991          |
| 20:80                   | 0.9                          | 20.6 ± 0.3                          | 0.992          |
| 0:100                   | 0.9                          | 19.7 ± 0.2                          | 0.992          |
| 100:0                   | 1.2                          | 34.6 ± 0.8                          | 0.992          |
| 80:20                   | 1.2                          | 30.8 ± 0.4                          | 0.991          |
| 60:40                   | 1.2                          | 28.1 ± 0.3                          | 0.992          |
| 40:60                   | 1.2                          | 25.7 ± 0.4                          | 0.990          |
| 20:80                   | 1.2                          | 24.1 ± 0.3                          | 0.992          |
| 0:100                   | 1.2                          | 23.0 ± 0.3                          | 0.991          |

**Table S5.** Conductivity data of the solvent mixtures at pressure  $p = 0.1$  MPa (Standard uncertainties  $u$  are  $u(\chi) = 0.0002$ ,  $u(\kappa) = 0.03 \cdot \kappa$ ,  $u(p) = 5$  kPa,  $u(\chi) = 0.0002$ ,  $u(T) = 0.1$  K).

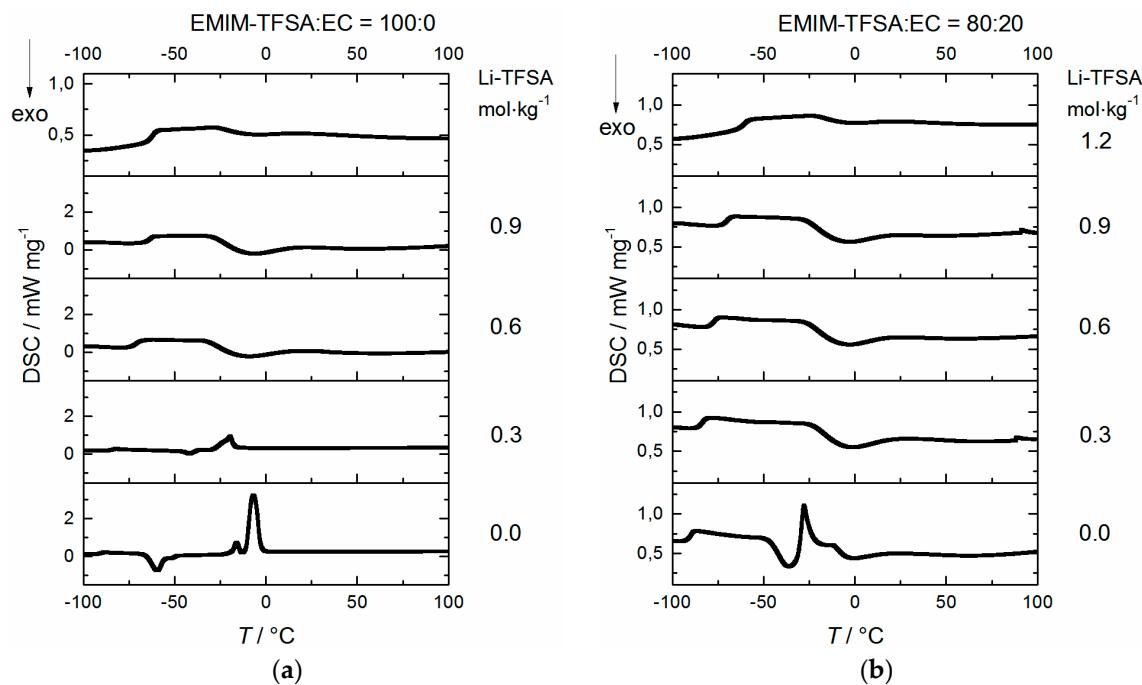
| EMIM-TFSA:EC<br>(wt/wt) | $\chi$ EC | $c$ (Li-TFSA)<br>mol·kg <sup>-1</sup> | $\kappa$  | $\kappa$  | $\kappa$  | $\kappa$  |
|-------------------------|-----------|---------------------------------------|---|---|---|---|
|                         |           |                                       | mS·cm <sup>-1</sup><br>20 °C<br>$u(\kappa) = 0.03 \cdot \kappa$ | mS·cm <sup>-1</sup><br>40 °C<br>$u(\kappa) = 0.04 \cdot \kappa$ | mS·cm <sup>-1</sup><br>60 °C<br>$u(\kappa) = 0.05 \cdot \kappa$ | mS·cm <sup>-1</sup><br>80 °C<br>$u(\kappa) = 0.05 \cdot \kappa$ |
| 100:0                   | 0         | 0                                     | 7.34  | 13.48   | 20.56   | 28.93   |
| 80:20                   | 0.526     | 0                                     | 12.37   | 19.69   | 27.14   | 40.37   |
| 60:40                   | 0.748     | 0                                     | 15.68   | 22.47   | 30.53   | 42.53   |
| 40:60                   | 0.870     | 0                                     | 14.42   | 20.45   | 26.95   | 35.92   |
| 20:80                   | 0.912     | 0                                     | 10.3  | 14.23   | 18.42   | 22.89   |
| 0:100                   | 1.000     | 0                                     | --  | --  | --  | --  |
| 100:0                   | 0         | 0.3                                   | 4.97  | 9.33  | 15.16   | 22.03   |
| 80:20                   | 0.526     | 0.3                                   | 8.08  | 13.73   | 20.43   | 27.78   |
| 60:40                   | 0.748     | 0.3                                   | 10.88   | 17.06   | 24.12   | 31.67   |
| 40:60                   | 0.870     | 0.3                                   | 11.53   | 17.35   | 24.9  | 32.99   |
| 20:80                   | 0.912     | 0.3                                   | 7.09  | 14.15   | 18.89   | 23.92   |
| 0:100                   | 1.000     | 0.3                                   | 4.76  | 6.53  | 8.54  | 10.73   |
| 100:0                   | 0         | 0.6                                   | 2.87  | 6.01  | 10.42   | 16.13   |
| 80:20                   | 0.526     | 0.6                                   | 4.96  | 9.09  | 14.67   | 21.09   |
| 60:40                   | 0.748     | 0.6                                   | 6.94  | 10.92   | 17.96   | 24.76   |
| 40:60                   | 0.870     | 0.6                                   | 7.75  | 12.1  | 18.5  | 25.8  |
| 20:80                   | 0.912     | 0.6                                   | 8.11  | 12.27   | 17.02   | 22.23   |
| 0:100                   | 1.000     | 0.6                                   | 6.02  | 8.66  | 11.9  | 15.59   |
| 100:0                   | 0         | 0.9                                   | 1.24  | 3.15  | 6.7   | 11.12   |
| 80:20                   | 0.526     | 0.9                                   | 2.43  | 5.18  | 9   | 13.9  |
| 60:40                   | 0.748     | 0.9                                   | 4.17  | 7.56  | 12.24   | 17.69   |
| 40:60                   | 0.870     | 0.9                                   | 5.22  | 9.14  | 14.01   | 19.52   |
| 20:80                   | 0.912     | 0.9                                   | 6.68  | 10.59   | 15.12   | 20.2  |
| 0:100                   | 1.000     | 0.9                                   | 5.31  | 8.39  | 11.73   | 15.29   |
| 100:0                   | 0         | 1.2                                   | 0.92  | 2.46  | 5.58  | 9.49  |
| 80:20                   | 0.526     | 1.2                                   | 1.11  | 2.8   | 6.05  | 9.82  |
| 60:40                   | 0.748     | 1.2                                   | 1.76  | 4.59  | 7.86  | 12.06   |
| 40:60                   | 0.870     | 1.2                                   | 2.46  | 5.48  | 9.13  | 13.56   |
| 20:80                   | 0.912     | 1.2                                   | 2.70  | 5.93  | 9.24  | 13.26   |
| 0:100                   | 1.000     | 1.2                                   | 2.83  | 6.29  | 9.19  | 12.9  |

**Table S6.** Results of Walden plots and linear regression.

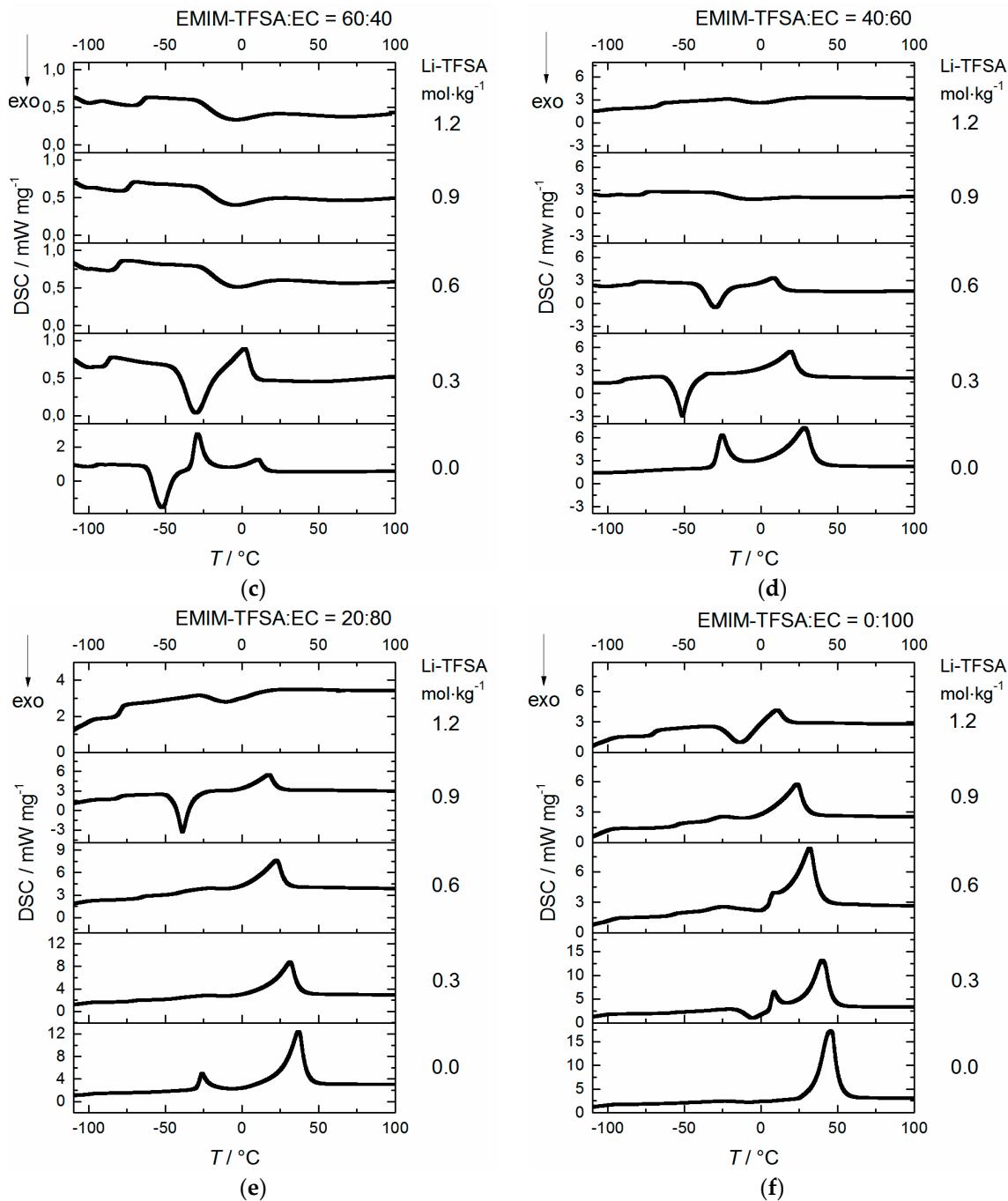
| Ratio (wt/wt) EMIM-TFSA:EC | <i>c</i> (Li-TFSA) mol·kg <sup>-1</sup> | Slope ( <i>a</i> ) | <i>R</i> <sup>2</sup> |
|----------------------------|---|--------------------|-----------------------|
| 100:0                      | 0                                       | 0.75 ± 0.01        | 0.999                 |
| 100:0                      | 0.3                                     | 0.75 ± 0.02        | 0.998                 |
| 100:0                      | 0.6                                     | 0.75 ± 0.02        | 0.998                 |
| 100:0                      | 0.9                                     | 0.83 ± 0.03        | 0.997                 |
| 100:0                      | 1.2                                     | 0.83 ± 0.03        | 0.997                 |
| 80:20                      | 0                                       | 0.79 ± 0.03        | 0.997                 |
| 80:20                      | 0.3                                     | 0.72 ± 0.01        | 0.999                 |
| 80:20                      | 0.6                                     | 0.73 ± 0.02        | 0.997                 |
| 80:20                      | 0.9                                     | 0.77 ± 0.02        | 0.999                 |
| 80:20                      | 1.2                                     | 0.82 ± 0.03        | 0.995                 |
| 60:40                      | 0                                       | 0.80 ± 0.01        | 0.999                 |
| 60:40                      | 0.3                                     | 0.74 ± 0.02        | 0.999                 |
| 60:40                      | 0.6                                     | 0.73 ± 0.02        | 0.998                 |
| 60:40                      | 0.9                                     | 0.71 ± 0.02        | 0.998                 |
| 60:40                      | 1.2                                     | 0.80 ± 0.03        | 0.996                 |
| 40:60                      | 0                                       | 0.73 ± 0.04        | 0.992                 |
| 40:60                      | 0.3                                     | 0.83 ± 0.03        | 0.997                 |
| 40:60                      | 0.6                                     | 0.81 ± 0.04        | 0.993                 |
| 40:60                      | 0.9                                     | 0.73 ± 0.02        | 0.998                 |
| 40:60                      | 1.2                                     | 0.78 ± 0.02        | 0.998                 |
| 20:80                      | 0                                       | 0.79 ± 0.01        | 0.999                 |
| 20:80                      | 0.3                                     | 0.89 ± 0.05        | 0.991                 |
| 20:80                      | 0.6                                     | 0.76 ± 0.02        | 0.999                 |
| 20:80                      | 0.9                                     | 0.68 ± 0.01        | 0.999                 |
| 20:80                      | 1.2                                     | 0.79 ± 0.03        | 0.995                 |
| 0:100                      | 0                                       | —                  | —                     |
| 0:100                      | 0.3                                     | 0.73 ± 0.02        | 0.998                 |
| 0:100                      | 0.6                                     | 0.75 ± 0.02        | 0.998                 |
| 0:100                      | 0.9                                     | 0.70 ± 0.01        | 0.999                 |
| 0:100                      | 1.2                                     | 0.69 ± 0.04        | 0.998                 |



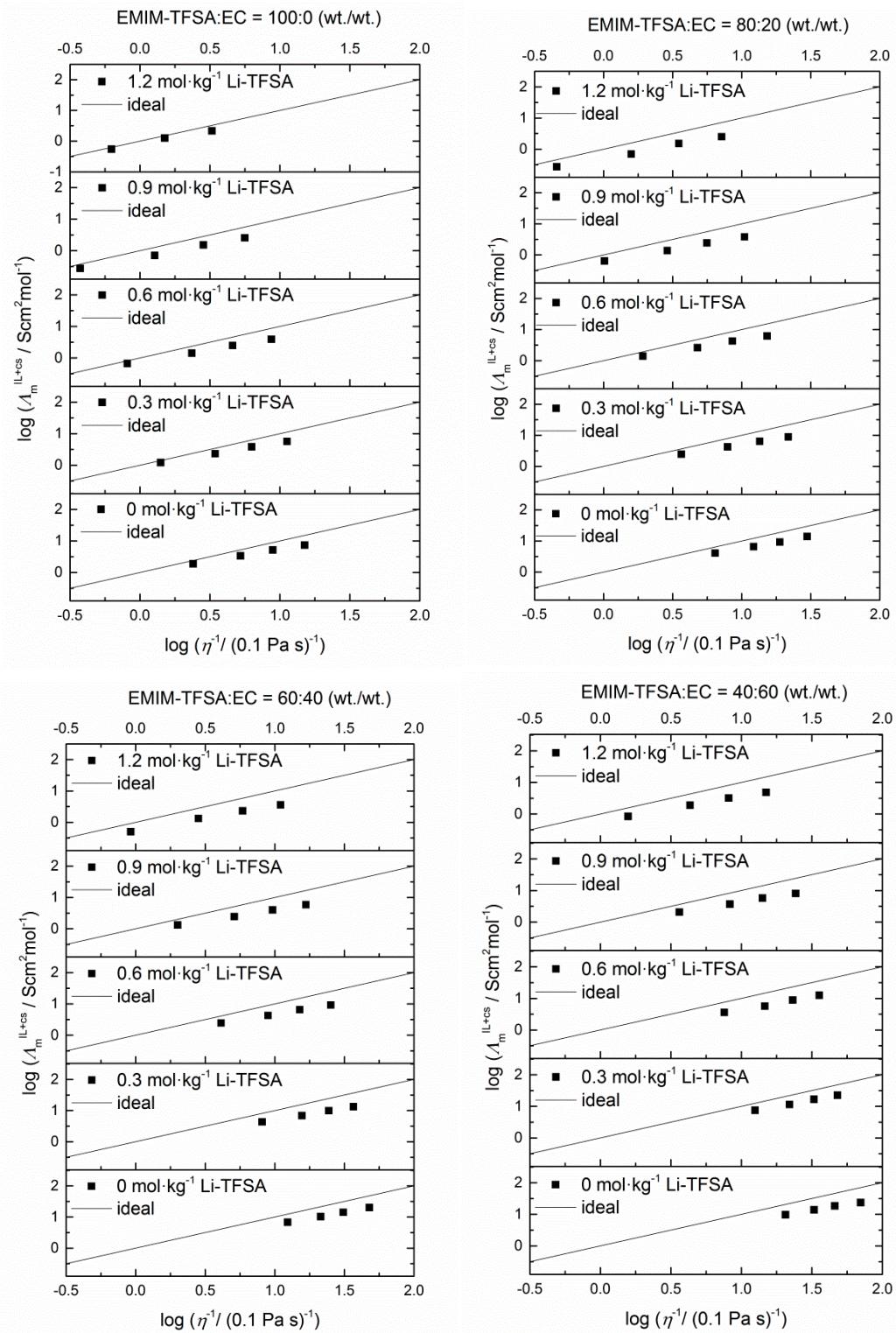
**Figure S1.** Residuum (a) of the real density of selected mixtures from the linear ideal behavior; Molar excess volume (b) of EMIM-TFSA/EC/Li-TFSA ternary mixtures as a function of the EC mass percentage rate (related to the EMIM-TFSA/EC solvent mixture) at different temperatures.

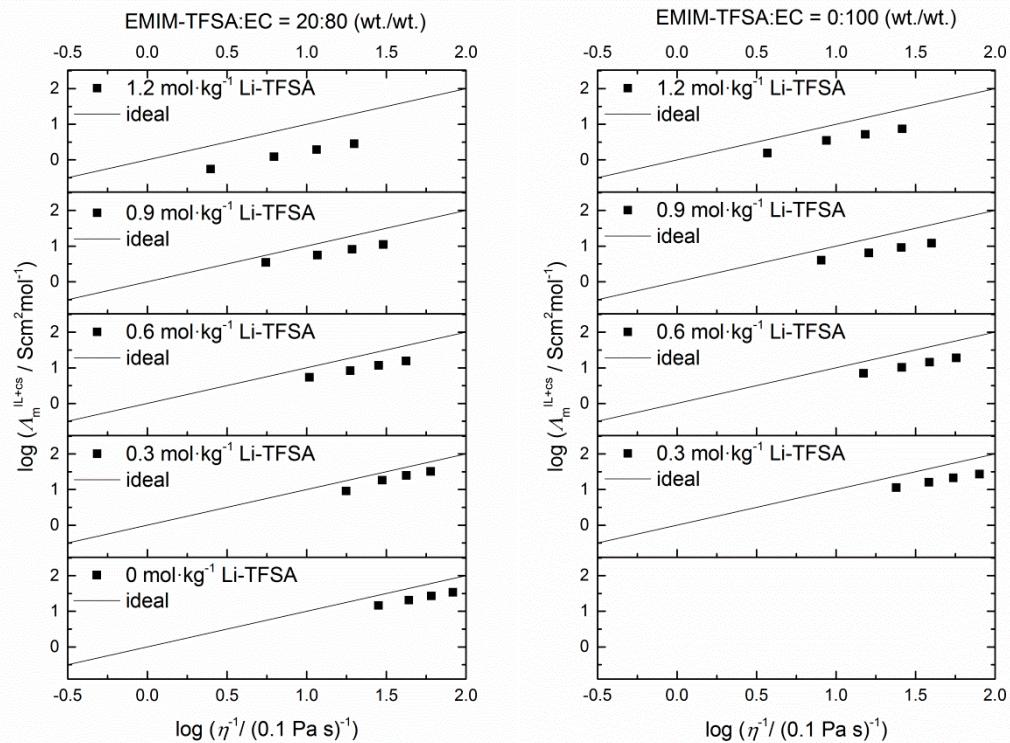


**Figure S2. Cont.**



**Figure S2.** (a–f) DSC measurements during heating ( $20\text{ K}\cdot\text{min}^{-1}$ ) in the temperature range of  $-110$  to  $100\text{ }^\circ\text{C}$  (exo down) of EMIM-TFSA: EC (wt/wt) + Li-TFSA mixtures. The concentration of Li-TFSA is mentioned on the right hand side of each figure. The composition of the solvent (EMIM-TFSA:EC) is written on the top of each figure. The figures are arranged in a descending order with respect to EC concentration.

**Figure S3. Cont.**



**Figure S3.** Walden plots of temperature-dependent (20–80°C) viscosity and conductivity data of the mixtures (EMIM-TFSA:EC = wt/wt) with selected Li-TFSA concentrations. The results of the measurements are depicted as black squares, whereas the black line displays the behavior of an ideal classical dilute aqueous solution (slope of one, labelled as “fit”). For a better comparison with plots in literature, the viscosity value is shown in units of Poise (0.1 Pa·s).